

AD-A014 732

TEST OF A SUPERSONIC AXIAL COMPRESSOR STAGE  
INCORPORATING SPLITTER VANES IN THE ROTOR

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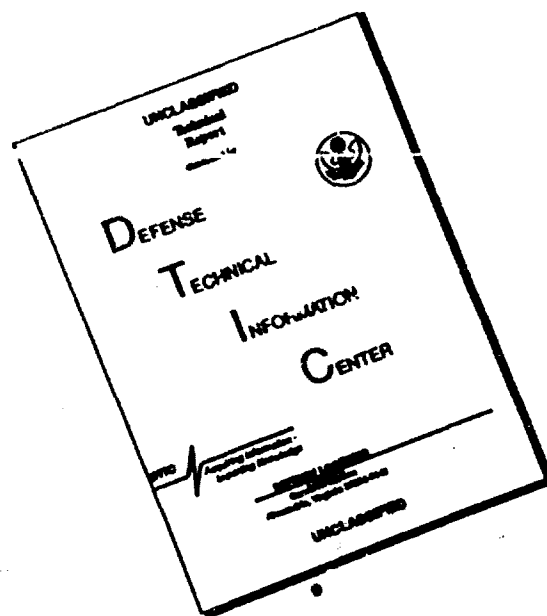
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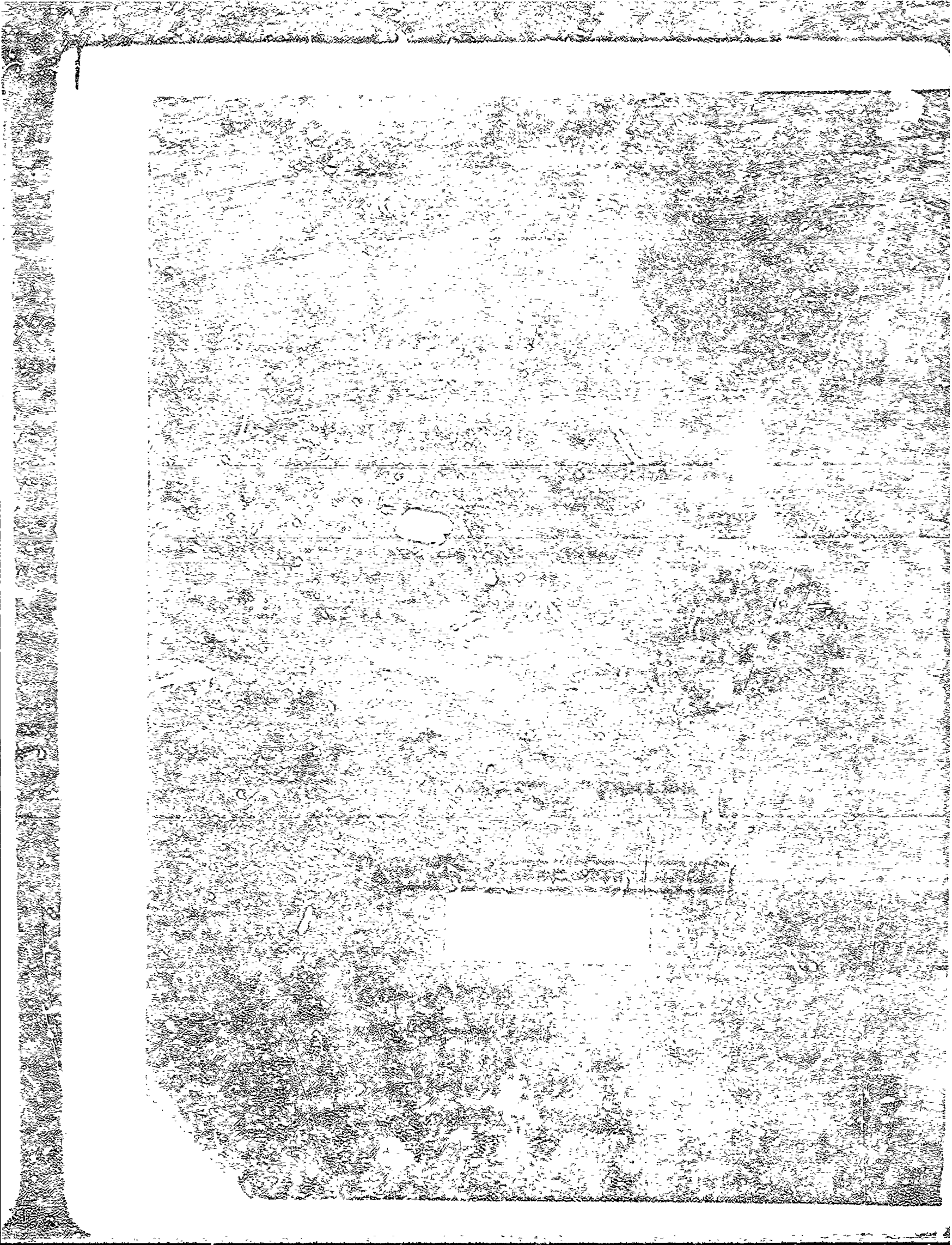
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SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER ARL 75-0165	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) TEST OF A SUPERSONIC AXIAL COMPRESSOR STAGE INCORPORATING SPLITTER VANES IN THE ROTOR		5. TYPE OF REPORT & PERIOD COVERED December 1972 - 31 Dec 1974 Technica -Interim
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) A. J. Wennerstrom W. A. Buzzell R. D. DeRose		8. CONTRACT OR GRANT NUMBER(s) Internal
9. PERFORMING ORGANIZATION NAME AND ADDRESS Fluid Mechanics Research Laboratory (LF) Aerospace Research Laboratories (AFSC) Wright-Patterson AFB, Ohio 45433		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS DoD Element 61102F Project 70650409
11. CONTROLLING OFFICE NAME AND ADDRESS Aerospace Research Laboratories (LF) Air Force Systems Command Wright-Patterson AFB, Ohio 45433		12. REPORT DATE JUNE 1975
		13. NUMBER OF PAGES 429
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) axial compressor                      gas turbines  turbine engines  turbomachinery		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Complete experimental results are presented from tests of an axial-compressor stage designed for a tip speed of 1600 ft/sec, a stage total pressure ratio of 3.06, and an inlet hub/tip radius ratio of 0.75. The rotor had been redesigned to incorporate a splitter vane between each pair of principal airfoils. At design speed, the compressor passed 88 percent of design flow, achieved a stage total pressure ratio of 2.77, and achieved isentropic efficiencies of 0.846 for the rotor and 0.674 for the stage. This represented a major improvement over the preceding configuration tested without rotor splitter.		

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vanes. Future tests are to include various types of boundary-layer control.

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## PREFACE

This interim report was prepared by Dr. Arthur J. Wennerstrom and 2/Lt William A. Buzzell of the Fluid Mechanics Research Laboratory, Aerospace Research Laboratories (AFSC), Wright-Patterson Air Force Base, Ohio and Mr. Robert D. DeRose of Systems Research Laboratories, Inc., Dayton, Ohio. The work herein reported was accomplished between December 1972 and December 1974.

The report presents results from a portion of the effort of the Fluid Machinery Research Group supervised by Dr. Arthur J. Wennerstrom and conducted under Work Unit 09 of Project 7065, "Aerospace Simulation Techniques Research," under the over-all direction of Mr. Elmer G. Johnson, Director.

## TABLE OF CONTENTS

SECTION	PAGE
I INTRODUCTION . . . . .	1
II APPARATUS . . . . .	2
1. FACILITY FLOW PATH . . . . .	2
2. COMPRESSOR TEST VEHICLE . . . . .	2
3. COMPRESSOR INSTRUMENTATION . . . . .	3
4. TEST FACILITY INSTRUMENTATION . . . . .	5
III TEST PROCEDURE AND DATA REDUCTION . . . . .	7
1. TEST PROCEDURE . . . . .	7
2. DATA REDUCTION - PHASE I . . . . .	8
3. DATA REDUCTION - PHASE II . . . . .	8
IV RESULTS . . . . .	9
1. OVER-ALL PERFORMANCE . . . . .	9
2. BLADE-ELEMENT PERFORMANCE (ACROSS BLADE) . . . . .	9
3. BLADE-ELEMENT PERFORMANCE (WITHIN-BLADE) . . . . .	9
4. ROTOR TIP DYNAMIC PRESSURE MEASUREMENTS . . . . .	10
V CONCLUSIONS . . . . .	11
. . . . .	
APPENDIX A: PHASE II WITHIN-BLADE ANALYSES (COMPUTER PRINTOUTS) . . . . .	139
1. TEST POINT 212050315040 (40%) . . . . .	141
2. TEST POINT 212050615050 (50%) . . . . .	156
3. TEST POINT 212051715560 (60%) . . . . .	171
4. TEST POINT 212070815970 (70%) . . . . .	186
5. TEST POINT 212071515980 (80%) . . . . .	201

SECTION	PAGE
6. TEST POINT 301181015885 (85%) . . . . .	216
7. TEST POINT 301181715890 (90%) . . . . .	231
8. TEST POINT 301230515695 (95%) . . . . .	246
9. TEST POINT 301231615700 (100%) . . . . .	251
10. TEST POINT 301240915602 (102%) . . . . .	276
APPENDIX B: COMPUTER INPUT DATA FOR DATA REDUCTION . . . . .	291
1. COMMON PHASE I DATA . . . . .	293
2. COMMON PHASE II FIXED DATA (LOG 1) ACROSS BLADE . . . . .	295
3. COMMON PHASE II INPUT AND TEST POINT DATA (LOG 3, 4) ACROSS BLADE . . . . .	298
4. COMMON PHASE II FIXED DATA (LOG 1) WITHIN BLADE . . . . .	300
5. COMMON PHASE II INPUT AND TEST POINT DATA (LOG 3,4) WITHIN BLADE . . . . .	306
6. INDIVIDUAL TEST INPUT DATA . . . . .	308
APPENDIX C: ADDITIONAL CALCOMP PLOTTING ROUTINE LISTINGS . . . . .	357
1. DEVPLOT LISTING . . . . .	359
2. STAPLOT LISTING . . . . .	362
APPENDIX D: RAW EXPERIMENTAL DATA . . . . .	367
REFERENCES	414



## LIST OF TABLES

TABLE		PAGE
I	INSTRUMENTATION LIST . . . . .	13
I	CALIBRATION OF SAMPLE THERMOCOUPLES . . . . .	17
III	CALIBRATION OF TEMPERATURE READOUT ELECTRONICS . . . . .	17
IV	MASS-AVERAGED COMPRESSOR PERFORMANCE . . . . .	18
V	IDENTIFICATION OF SYMBOLS FOR 40%-SPEED ACROSS-BLADE FIGURES . . . . .	31
VI	IDENTIFICATION OF SYMBOLS FOR 50%-SPEED ACROSS-BLADE FIGURES . . . . .	35
VII	IDENTIFICATION OF SYMBOLS FOR 60%-SPEED ACROSS-BLADE FIGURES . . . . .	39
VIII	IDENTIFICATION OF SYMBOLS FOR 70%-SPEED ACROSS-BLADE FIGURES . . . . .	43
IX	IDENTIFICATION OF SYMBOLS FOR 80%-SPEED ACROSS-BLADE FIGURES . . . . .	47
X	IDENTIFICATION OF SYMBOLS FOR 85%-SPEED ACROSS-BLADE FIGURES . . . . .	51
XI	IDENTIFICATION OF SYMBOLS FOR 90%-SPEED ACROSS-BLADE FIGURES . . . . .	55
XII	IDENTIFICATION OF SYMBOLS FOR 95%-SPEED ACROSS-BLADE FIGURES . . . . .	60
XIII	IDENTIFICATION OF SYMBOLS FOR 100%-SPEED ACROSS-BLADE FIGURES . . . . .	65
XIV	IDENTIFICATION OF SYMBOLS FOR 105%-SPEED ACROSS-BLADE FIGURES . . . . .	70

## LIST OF ILLUSTRATIONS

FIGURE		PAGE
1	Compressor Facility Flow Path . . . . .	19
2	Test Facility . . . . .	20
3	Compressor Cross Section with Instrumentation Locations .	21
4	Rotor with Splitter Vanes . . . . .	23
5	Vehicle Instrumentation Bulkhead . . . . .	24
6	Slot Vented Temperature Probe Design . . . . .	25
7	Temperature Calibration Setup . . . . .	26
8	Kiel Stagnation Tube Design . . . . .	27
9	Instrumentation Rakes . . . . .	28
10	Vane-Mounted Instrumentation . . . . .	29
11	Compressor Performance Map . . . . .	30
12	Rotor Relative Mach Number vs Inlet Radius (40% Speed) . . . . .	32
13	Rotor Incidence vs Inlet Radius (40% Speed) . . . . .	32
14	Rotor Diffusion Factor vs Outlet Radius (40% Speed) . . .	32
15	Rotor Loss Coefficient vs Outlet Radius (40% Speed) . . .	32
16	Rotor Deviation vs Outlet Radius (40% Speed) . . . . .	33
17	Stator Incidence vs Inlet Radius (40% Speed) . . . . .	33
18	Stator Mach. Number vs Inlet Radius (40% Speed) . . . . .	34
19	Stator Loss Coefficient vs Outlet Radius (40% Speed) . .	34
20	Stator Diffusion Factor vs Outlet Radius (40% Speed) . .	34
21	Rotor Relative Mach Number vs Inlet Radius (50% Speed) .	36
22	Rotor Incidence vs Inlet Radius (50% Speed) . . . . .	36
23	Rotor Diffusion Factor vs Outlet Radius (50% Speed) . . .	36

FIGURE		PAGE
24	Rotor Loss Coefficient vs Outlet Radius (50% Speed) . . .	36
25	Rotor Deviation vs Outlet Radius (50% Speed) . . . . .	37
26	Stator Incidence vs Inlet Radius (50% Speed) . . . . .	37
27	Stator Mach Number vs Inlet Radius (50% Speed) . . . . .	38
28	Stator Loss Coefficient vs Outlet Radius (50% Speed) . .	38
29	Stator Diffusion Factor vs Outlet Radius (50% Speed). . .	38
30	Rotor Relative Mach Number vs Inlet Radius (50% Speed) . . . . .	40
31	Rotor Incidence vs Inlet Radius (60% Speed) . . . . .	40
32	Rotor Diffusion Factor vs Outlet Radius (60% Speed) . . .	40
33	Rotor Loss Coefficient vs Outlet Radius (60% Speed) . . .	40
34	Rotor Deviation vs Outlet Radius (60% Speed) . . . . .	41
35	Stator Incidence vs Inlet Radius (60% Speed) . . . . .	41
36	Stator Mach Number vs Inlet Radius (60% Speed) . . . . .	42
37	Stator Loss Coefficient vs Outlet Radius (60% Speed). . .	43
38	Stator Diffusion Factor vs Outlet Radius (60% Speed) . . .	43
39	Rotor Relative Mach Number vs Inlet Radius (70% Speed). .	44
40	Rotor Incidence vs Inlet Radius (70% Speed) . . . . .	44
41	Rotor Diffusion Factor vs Outlet Radius (70% Speed) . . .	44
42	Rotor Loss Coefficient vs Outlet Radius (70% Speed) . . .	44
43	Rotor Deviation vs Outlet Radius (70% Speed) . . . . .	45
44	Stator Incidence vs Inlet Radius (70% Speed) . . . . .	45
45	Stator Mach Number vs Inlet Radius (70% Speed) . . . . .	46
46	Stator Loss Coefficient vs Outlet Radius (70% Speed) . .	46
47	Stator Diffusion Factor vs Outlet Radius (70% Speed) . .	46

FIGURE		PAGE
48	Rotor Relative Mach Number vs Inlet Radius (80% Speed) . .	48
49	Rotor Incidence vs Inlet Radius (80% Speed) . . . . .	48
50	Rotor Diffusion Factor vs Outlet Radius (80% Speed) . . .	48
51	Rotor Loss Coefficient vs Outlet Radius (80% Speed) . . .	48
52	Rotor Deviation vs Outlet Radius (80% Speed) . . . . .	49
53	Stator Incidence vs Inlet Radius (80% Speed) . . . . .	49
54	Stator Mach Number vs Inlet Radius (80% Speed) . . . . .	50
55	Stator Loss Coefficient vs Outlet Radius (80% Speed) . . .	50
56	Stator Diffusion Factor vs Outlet Radius (80% Speed) . . .	50
57	Rotor Relative Mach Number vs Inlet Radius (85% Speed) . .	52
58	Rotor Incidence vs Inlet Radius (85% Speed) . . . . .	52
59	Rotor Diffusion Factor vs Outlet Radius (85% Speed) . . .	52
60	Rotor Loss Coefficient vs Outlet Radius (85% Speed) . . .	52
61	Rotor Deviation vs Outlet Radius (85% Speed) . . . . .	53
62	Stator Incidence vs Inlet Radius (85% Speed) . . . . .	53
63	Stator Mach Number vs Inlet Radius (85% Speed) . . . . .	54
64	Stator Loss Coefficient vs Outlet Radius (85% Speed) . . .	54
65	Stator Diffusion Factor vs Outlet Radius (85% Speed) . . .	54
66	Rotor Relative Mach Number vs Inlet Radius (90% Speed) . .	56
67	Rotor Incidence vs Inlet Radius (90% Speed) . . . . .	56
68	Rotor Diffusion Factor vs Outlet Radius (90% Speed) . . .	56
69	Rotor Loss Coefficient vs Outlet Radius (90% Speed) . . .	56
70	Rotor Deviation vs Outlet Radius (90% Speed) . . . . .	57
71	Stator Incidence vs Inlet Radius (90% Speed) . . . . .	58

FIGURE		PAGE
72	Stator Mach Number vs Inlet Radius (90% Speed) . . . . .	59
73	Stator Loss Coefficient vs Outlet Radius (90% Speed) . .	59
74	Stator Diffusion Factor vs Outlet Radius (90% Speed) . .	59
75	Rotor Relative Mach Number vs Inlet Radius (95% Speed) .	61
76	Rotor Incidence vs Inlet Radius (95% Speed) . . . . .	61
77	Rotor Diffusion Factor vs Outlet Radius (95% Speed) . . .	61
78	Rotor Loss Coefficient vs Outlet Radius (95% Speed) . . .	61
79	Rotor Deviation vs Outlet Radius (95% Speed) . . . . .	62
80	Stator Incidence vs Inlet Radius (95% Speed) . . . . .	63
81	Stator Mach Number vs Inlet Radius (95% Speed) . . . . .	64
82	Stator Loss Coefficient vs Outlet Radius (95% Speed) . .	64
83	Stator Diffusion Factor vs Outlet Radius (95% Speed) . .	64
84	Rotor Relative Mach Number vs Inlet Radius (100% Speed) .	66
85	Rotor Incidence vs Inlet Radius (100% Speed) . . . . .	66
86	Rotor Diffusion Factor vs Outlet Radius (100% Speed) . .	66
87	Rotor Loss Coefficient vs Outlet Radius (100% Speed) . .	66
88	Rotor Deviation vs Outlet Radius (100% Speed) . . . . .	67
89	Stator Incidence vs Inlet Radius (100% Speed) . . . . .	68
90	Stator Mach Number vs Inlet Radius (100% Speed) . . . . .	69
91	Stator Loss Coefficient vs Outlet Radius (100% Speed) . .	69
92	Stator Diffusion Factor vs Outlet Radius (100% Speed) . .	69
93	Rotor Relative Mach Number vs Inlet Radius (102% Speed) .	71
94	Rotor Incidence vs Inlet Radius (102% Speed) . . . . .	71
95	Rotor Diffusion Factor vs Outlet Radius (102% Speed) . . .	71



FIGURE		PAGE
96	Rotor Loss Coefficient vs Outlet Radius (102% Speed) . .	71
97	Rotor Deviation vs Outlet Radius (102% Speed) . . . . .	72
98	Stator Incidence vs Inlet Radius (102% Speed) . . . . .	73
99	Stator Mach Number vs Inlet Radius (102% Speed) . . . . .	74
100	Stator Loss Coefficient vs Outlet Radius (102% Speed). .	74
101	Stator Diffusion Factor vs Outlet Radius (102% Speed). .	74
102	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	75
103	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	75
104	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	75
105	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	75
106	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	76
107	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	76
108	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	77
109	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	77
110	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 40% Speed) . . . . .	77
111	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	78
112	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	78
113	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	78

FIGURE		PAGE
114	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	78
115	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	79
116	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	79
117	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	80
118	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	80
119	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 50% Speed) . . . . .	80
120	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	81
121	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	81
122	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	81
123	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	81
124	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	82
125	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	82
126	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	83
127	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	83
128	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 60% Speed) . . . . .	83
129	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	84

FIGURE		PAGE
130	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	84
131	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	84
132	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	84
133	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	85
134	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	85
135	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	86
136	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	86
137	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 70% Speed) . . . . .	86
138	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	87
139	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	87
140	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	87
141	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	87
142	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	88
143	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	88
144	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	89
145	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	89

FIGURE		PAGE
146	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 80% Speed) . . . . .	89
147	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	90
148	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	90
149	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	90
150	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	90
151	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	91
152	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	91
153	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	92
154	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	92
155	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 85% Speed) . . . . .	92
156	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	93
157	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	93
158	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	93
159	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	93
160	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	94
161	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	94

FIGURE		PAGE
162	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	95
163	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	95
164	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	95
165	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	96
166	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	96
167	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	96
168	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 90% Speed) . . . . .	96
169	Rotor Deviation vs Outlet Radius (Within-Blade Analysis, 95% Speed) . . . . .	97
170	Stator Incidence vs Inlet Radius (Within-Blade Analysis, 95% Speed) . . . . .	97
171	Stator Mach Number vs Inlet Radius (Within-Blade Analysis, 95% Speed) . . . . .	98
172	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 95% Speed) . . . . .	98
173	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 95% Speed) . . . . .	98
174	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 100% Speed) . . . . .	99
175	Rotor Incidence vs Inlet Radius (Within-Blade Analysis, 100% Speed) . . . . .	99
176	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 100% Speed) . . . . .	99
177	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 100% Speed) . . . . .	99



FIGURE		PAGE
178	Rotor Deviation vs Outlet Radius (Within- Blade Analysis, 100% Speed) . . . . .	100
179	Stator Incidence vs Inlet Radius (Within- Blade Analysis, 100% Speed). . . . .	100
180	Stator Mach Number vs Inlet Radius (Within- Blade Analysis, 100% Speed) . . . . .	101
181	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 100% Speed) . . . . .	101
182	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 100% Speed) . . . . .	101
183	Rotor Relative Mach Number vs Inlet Radius (Within-Blade Analysis, 102% Speed) . . . . .	102
184	Rotor Incidence vs Inlet Radius (Within- Blade Analysis, 102% Speed) . . . . .	102
185	Rotor Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 102% Speed) . . . . .	102
186	Rotor Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 102% Speed) . . . . .	102
187	Rotor Deviation vs Outlet Radius (Within- Blade Analysis, 102% Speed) . . . . .	103
188	Stator Incidence vs Inlet Radius (Within- Blade Analysis, 102% Speed) . . . . .	103
189	Stator Mach Number vs Inlet Radius (Within- Blade Analysis, 102% Speed) . . . . .	104
190	Stator Loss Coefficient vs Outlet Radius (Within-Blade Analysis, 102% Speed). . . . .	104
191	Stator Diffusion Factor vs Outlet Radius (Within-Blade Analysis, 102% Speed). . . . .	104
192	Axial Static Pressure Distribution (Within- Blade Analysis, 40% Speed) . . . . .	105
193	Axial Static Pressure Distribution (Within- Blade Analysis, 50% Speed) . . . . .	106

FIGURE		PAGE
194	Axial Static Pressure Distribution (Within-Blade Analysis, 60% Speed) . . . . .	107
195	Axial Static Pressure Distribution (Within-Blade Analysis, 70% Speed) . . . . .	108
196	Axial Static Pressure Distribution (Within-Blade Analysis, 80% Speed) . . . . .	109
197	Axial Static Pressure Distribution (Within-Blade Analysis, 85% Speed) . . . . .	110
198	Axial Static Pressure Distribution (Within-Blade Analysis, 90% Speed) . . . . .	111
199	Axial Static Pressure Distribution (Within-Blade Analysis, 95% Speed) . . . . .	112
200	Axial Static Pressure Distribution (Within-Blade Analysis, 100% Speed) . . . . .	113
201	Axial Static Pressure Distribution (Within-Blade Analysis, 102% Speed) . . . . .	114
202	Rotor Within-Blade Deviation Angle Distribution (40% Speed Point) . . . . .	115
203	Rotor Within-Blade Deviation Angle Distribution (50% Speed Point) . . . . .	116
204	Rotor Within-Blade Deviation Angle Distribution (60% Speed Point) . . . . .	117
205	Rotor Within-Blade Deviation Angle Distribution (70% Speed Point) . . . . .	118
206	Rotor Within-Blade Deviation Angle Distribution (80% Speed Point) . . . . .	119
207	Rotor Within-Blade Deviation Angle Distribution (85% Speed Point) . . . . .	120
208	Rotor Within-Blade Deviation Angle Distribution (90% Speed Point) . . . . .	121
209	Rotor Within-Blade Deviation Angle Distribution (95% Speed Point) . . . . .	122

FIGURE		PAGE
210	Rotor Within-Blade Deviation Angle Distribution (100% Speed Point) . . . . .	123
211	Rotor Within-Blade Deviation Angle Distribution (102% Speed Point) . . . . .	124
212	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 40% Speed) . . . . .	125
213	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 50% Speed) . . . . .	126
214	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 60% Speed) . . . . .	127
215	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 70% Speed) . . . . .	128
216	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 80% Speed) . . . . .	129
217	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 85% Speed) . . . . .	130
218	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 90% Speed) . . . . .	131
219	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 95% Speed) . . . . .	132
220	Stator Mid Span Surface Static Pressure Distribution (Within-Blade Analysis, 100% Speed) . . . . .	133
221	Stator Mid-Span Surface Static Pressure Distribution (Within-Blade Analysis, 102% Speed) . . . . .	134

FIGURE		PAGE
222	Rotor Mid-Radius Deviation vs Incidence Angle . .	135
223	Rotor Deviation Angle Distribution . . . . .	136
224	NACA Compressor Loss Correlation with ARL Configuration #2 Superimposed . . . . .	137

## SECTION I

### INTRODUCTION

This report presents the results of an experimental evaluation of the single stage, supersonic axial compressor described in Reference 1 and modified according to Reference 2. This compressor was designed for an over-all stage total pressure ratio of 3.06 to 1 at an isentropic efficiency of 81.5 percent. Design tip speed was 1600 ft/sec at standard conditions, and the inlet hub/tip radius ratio was 0.75. There were no inlet guide vanes. The modification described in Reference 2 consisted of redesign of the rotor to incorporate a "splitter vane" between each of the principal rotor airfoils. The splitter vane consisted of an airfoil located circumferentially mid-way in the downstream half of each rotor blade passage and extending full span.

The compressor tested was designed for diffusion levels beyond the range of past experience in both rotor and stator. This choice was deliberate in order to provide a suitable test bed for the evaluation of boundary layer control devices applicable to a compressor and to obtain data at values of Diffusion Factor above 0.5. The performance of the original design, reported in Reference 3, was extremely poor. The results reported herein, obtained after the addition of splitter vanes, represent a major improvement in both rotor and stage performance. The rotor performed relatively close to, although somewhat below, design goals. Stage performance was still significantly short of design objectives. No boundary layer control devices were installed for this test.

The second section of this report describes the test facility flow path, the compressor test vehicle, and the complete instrumentation system. Section III describes the procedures used in taking data and subsequently in reducing the data. The results of the test are presented in Section IV. Section V, the last section, summarizes the conclusions drawn from the data. Appendix A presents detailed aerodynamic results, including computing stations within blade rows, for the data point on each speed line corresponding to peak stage efficiency. *The rest of the Appendices provide sufficient data such that any reader wishing to process any data point not fully presented here, or wishing to process any data point differently, can, with the aid of References 6 and 7, completely reprocess the data or adapt the raw data to his own data reduction scheme.*



## SECTION II

### APPARATUS

#### 1. FACILITY FLOW PATH

The test facility used is of the open-loop variety. It is schematically shown in Figure 1. Air enters the facility through a filter designed to remove five micron particles with a 99.5 percent efficiency. The air then passes through a 30-inch duct to a Ball Flow Tube located about six pipe diameters downstream. About two pipe diameters further downstream, the air is turned 90 degrees with the aid of turning vanes and then passes through a perforated plate designed to reduce inlet pressure approximately three psi at 24 lb/sec flow at standard atmospheric conditions. Following this, the air passes through a tube bundle and subsequently enters a 48-inch diameter settling chamber. The settling chamber contains a perforated conical flow spreader and two screens patterned after the model investigation reported in Reference 4. From the settling chamber, air enters the compressor through a direct-coupled bellmouth. Air leaving the compressor is deflected radially outward to a peripheral throttle. The throttle consists of one stationary and one rotating cylindrical ring, each with 16 circumferentially distributed matching holes. Throttling takes place at a diameter of approximately 47 inches. Downstream of the throttle, the flow enters a collector, from which it is passed through a 24-inch duct to a silencer, and back to the atmosphere. A fast-acting poppet type valve, bypassing the throttle valve, is also available to relieve surge conditions. A cutaway drawing of the complete test facility is shown in Figure 2.

#### 2. COMPRESSOR TEST VEHICLE

A cross section of the research compressor is shown in Figure 3. The design employs a cantilevered rotor supported by four 0.5-inch thick bearing support struts with leading edges located about two stator chord lengths downstream of the stator trailing edge plane. The rotor tip diameter at the leading edge is nominally 18 inches. Oil seals are controlled gap carbon seals with an air barrier. No oil leakage into the flow path has ever been experienced. Cold rotor radial tip clearance with the rotor at rest is 0.037 to 0.039 inch. Hot clearance at design speed is predicted to be approximately 0.020 inch or about 0.6 percent of the mean rotor chord. The rotor shaft is mounted on ball bearings. Radial runout does not exceed 0.0005 inch. The bulletnose and inlet hub flow path are supported by six bi-convex struts in the inlet. The flow area contraction ratio between the trailing edge plane of the struts and the leading edge plane of the rotor is 2.72 to 1. Surface finish on all surfaces adjacent to the flow upstream of the bearing support struts is 32 microinches or better. An abrasible coating has been employed in the casing adjacent to the rotor tip. However, no rubs have been experienced, even in stall. The rotor is of integral construction, the blades and disc being machined from a single forging

of 6Al-4V titanium. The stator blades are individually inserted but are machined integrally with platforms at hub and tip. The gap between adjacent platforms lies in the range of 0 to 0.002 inch. A photograph of the rotor is shown in Figure 4.

### 3. COMPRESSOR INSTRUMENTATION

Aerodynamic instrumentation in the compressor consists of measuring points in stator leading edges for total pressure and temperature, rakes downstream of the stators for total pressure and temperature, a large number of static pressure taps distributed on the inner and outer flow path and on the surface of one pair of stator blades, and dynamic wall pressure measurements made over the rotor tip. Measurements of inlet total pressure and temperature, mass flow, relative humidity, and rotor speed are accomplished outside of the compressor and are discussed in paragraph 4 of Section II. The Supersonic Compressor research vehicle has a total of 133 sensors measuring aerodynamic parameters at various points throughout the stage. Refer to Figure 3 and Table 1 for specific locations. Some of the static pressures are sensed at more than one point and are manifolded to become, in each case, a single measurement. Figure 5 shows the vehicle instrumentation bulkhead.

#### a. Temperature Measurements

##### (1) Location

A total of thirty-nine Chromel-Alumel thermocouples are used to sense temperature. Four are mounted in the plenum, ten are mounted in the vane leading edges, and twenty-five are located in the five discharge plane rakes. The vane leading edge and the rake mounted thermocouples are of the slot vented probe type (Figures 6, 9a., and 10). A detailed analysis of the features of the slot vented design, along with recovery factor characteristics, may be found in Reference 5. The rakes were designed with the sensors dividing the discharge annulus into equal radial increments while circumferential spacing is on divisions equal to 2.2 times the distance between vane trailing edges. In Figure 3, the discharge plane drawing is in error. The temperature rake shown at 209° 31' should be located at 211° 33'.

The ten stator leading edge thermocouple probes are mounted on four vanes with two vanes having two thermocouples and two vanes having three thermocouples. As with the discharge rakes, these probes are also spaced to divide radially the stator annulus into five equal increments; however, in this case with two sensors per radius.

##### (2) Calibration

All thermocouples were fabricated from individually insulated, single coils of Chromel and Alumel wire. Samples were taken periodically along the coils as the thermocouples were made for vehicle installation. These sample thermocouples were calibrated against a model 162 platinum resistance bulb primary standard manufactured by

Rosemount Engineering Company. A constant temperature oil bath, made by lauda Division of Brinkman Instruments, Inc. was used as the heat medium. The bath was set at four different temperatures within the range of interest. The results, indicated in Table 2, show a worst case error of plus or minus 0.5°F at the highest temperature.

With thermocouple calibrated as indicated, the entire electronic system employed to record temperature data was examined. The results are shown in Table 3. Taking the worst case error, at the highest temperature, for both the thermocouples and readout system yields a maximum error of plus or minus 0.9°F. The more realistic RSS error goes from 0.23°F at 150 degrees to 0.65°F at 350 degrees. Finally, when recovery factor variation is added, the RSS error at 350°F becomes plus or minus 1.0°F. Figure 7 depicts the equipment used in the calibrations.

#### b. Pressure Measurements

##### (1) Location

Thirty-five static (PS) and thirty-five total (PT) pressures are measured in the vehicle flowpath. Twenty-five of the static taps are distributed at various points on the compressor flowpath liners. In particular, ten of these are located over the rotor blade tip, starting at 0.25 inch axially forward of the leading edge and following at 0.25 inch axial intervals extending downstream. A further ten statics are located approximately mid-chord radially on two vanes with seven suction side taps on one vane and three pressure side taps on the other.

The ten vane mounted total pressure probes are of the Kiel stagnation tube design (Figure 8) and are mounted with two sensors on each of two vanes and three on each of two other vanes. All are radially located to divide the annulus into five equal parts, with two measurements per radius. The other twenty-five are impact tubes mounted as five radial rakes of five sensors each, dividing the discharge annulus into equal increments which are circumferentially spaced in a manner similar to that of the temperature rakes. An impact pressure rake is shown in Figure 9.b.

Located for use in conjunction with the static taps placed over the rotor blade tips are eight Kistler Model Number 603A pressure transducers and a Bentley Model 316 proximity detector. Because of problems observed at high speed with the Kistler dynamic pressure data, no further mention will be made of this system.

##### (2) Calibration

Four Statham strain gage type transducers are used to convert the various pressures into electrical signals for processing through readout and recording. One transducer is located in each of four, forty-eight port Scanivalve sequential pressure switching devices. The

pressures to be sampled are connected to odd numbered ports while moderate vacuum is applied to all even (Roughing) ports to minimize hysteresis effects.

Three calibration pressures are sensed by all four Scanivalves on every scan. These are barometric, 15 PSIG and 30 PSIG. The 15 and 30 PSIG standards are supplied by Ametek Model PK-30 self-regulating, primary deadweight type, pressure standards referred to atmosphere. The computer software used for data reduction corrects these two gauge values against variation in local barometric pressure and creates a new transducer calibration curve for every scan. Two absolute calibration pressures have been added to this system for use in future tests, and the barometric calibration pressure has been eliminated.

#### c. Readout Electronics

Data are collected and recorded through use of a Hewlett Packard 2012B Data Acquisition System (DAS). This system is comprised of a 2911 guarded crossbar scanner, 2547A coupler, 2402A integrating digital voltmeter, 5050B digital recorder, and a Kennedy 1506 incremental tape recorder.

As previously stated, pressure measurements are routed through four Scanivalve units using Stathan transducers for conversion into electronic signals. A "Scanivalve" offers the advantage of using the same transducer to measure many pressures and lends itself to on-line calibration as described above. An interface unit was built to program the Scanivalves, along with other parameters, into the HP DAS in a manner which minimizes scanning time without compromising transducer settling time. Instead of sampling the same port on all valves sequentially before stepping to the next port, the digital interface causes each valve to move through its next roughing port to its next data point immediately after being interrogated. Each transducer then has an opportunity to settle out at its next test pressure while two others are sequentially interrogated. This sequence is repeated until all ports are sampled. Approximately six seconds lapse for the entire procedure.

Thermocouple outputs are routed through a Kaye Instruments' Model K179 electronic ice point reference into the interface unit and then to the HP DAS.

### 4. TEST FACILITY INSTRUMENTATION

#### a. Rotor Speed

A Bentley Model 306 transducer senses six grooves machined into the gearbox/rotor driveshaft coupling. The output is fed into a Model 3115 proximator for signal conditioning. The proximator signal is a train of pulses having a repetition rate corresponding to rotor RPM/10. This

repetition rate is directly recorded by the HP DAS. A Bently Model 5030 digital tachometer provides a visual indication of rotor speed accurate to ten RPM. The Tachometer also includes an adjustable speed limiting switch as a safety feature.

b. Mass Flow

Inlet pressure is metered through a product series 122 Dall tube venturi manufactured by B.I.F. Industries with a 12.687-inch throat. Metering accuracy has been calibrated to plus or minus one-half percent by the manufacturer. Static pressure taps are located both in the throat and in the inlet cavity.

c. Inlet (Plenum) Total Pressure and Temperature

Compressor inlet total pressure is assumed equal to plenum static pressure just downstream of the last screen. Four static taps are manifolded into one pressure and recorded on two separate Scanivalves. The Maximum error associated with this assumption is 0.06 percent. Temperature is sensed by four bare junction thermocouples located in the same axial plane as the pressure taps, and supported on two crossed cables.

d. Analog Compressor Mapping

An on-line plot of stage pressure ratio vs pseudo mass flow was effected through use of a Mosely Model 2FRA X-Y plotter. Teledyne pressure transducers were used to sense stage inlet P01, stage exit P03 from a mid-radius stagnation tube and hub P1 (measured 0.25 inch upstream of the rotor). Operational amplifiers were used to ratio exit P03 to inlet P01 and also to ratio hub P1 to inlet P01. Stage pressure ratio was used to excite the Y-axis while  $1 - (P1/P01)$  was sent to the X-axis. The approximate compressor map so obtained was used to select a reasonable distribution of throttle settings at which to record detailed data.

e. Relative Humidity

A Foxboro Dewcel Model 2711TG-K222 was mounted in the inlet stack to monitor humidity. This device continuously measures the moisture content of the air by sensing the temperature at which the partial pressure of its water vapor is equal to the water vapor pressure of a saturated salt solution. The humidity information is acquired by the DAS as a thermocouple reading on every test run and subsequently treated in the Phase I data reduction program.

## SECTION III

### TEST PROCEDURE AND DATA REDUCTION

#### 1. TEST PROCEDURE

Test data were taken in order of increasing speed, with each speed-line being entirely probed before any data at higher speed were acquired. The on-line analog x-y plot capability discussed in paragraph 4.d. of Section II was used to select the test points, since on-line data reduction was not available.

For each speedline, test data were first acquired at a partially-closed exhaust throttle settling, after which the compressor was gradually throttled to include stall. After recovery, data were taken at several points as the throttle was opened from near-stall to wide-open. Stall was indicated by two sources: the dynamic pressure sensors across the rotor tip, which were displayed on oscilloscopes on the test operator's console, and a microphone in the plenum. Sudden oscillations of the above-mentioned x-y plotter were further indicators that stall had occurred.

Data were acquired at the rate of about one speedline per hour. On dates when elevated speed lines were investigated, a single test point at each of several lower speeds was taken to assure data integrity by comparison to previously acquired data at these lower speeds.

Prior to each test, an atmospheric pressure reading was obtained from a mercury barometer at the test site. The rig was initially brought up to speed and then monitored for about ten minutes, when it was assumed equilibrium had been reached. A five-minute dwell at each throttle setting was observed prior to data acquisition. Two data scans were acquired per test point on each speedline.

A 12-character test identification number was manually assigned to each test point and acquired by the DAS as the first item of information during data acquisition at that point (character 1: last digit of year; characters 2-3: numerical month; characters 4-5: numerical day of month; characters 6-7: test point number on that particular date; characters 8-10: numerical throttle setting; characters 11-12: last two digits of the nominal percent-speed (e.g., 85% = 85; 100% = 00)). Where two scans were taken at a particular test point automatically each scan bears the same test identification number.

Finally, a listing of all raw experimental data which were acquired during testing of this stage is provided in Appendix D, and all computer input data used for Phases I and II of the data reduction are provided in Appendix B.

## 2. DATA REDUCTION - PHASE I

Phase I reduction of the test data was accomplished by using a slightly modified version of the computer program described in Reference 6. The modifications are subsequently described in Reference 3.

In Reference 6, Equation (11) is in error and should be expressed as follows:

$$W = C1 \cdot \frac{CQ \ Y \ d^2 \ F}{\sqrt{1 - \beta^4}} \sqrt{h(\gamma_a + \gamma_v)}$$

No change, however, is required to the actual computer coding of the original program.

## 3. DATA REDUCTION - PHASE II

Phase II reduction of the test data was accomplished by using the computer program described in Reference 7.

To aid in the calculation procedure of the within blade analysis, a CALCOMP plotting routine labeled DEVPLOT was developed to allow better visualization of the deviation angles at each rotor computing station and hub, mid, and tip streamlines. The DEVPLOT input values used are the final deviation angles determined during a within blade calculation. The values are given as a function of normalized axial distance. A complete listing of this program is given in Appendix C1.

In addition to the DEVPLOT routine, a second CALCOMP plotting routine was utilized to plot the stator mid-span surface static pressure distribution for each within blade analysis. This program is labeled STAPLOT and uses the experimental readings of the seven suction surface static taps and the three pressure surface static taps (located on the mid-span of the instrumented stator blades) as input values. Extrapolated static pressure values for the stator leading and trailing edges are also input to the plotting routine. These values are based on the radial location of the first and last suction surface static taps and the leading and trailing edge calculated values of static pressure determined by the within blade analysis. A complete listing of this program is given in Appendix C2.

## SECTION IV

### RESULTS

#### 1. OVER-ALL PERFORMANCE

The mass-averaged performance of the rotor and of the complete compressor stage is tabulated in Table 4 and plotted in Figure 12. The performance shown is a major improvement over the original configuration tested (without rotor splitter vanes) and reported in Reference 3. At 100 percent design corrected speed, corrected flow was approximately 12 percent low, rotor efficiency was 5 points low, stage efficiency was 14 points low, rotor total pressure ratio peaked at 3.47 versus a design value of 3.35, and stage total pressure ratio peaked at 2.77 versus 3.06, respectively. The compressor was throttled to stall at each corrected speed shown on the map. The data point nearest stall was taken at a throttle opening approximately 0.5 percent further open than the setting which precipitated stall. This change in throttle area is equivalent to about 0.9 percent of the annulus area at the rotor inlet.

#### 2. BLADE-ELEMENT PERFORMANCE (ACROSS BLADE)

The radial distributions of relative inlet Mach number, incidence angle, loss coefficient, deviation angle, and diffusion factor for both rotor and stator are presented in Figures 13 through 82, using Tables 5-11, for each data point shown on the compressor map. One set of these five radial distributions is presented for each blade row at each corrected speed. In each of these sets, the distributions for all throttle settings are superimposed on each respective plot. As described earlier in Section III, this data was reduced using the full radial equilibrium equation with the equations of momentum, continuity, etc. satisfied at each computing station for each streamline. This data, also used for the compressor map, was reduced with computing stations only at blade-row edges and in free spaces; there were no computing stations internal to blade rows.

#### 3. BLADE-ELEMENT PERFORMANCE (WITHIN BLADE)

The data point nearest maximum stage efficiency for each operating speed was selected for more detailed analysis. The more detailed analysis involved the introduction of four additional computing stations within the rotor. The data reduction was then accomplished in the same manner as before, with blockages and deviation angles internal to the rotor adjusted so that the calculated and measured static pressures along the casing adjacent to the rotor tip were as nearly coincident as possible. The results of these analyses include plots of the radial



distribution of the same five parameters for rotor and stator described in the preceding paragraph (Figures 102 through 191), plots of the experimental (rotor only) and calculated axial distribution of static pressure at hub, mean, and case (Figures 192 through 201), corresponding plots of the distribution of deviation angle within the rotor blade row (Figures 202 through 211), plots of the surface distributions of static pressure for a mid-span section of the stator (Figures 212 through 221), and a complete aerodynamic description at each computing station - streamline intersection (Appendix A).

#### .. ROTOR TIP DYNAMIC PRESSURE MEASUREMENTS

The dynamic distribution of static pressure over the rotor tips was observed during operation to assess qualitatively flow stability during the test. In general, the flow appeared much more stable at the higher speeds than was the case with the previous compressor configuration reported in Reference 3. Also, as design speed was approached, the dynamic pressure signal measured 0.25 inch upstream of the rotor became very weak, indicating that the passage shock had probably been swallowed. A few bursts of these data were recorded on wide-band FM magnetic tape. However, no further processing of these data was attempted since at no time during the course of these tests were all elements of the dynamic pressure recording system working satisfactorily simultaneously.

## SECTION V

### CONCLUSIONS

The major conclusion drawn from the reported tests was that splitter vanes added to the axial compressor rotor accomplished their intended purpose of controlling rotor deviation angles at off-design, high incidence operating conditions with a satisfactory level of total pressure losses. Furthermore, operation of the compressor was now close enough to its design point that it appeared feasible to embark upon the series of boundary-layer-control modifications originally envisioned to assess their potential usefulness in this type of environment.

The dramatic decrease achieved in deviation angle is best seen by referring to Figures 222 and 223. The first of these figures presents deviation angle at the rotor trailing edge mid-radius location versus rotor incidence at mid-radius on the leading edge for the original rotor as presented in Reference 3 and also for the new rotor. Whereas a definite trend was apparent for the original rotor, all data points for the new rotor fall in a cluster, exhibiting no apparent sensitivity to incidence angle. The single data point shown for each corrected speed corresponds to operation at peak stage efficiency for each respective speed. The second of these figures compares the design radial distribution of deviation angle with distributions measured at design speed for the first and second rotor configurations. Whereas deviation angles measured with the first rotor remained well above design values all along the span, deviation angles recorded for the second rotor remained substantially lower than design values over most of the span. Only locally near the tip was deviation observed to rise rapidly above the design level. This might be due to boundary layer separation on the outer casing. It might also be due to rotor boundary layer and wake fluid, rotating at near blade speed, being centrifuged outward and collecting at the outer casing.

In order to assess the loss characteristics of the rotor, it was necessary to divide the measured total losses into diffusion losses and shock losses. Reference 8 presents the results of a cascade test of a blade section corresponding to streamsurface No. 10 in the design calculations of Reference 1, with splitter vanes added. At design-point operating conditions, static pressure along the suction surface of the principal airfoils was seen to be nearly constant at the undisturbed free-stream value up to the shock impingement point indicating that neither precompression nor expansion has occurred upstream of the passage shock wave. Consequently, since the compressor stage passed only about 88 percent of design flow, the suction surface Mach number just upstream of the shock wave was assumed

to be increased above the free stream relative value by an amount equal to a Prandtl-Meyer expansion from the relative free stream Mach number through an angle equal to the difference between actual operating incidence and design incidence. Shock loss was then presumed equal to the total pressure loss through a normal shock having an upstream Mach number equal to the average of the relative free stream and section surface Mach numbers on any streamsurface. Interpolating between stream-surfaces, these computations were performed for blade sections at 10, 50 and 90 percent span. Shock loss was subtracted from the total loss measured at the same location, and the result was plotted in the form of Total Pressure Loss Parameter versus Diffusion Factor in Figure 224. Blade solidity was presumed equal to the sum of principal blade chord plus splitter vane chord divided by the mean circumferential spacing between principal blade sections. Shown in this same figure are curves derived from Reference 9 and the extrapolation made for design purposes and presented in Reference 1. The interesting conclusion drawn from this figure is that at Diffusion Factors below 0.6, where there is extensive data, the blade section including splitter vanes performs exactly as would be expected, upon taking the increased solidity into account. However, at Diffusion Factors substantially above 0.6, the blade section with splitter vanes continues to perform satisfactorily and with losses lower than expected.

Consequently, the application of splitter vanes to axial compressor blade rows has potential for configurations combining relatively low aspect ratio with high aerodynamic loading. They should be suitable for stationary as well as rotating blade rows. They may also be suitable for fully subsonic blade sections as well as supersonic sections for which the concept was demonstrated. Although the rotor performance reported herein was good, the data of Reference 8 indicate that the splitter vane design was not optimum. The simple approach used for this splitter vane design, which consisted of duplicating the camber line of the principal airfoils and locating the splitter vane in mid-channel, resulted in very poor pressure distributions around the splitter vane, including re-expansion to supersonic Mach numbers according to Reference 8. It appears that a splitter vane carefully designed in the cascade plane might produce much lower losses than reported herein.

TABLE I  
INSTRUMENTATION LIST

ITEM NUMBER	TYPE SENSOR	LOCATION			REMARKS
		AXIAL	RADIAL	CIRCUMFERENTIAL	
057	T/C	6.181	7.800	36° 48'	Disch. Rake Element
058	T/C				Humidity
059	T/C				(Not In Use)
060	T/C			45°	Plenum
061	T/C			135°	Plenum
062	T/C			225°	Plenum
063	T/C			315°	Plenum
064	T/C	LE	8.371	Vane 22	Leading Edge
065	T/C	LE	8.371	Vane 42	Leading Edge
066	T/C	LE	8.251	Vane 24	Leading Edge
067	T/C	LE	8.251	Vane 44	Leading Edge
068	T/C	LE	8.121	Vane 22	Leading Edge
069	T/C	LE	8.121	Vane 42	Leading Edge
070	T/C	LE	8.001	Vane 24	Leading Edge
071	T/C	LE	8.001	Vane 44	Leading Edge
072	T/C	LE	7.871	Vane 22	Leading Edge
073	T/C	LE	7.871	Vane 42	Leading Edge
074	T/C	6.181	8.440	4° 28'	Disch. Rake Element
075	T/C	6.181	8.440	36° 48'	Disch. Rake Element
076	T/C	6.181	8.440	69° 7'	Disch. Rake Element
077	T/C	6.181	8.440	211° 33'	Disch. Rake Element
078	T/C	6.181	8.440	243° 58'	Disch. Rake Element
079	T/C	6.181	8.280	4° 28'	Disch. Rake Element
080	T/C	6.181	8.280	36° 48'	Disch. Rake Element
081	T/C	6.181	8.280	69° 7'	Disch. Rake Element
082	T/C	6.181	8.280	211° 33'	Disch. Rake Element
083	T/C	6.181	8.280	243° 58'	Disch. Rake Element
084	T/C	6.181	8.120	4° 28'	Disch. Rake Element
085	T/C	6.181	8.120	36° 48'	Disch. Rake Element
086	T/C	6.181	8.120	69° 7'	Disch. Rake Element
087	T/C	6.181	8.120	211° 33'	Disch. Rake Element
088	T/C	6.181	8.120	243° 58'	Disch. Rake Element
089	T/C	6.181	7.960	4° 28'	Disch. Rake Element
090	T/C	6.181	7.960	36° 48'	Disch. Rake Element
091	T/C	6.181	7.960	69° 7'	Disch. Rake Element
092	T/C	6.181	7.960	211° 33'	Disch. Rake Element
093	T/C	6.181	7.960	243° 58'	Disch. Rake Element
094	T/C	6.181	7.800	4° 28'	Disch. Rake Element
095					
096	T/C	6.181	7.800	69° 7'	Disch. Rake Element
097	T/C	6.181	7.800	211° 33'	Disch. Rake Element
098	T/C	6.181	7.800	243° 58'	Disch. Rake Element

TABLE I (continued)

ITEM NUMBER	TYPE SENSOR	LOCATION			REMARKS
		AXIAL	RADIAL	CIRCUMFERENTIAL	
101	Atmos				Barometric Pressure
103	PS				Venturi Throat
105	PS				Venturi Cavity
107	PT				Plenum
109	PS	-0.25	ID	315°	Casing (Same as 751)
111	PS	-0.25	OD	315°	Casing
113	PS	0.00	OD	306°	Casing
115	PS	0.25	OD	294°	Casing
117	PS	0.50	OD	180°	Casing
119	PS	0.75	OD	190°	Casing
121	PS	1.00	OD	310°	Casing
123	PS	1.25	OD	170°	Casing
125	PS	1.50	OD	290°	Casing
127	PS	1.75	OD	301°	Casing
129	PS	2.00	OD	160°	Casing
131	PS	3.227	8.163	Vane 16	Suction Side Vane
133	PS	3.393	8.175	Vane 16	Suction Side Vane
135	PS	3.361	8.184	Vane 16	Suction Side Vane
137	PS	3.837	8.190	Vane 16	Suction Side Vane
139	PS	4.115	8.191	Vane 16	Suction Side Vane
141	Ref.				Not Used
143	Ref.				Atmos.
145	Ref.				15 PSIG Reference
147	Ref.				30 PSIG Reference
201	Atmos				Barometric Pressure
203	PS				Same as 103
205	PS				Same as 105
207	PT				Same as 107 and 752
209	PS	4.281	8.192	Vane 16	Suction Side Vane
211	PS	4.559	8.194	Vane 16	Suction Side Vane
213	PS	-2.00	ID	45° & 135°	Two Manifoldded Taps
215	PS	-2.00	ID	225° & 315°	Two Manifoldded Taps
217	PS	-2.00	OD	45° & 135°	Two Manifoldded Taps
219	PS	-2.00	OD	225° & 315°	Two Manifoldded Taps
221	PS	2.25	OD	Vanes 18, 22, 40 & 44	Four Manif. Taps
223	PS	2.25	ID	113.5°, 156.5° 290.5° & 334.5°	Four Manif. Taps
225	PS	6.181	OD	60°	Casing
227	PS	6.181	OD	120°	Casing
229	PS	6.181	OD	252°	Casing
231	PS	6.181	OD	300°	Casing
233	PS	6.181	ID	60°	Casing
235	PS	6.181	ID	120°	Casing
237	PS	6.181	ID	252°	Casing
239	PS	6.181	ID	300°	Casing

TABLE I (continued)

ITEM NUMBER	TYPE SENSOR	LOCATION			REMARKS
		AXIAL	RADIAL	(INCIDENTIAL)	
241	Ref.				Not Used
243	Ref.				Atmos.
245	Ref.				15 PSIG Reference
247	Ref.				90 PSIG Reference
301					Not Used
303					Not Used
305	PS	3.393	8.175	Vane 17	Pres. Side of Vane
307	PS	3.837	8.189	Vane 17	Pres. Side of Vane
309	PS	4.281	8.191	Vane 17	Pres. Side of Vane
311	PT	LE	8.371	Vane 20	Leading Edge
313	PT	LE	8.371	Vane 40	Leading Edge
315	PT	LE	8.251	Vane 38	Leading Edge
317	PT	LE	8.251	Vane 47	Leading Edge
319	PT	LE	8.121	Vane 20	Leading Edge
321	PT	LE	8.121	Vane 40	Leading Edge
323	PT	LE	8.001	Vane 18	Leading Edge
325	PT	LE	8.001	Vane 47	Leading Edge
327	PT	LE	7.871	Vane 20	Leading Edge
329	PT	LE	7.871	Vane 40	Leading Edge
331	PT	6.181	7.800	20° 47'	Disch. Rake Element
333	PT	6.181	7.800	52° 57'	Disch. Rake Element
335	PT	6.181	7.800	195° 29'	Disch. Rake Element
337	PT	6.181	7.800	227° 49'	Disch. Rake Element
339	PT	6.181	7.800	260° 8'	Disch. Rake Element
341	Ref.				Not Used
343	Ref.				Atmos.
345	Ref.				15 PSIG Reference
347	Ref.				90 PSIG Reference
401	PT	6.181	7.960	20° 47'	Disch. Rake Element
403	PT	6.181	7.760	52° 57'	Disch. Rake Element
405	PT	6.181	7.960	195° 29'	Disch. Rake Element
407	PT	6.181	7.960	227° 49'	Disch. Rake Element
409	PT	6.181	7.960	260° 8'	Disch. Rake Element
411	PT	6.181	8.120	20° 47'	Disch. Rake Element
413	PT	6.181	8.120	52° 57'	Disch. Rake Element
415	PT	6.181	8.120	195° 29'	Disch. Rake Element
417	PT	6.181	8.120	227° 49'	Disch. Rake Element
419	PT	6.181	8.120	260° 8'	Disch. Rake Element
421	PT	6.181	8.280	20° 47'	Disch. Rake Element
423	PT	6.181	8.280	52° 57'	Disch. Rake Element
425	PT	6.181	8.280	195° 29'	Disch. Rake Element
427	PT	6.181	8.280	227° 49'	Disch. Rake Element
429	PT	6.181	8.280	260° 8'	Disch. Rake Element
431	PT	6.181	8.440	20° 47'	Disch. Rake Element
433	PT	6.181	8.440	52° 57'	Disch. Rake Element

TABLE I (concluded)

[illegible]

TABLE II

## CALIBRATION OF SAMPLE THERMOCOUPLES

BATH SET PT. °C <sup>A</sup>	°F <sup>B</sup>	AVG. OF 9 SAMPLES °F	MAX. SPREAD ± °F
65	148.1	148.4	0.1
100	211.4	210.9	0.1
150	300.8	301.4	0.4
175	346.5	346.4	0.5

A Oil Bath Set Pt.

B Mueller bridge readout converted to temperature.

TABLE III

## CALIBRATION OF TEMPERATURE READOUT ELECTRONICS

SET PT. Avg <sup>+</sup> °F	PRINTER OUTPUT Avg <sup>+</sup> °F	MAX. SPREAD ± °F
148.2	148.3	0.2
210.7	210.7	0.2
301.7	301.7	0.3
345.4	345.5	0.4

+ Average of two calibrated T/C's.

\* Average of eight channels.



### TABLE IV

Yat I.O.	rpm	FLW (L/SEC)	----- PRESSURE RATIO -----	----- EFFICIENCY -----	----- STAGE PRESSURE RATIO -----	----- EFFICIENCY -----
212070109300	172.8	11.050	1.2311	.9330	1.1068	.7540
212070121000	175.4	11.220	1.2391	.9190	1.2150	.8340
212070131000	178.2	11.220	1.2501	.9070	1.2330	.8630
212070141000	181.7	9.460	1.2551	.8760	1.2300	.8230
212070151000	184.5	9.910	1.2591	.8600	1.2340	.7970
212070161000	187.3	9.620	1.2551	.8550	1.2340	.7880
212070171000	191.0	13.090	1.4031	.9100	1.3710	.8350
212070181000	191.2	12.310	1.4160	.8500	1.3840	.8290
212070191000	191.3	11.260	1.4160	.8680	1.3010	.8020
212070201000	191.4	13.170	1.4100	.9100	1.3720	.8340
212070211000	191.5	13.450	1.4341	.9210	1.3510	.8130
212070221000	191.6	13.790	1.4391	.9250	1.3020	.7820
212070231000	191.7	15.090	1.4391	.9310	1.5400	.7550
212070241000	191.8	15.600	1.6341	.9310	1.4910	.7350
212070251000	191.9	15.630	1.6291	.9100	1.4400	.6680
212070261000	192.0	15.610	1.6401	.9010	1.5690	.8160
212070271000	192.1	14.670	1.6131	.8600	1.5770	.8060
212070281000	192.2	15.870	1.6171	.9620	1.5730	.7070
212070291000	192.3	17.000	1.9131	.8300	1.7230	.7320
212070301000	192.4	17.000	1.9130	.8800	1.7010	.7110
212070311000	192.5	17.600	1.9130	.9390	1.7230	.7310
212070321000	192.6	17.420	1.9201	.9650	1.7840	.7770
212070331000	192.7	17.270	1.9211	.9340	1.8040	.7920
212070341000	192.8	18.710	1.9161	.8690	1.8100	.7840
212070351000	192.9	19.900	2.2771	.8790	1.9640	.7060
212070361000	193.0	14.870	2.2161	.8750	1.9620	.7010
212070371000	193.1	14.730	2.2791	.9750	2.0080	.7270
212070381000	193.2	14.630	2.2751	.8740	2.0520	.7530
212070391000	193.3	20.729	2.4731	.8672	2.1497	.7137
212070401000	193.4	20.501	2.4811	.8662	2.1865	.7317
212070411000	193.5	21.033	2.4792	.8094	2.1000	.6932
212070421000	193.6	20.700	2.4731	.8690	2.1239	.7066
212070431000	193.7	21.500	2.6551	.8460	2.2860	.6890
212070441000	193.8	21.800	2.6551	.9460	2.3060	.6980
212070451000	193.9	21.750	2.6570	.8450	2.3240	.7030
212070461000	194.0	21.830	2.6561	.9470	2.2560	.6730
212070471000	194.1	23.600	2.9531	.8450	2.4270	.6610
212070481000	194.2	23.900	2.9571	.8450	2.4530	.6730
212070491000	194.3	23.700	2.9571	.8430	2.4920	.6820
212070501000	194.4	23.559	3.3521	.8441	2.6994	.6709
212070511000	194.5	25.633	3.3411	.9427	2.7076	.6737
212070521000	194.6	25.757	3.3411	.8456	2.6445	.6568
212070531000	194.7	26.001	3.3411	.8458	2.6820	.6652
212070541000	194.8	26.401	3.3411	.8455	2.7410	.6603
212070551000	194.9	26.208	3.4711	.8429	2.7731	.6680

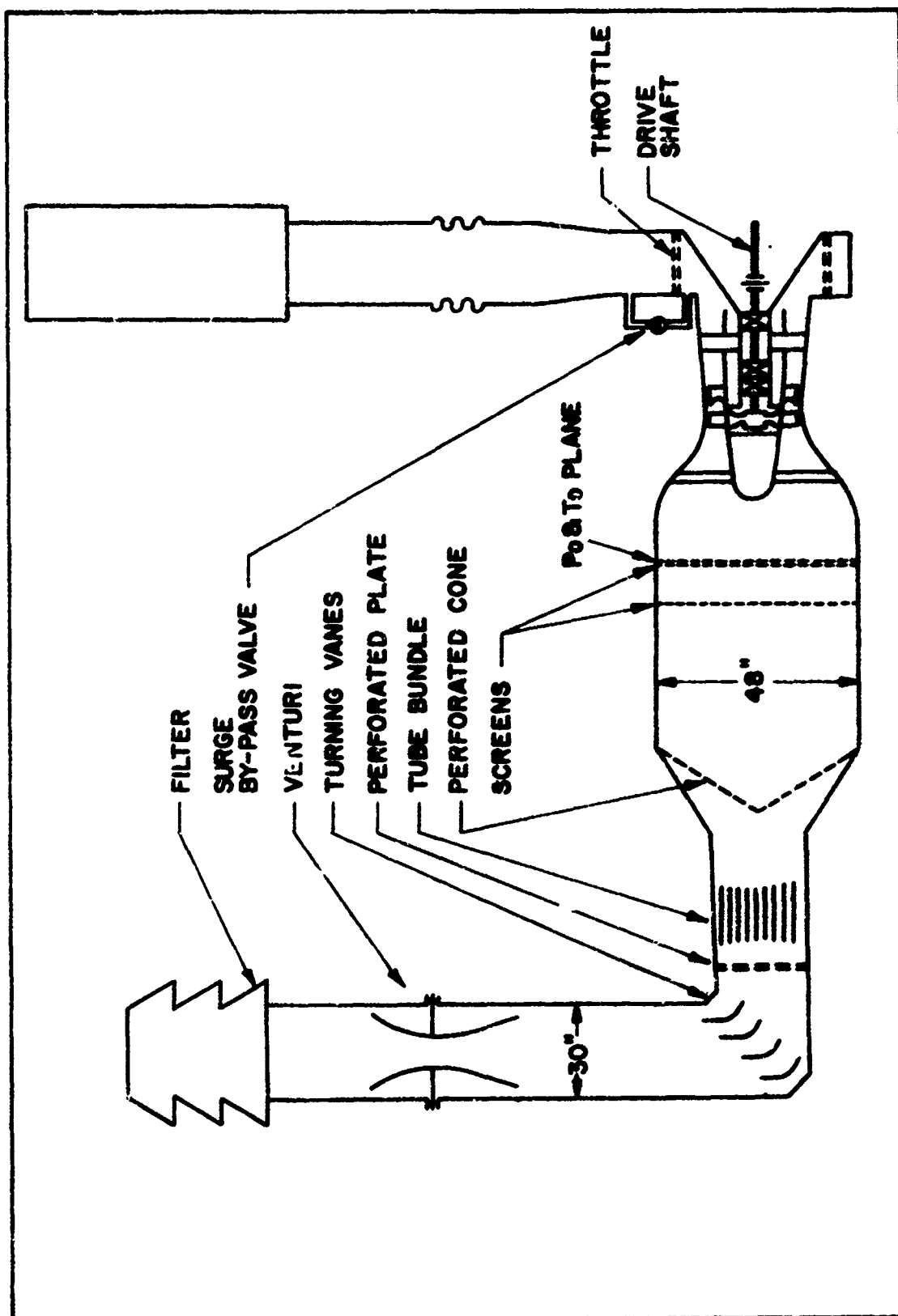
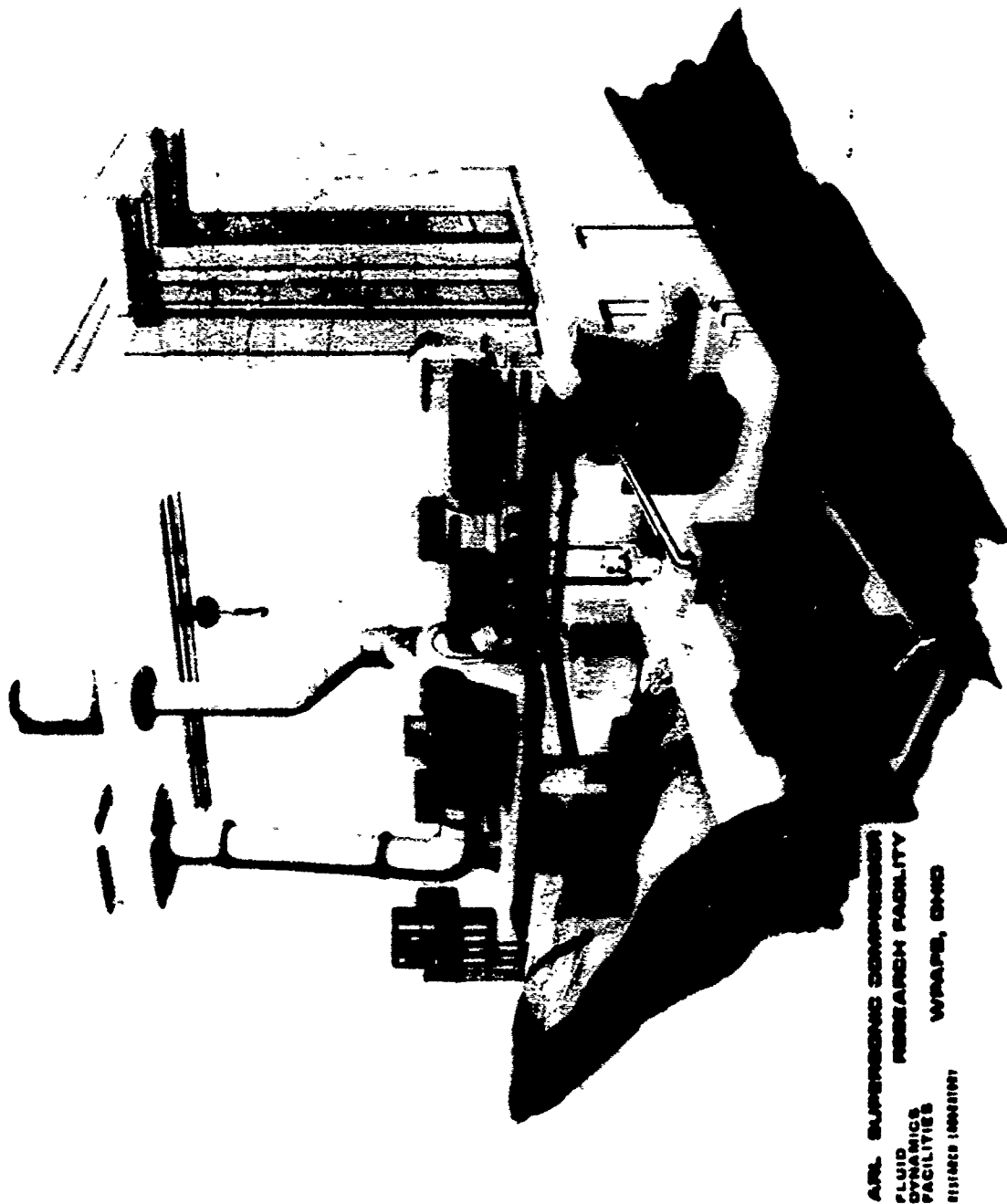
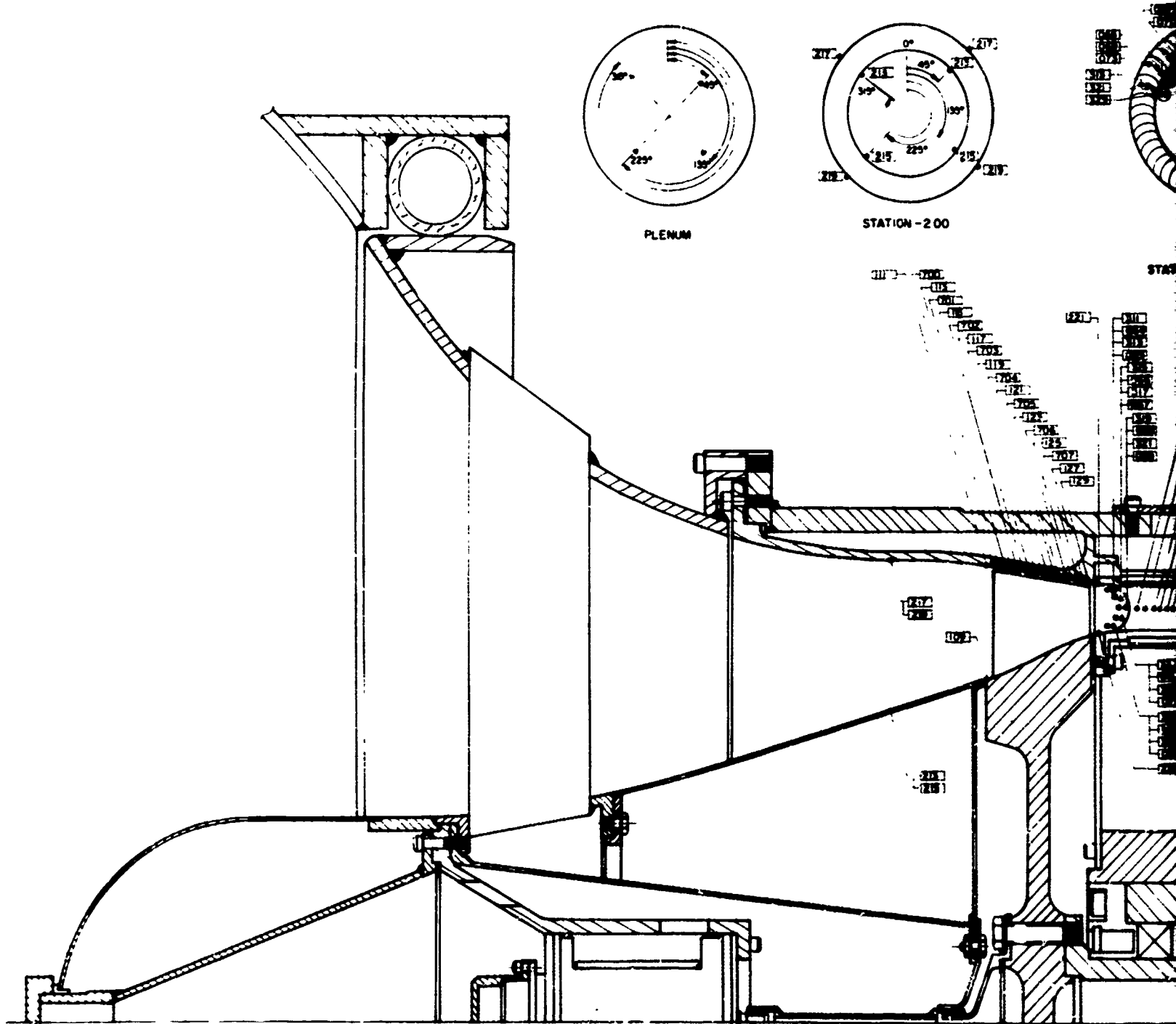


FIGURE 1. COMPRESSOR FACILITY FLOW PATH



ARL SUPERSONIC COMPRESSOR  
FLUID DYNAMICS RESEARCH FACILITY  
FACILITIES WPAFB, OHIO  
DISTRICT 100000000

FIGURE 2. TEST FACILITY



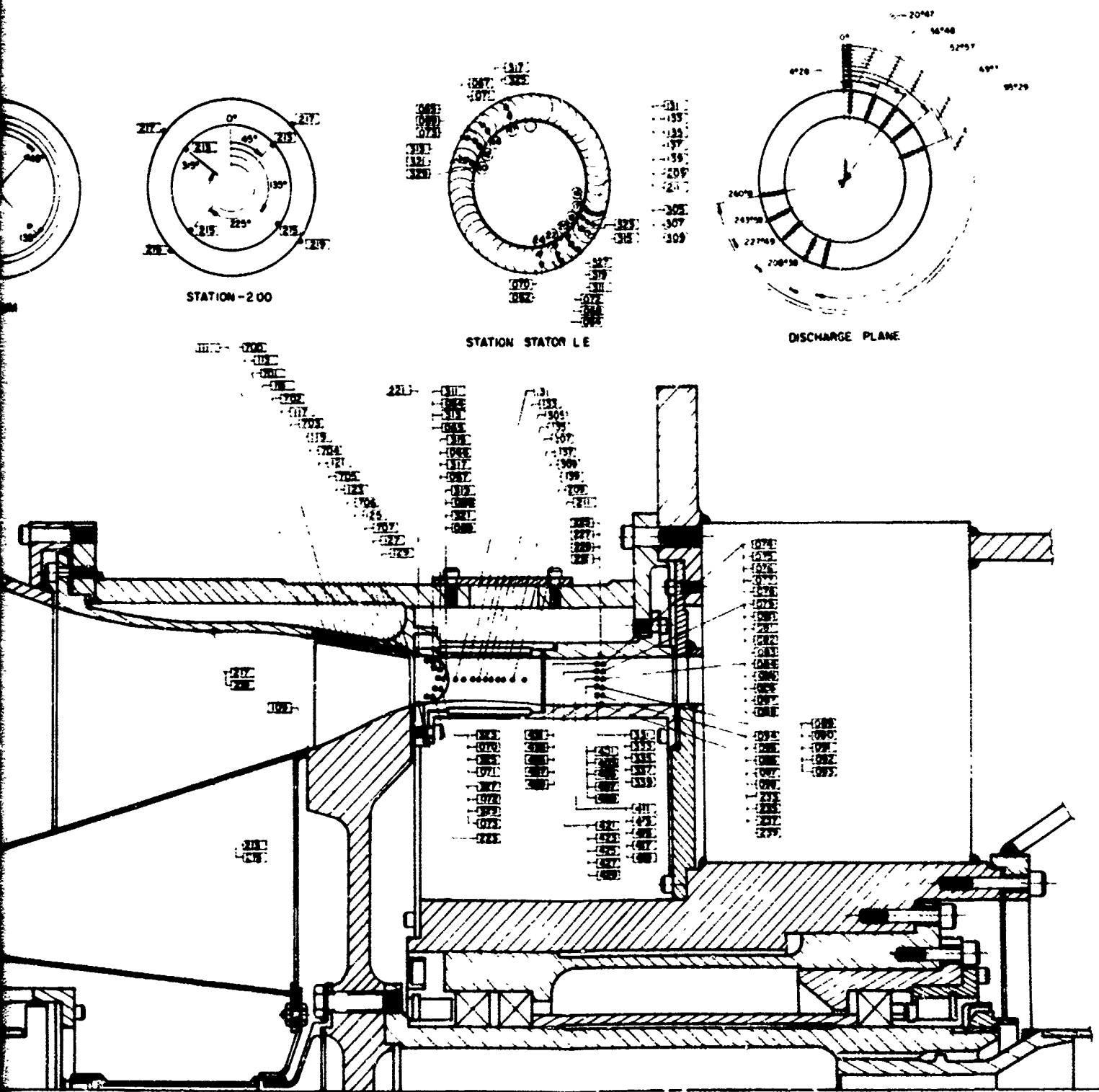




FIGURE 4. ROTOR WITH SPLITTER VANES



FIGURE 5. VEHICLE INSTRUMENTATION BULKHEAD

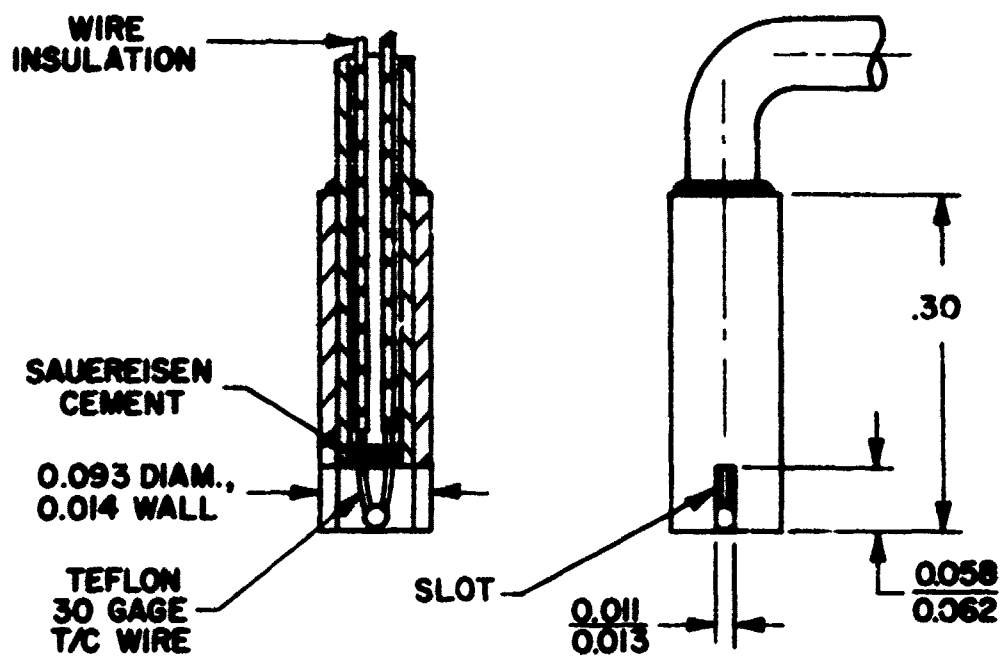


FIGURE 6. SLOT VENTED TEMPERATURE PROBE DESIGN



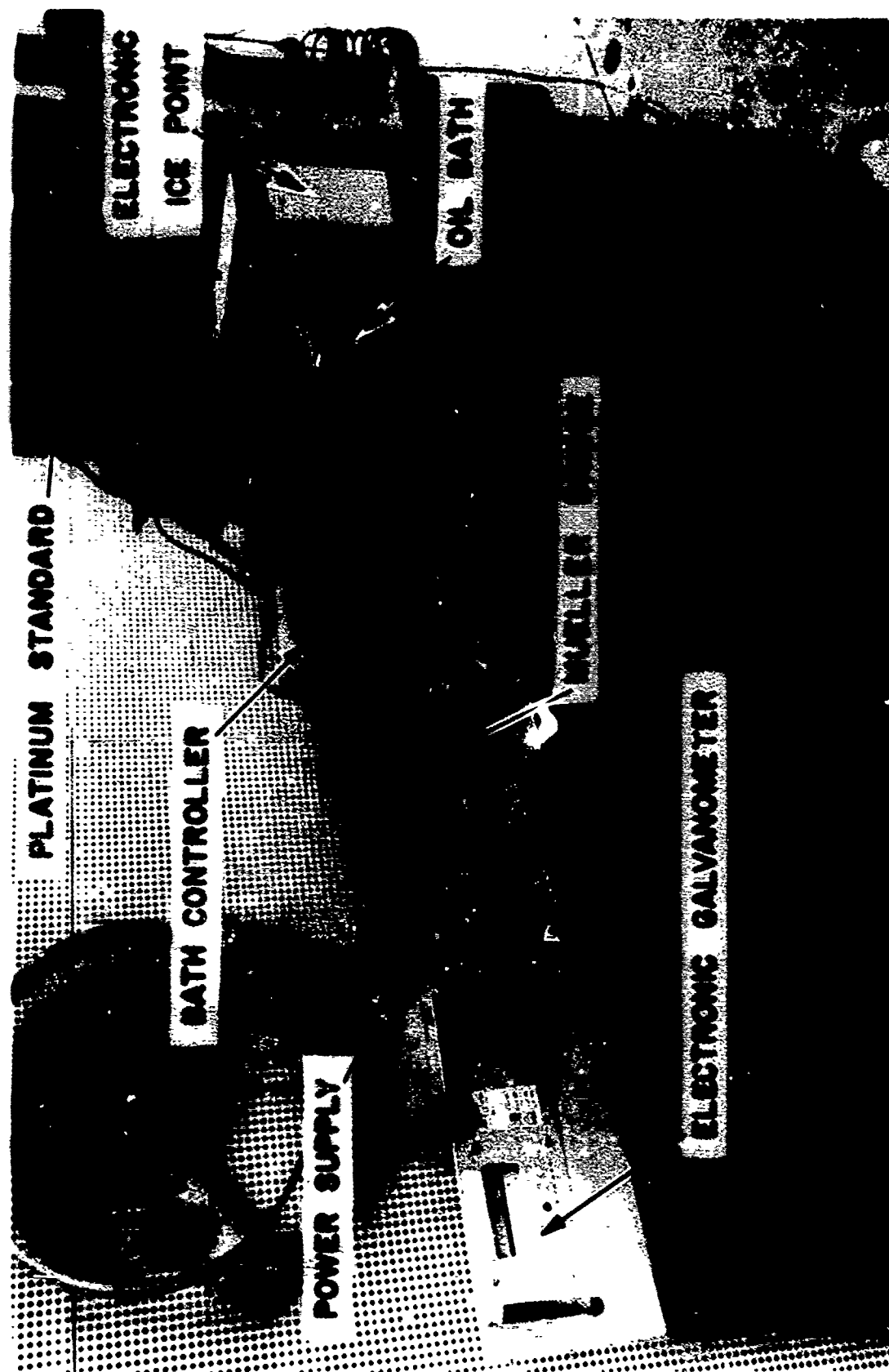


FIGURE 7. TEMPERATURE CALIBRATION SETUP

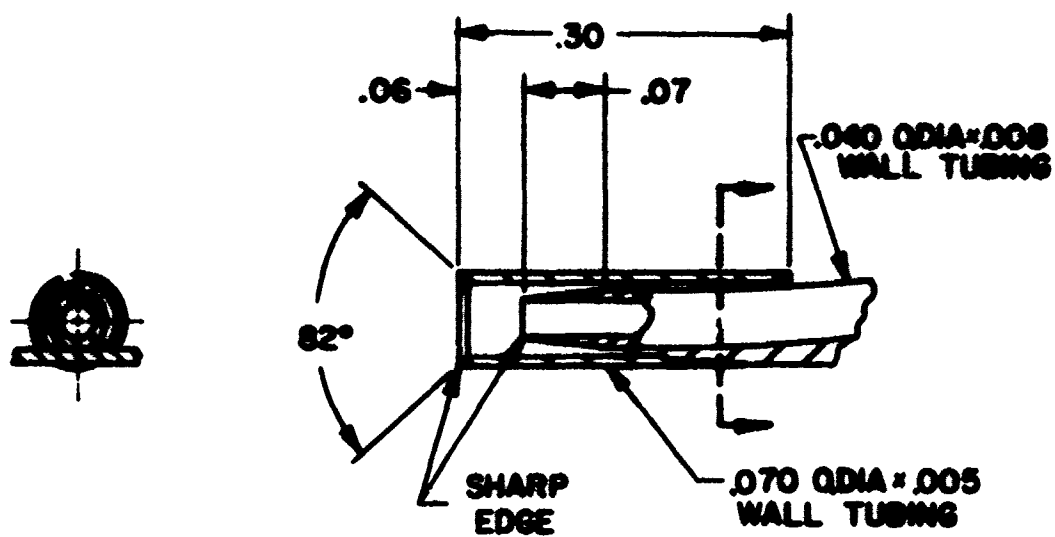


FIGURE 8. KIEL STAGNATION TUBE DESIGN

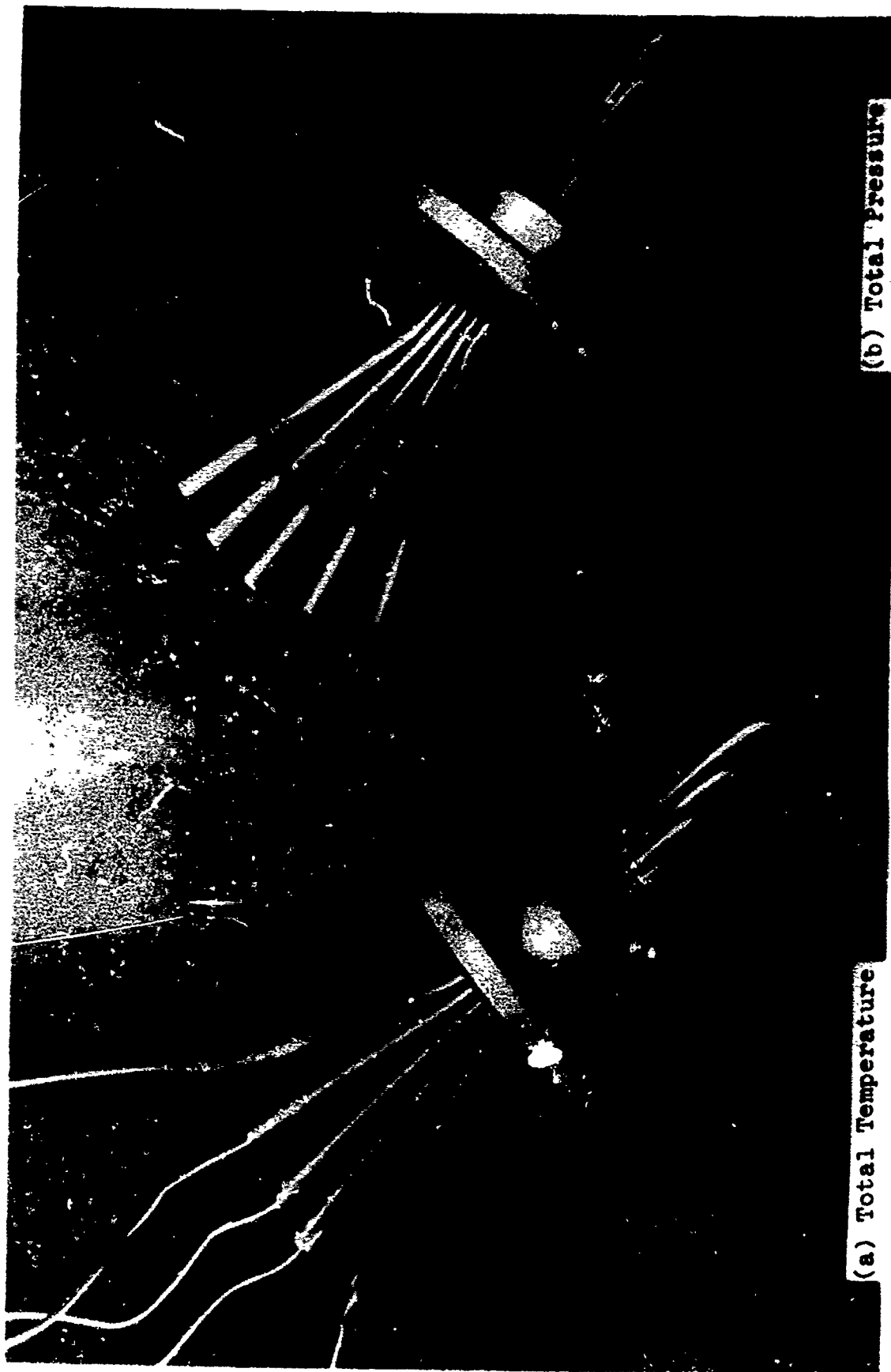


FIGURE 9. INSTRUMENTATION RAKES



**FIGURE 10. VANE-MOUNTED INSTRUMENTATION**

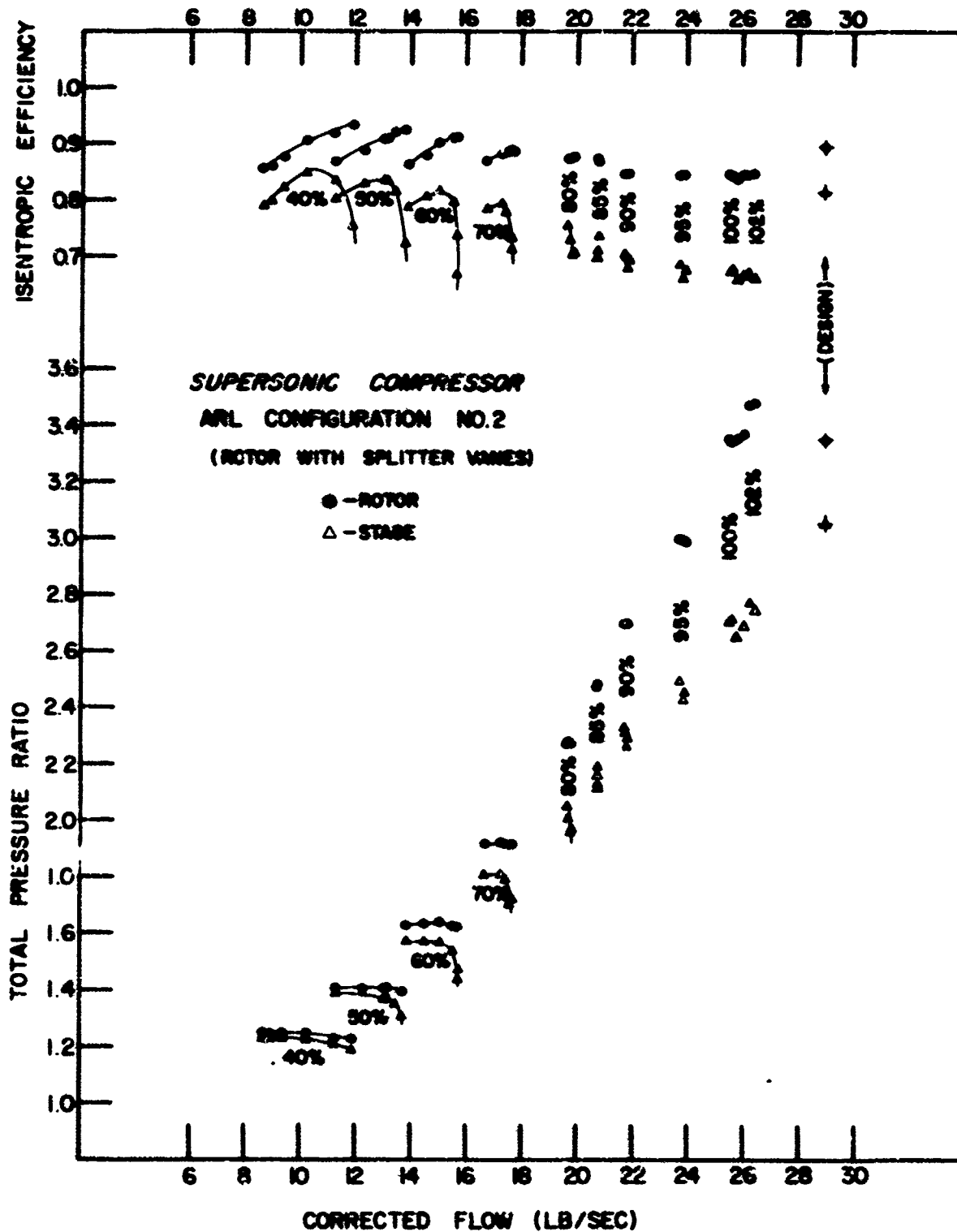


FIGURE 11. COMPRESSOR PERFORMANCE MAP

TABLE V

IDENTIFICATION OF SYMBOLS  
FOR 40%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
212050109840	⊙
212050213440	▽
212050315040	+
212050415940	×
212050516240	◇
212050616440	↓

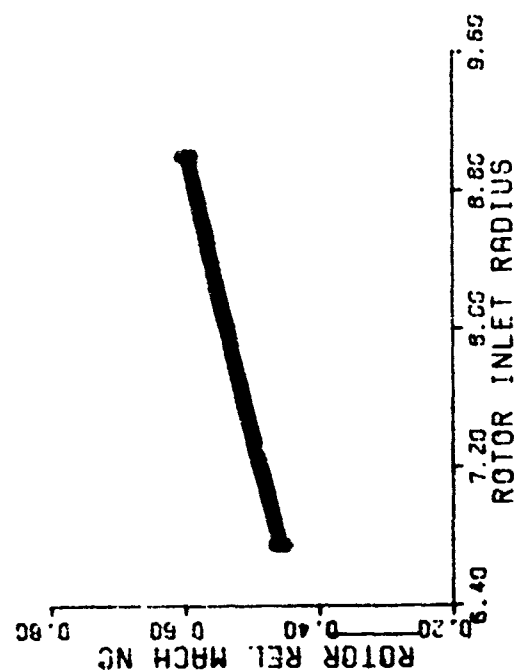


FIGURE 12. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (40% SPEED)

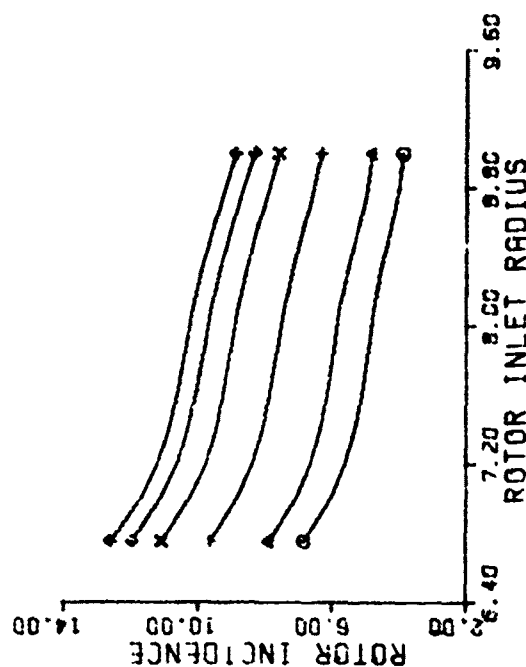


FIGURE 13. ROTOR INCIDENCE VS INLET RADIUS (40% SPEED)

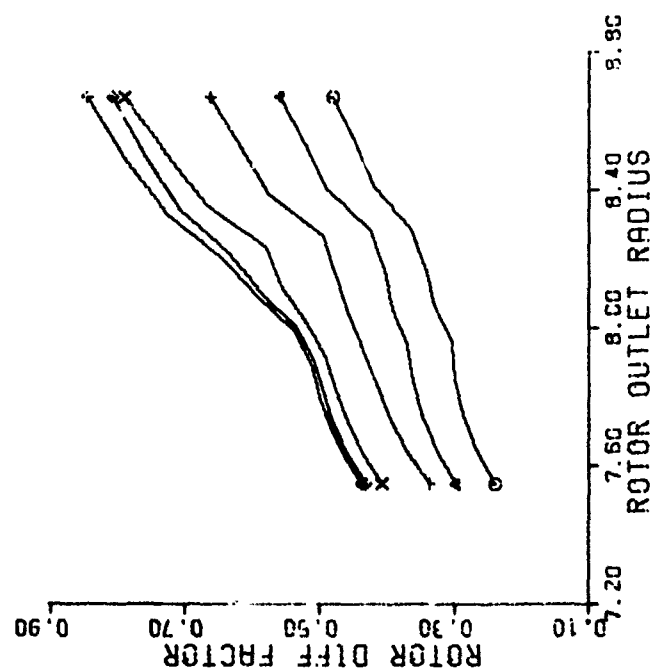


FIGURE 14. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (40% SPEED)

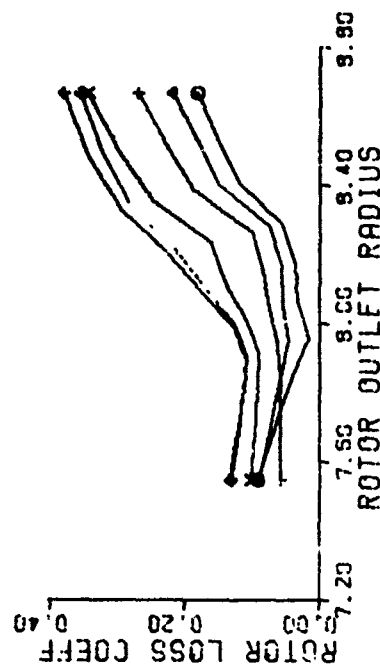


FIGURE 15. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (40% SPEED)

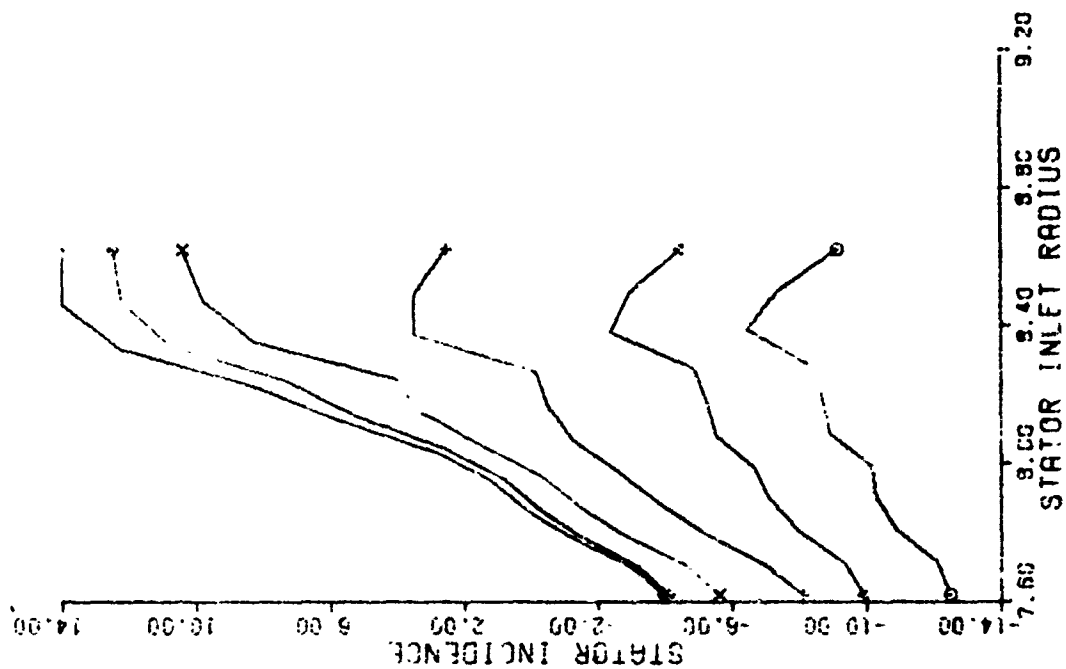


FIGURE 17. STATOR INCIDENCE VS INLET RADIUS  
(40% SPEED)

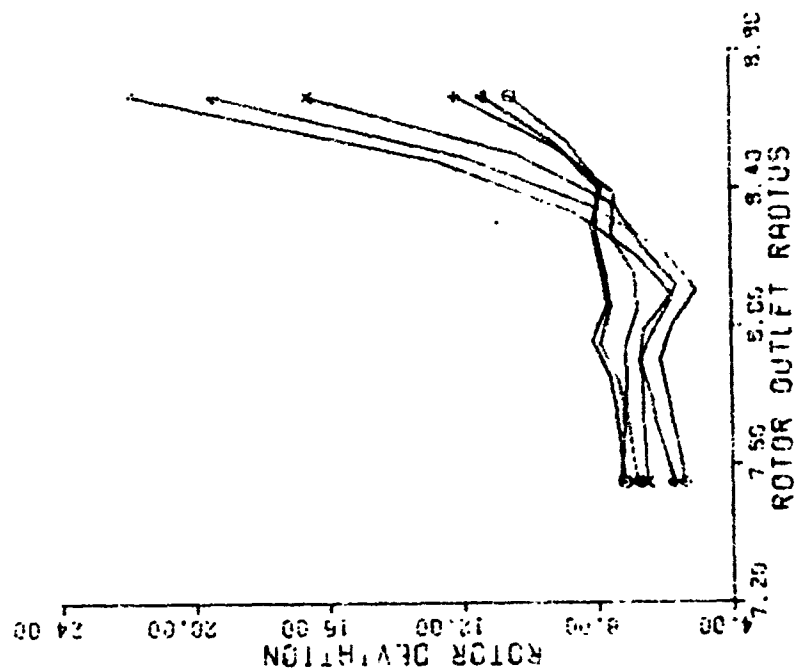


FIGURE 16. ROTOR DEVIATION VS OUTLET RADIUS  
(40% SPEED)



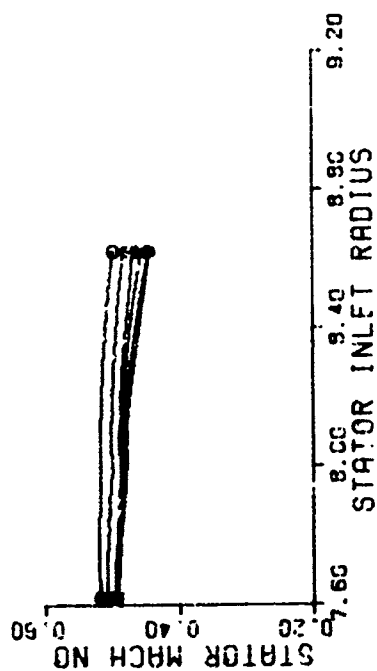


FIGURE 18. STATOR MACH NUMBER VS INLET RADIUS (40% SPEED)

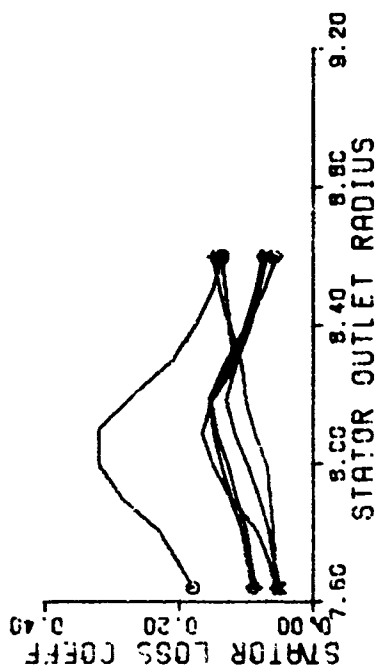


FIGURE 19. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (40% SPEED)

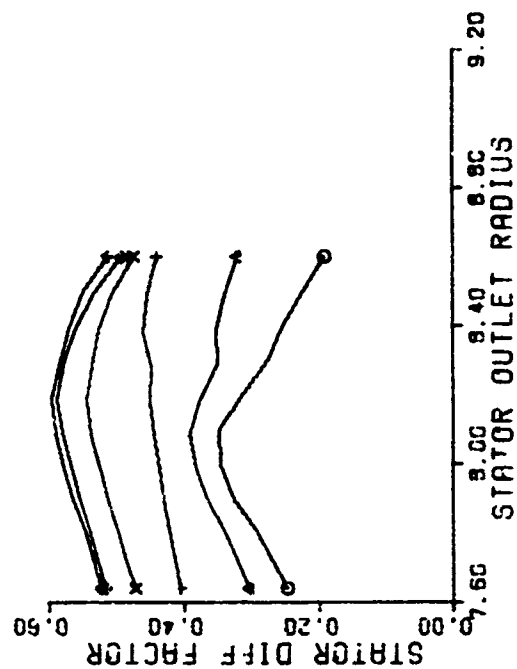


FIGURE 20. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (40% SPEED)

TABLE VI

IDENTIFICATION OF SYMBOLS  
FOR 50%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
212050615050	⊙
212050815750	▽
212050916250	+
212051015050	×
212051114250	⊕
212051212250	⊗

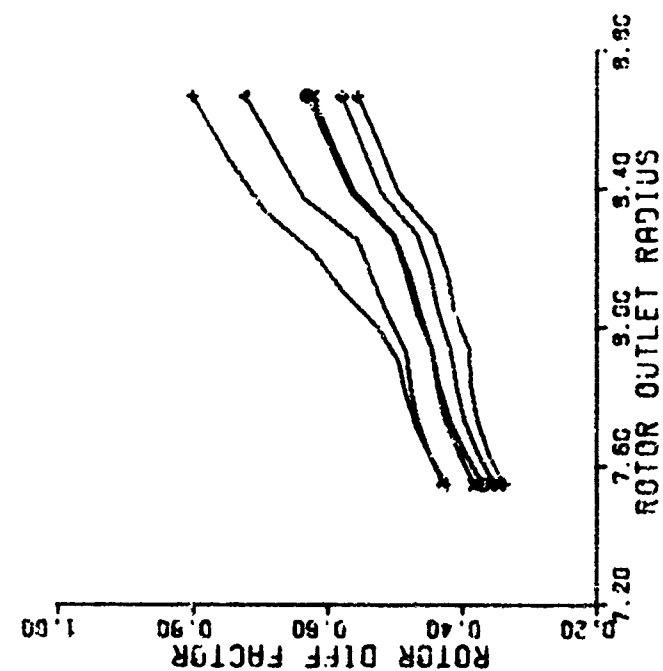
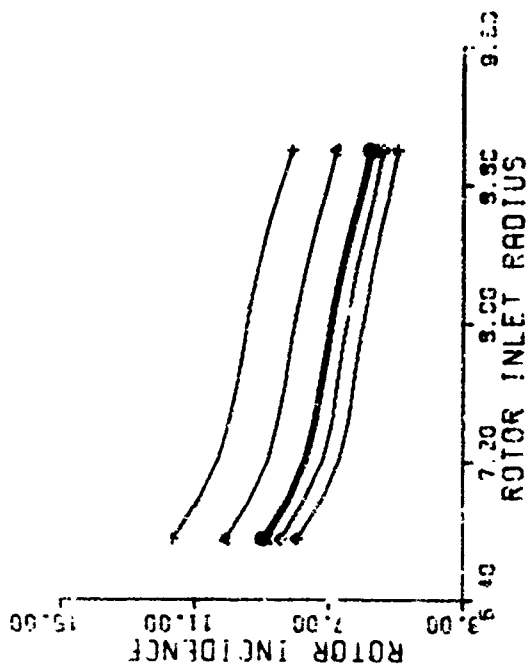
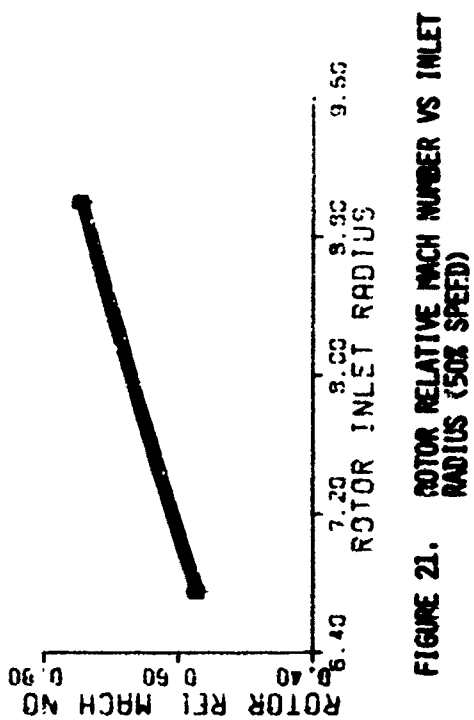


FIGURE 22. ROTOR INCIDENCE VS INLET RADIUS (50% SPEED)

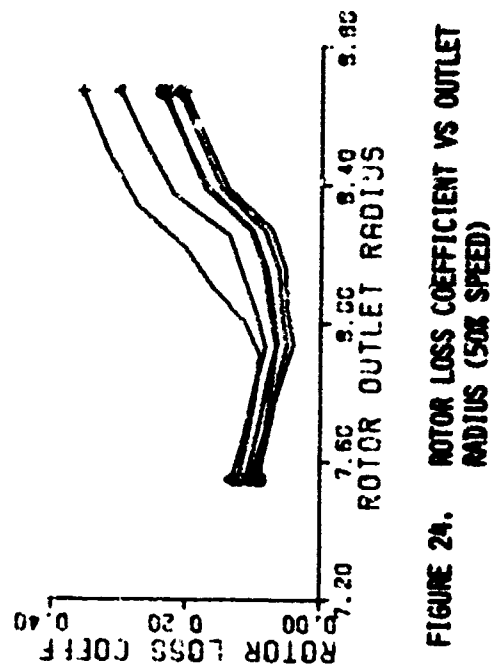


FIGURE 23. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (50% SPEED)

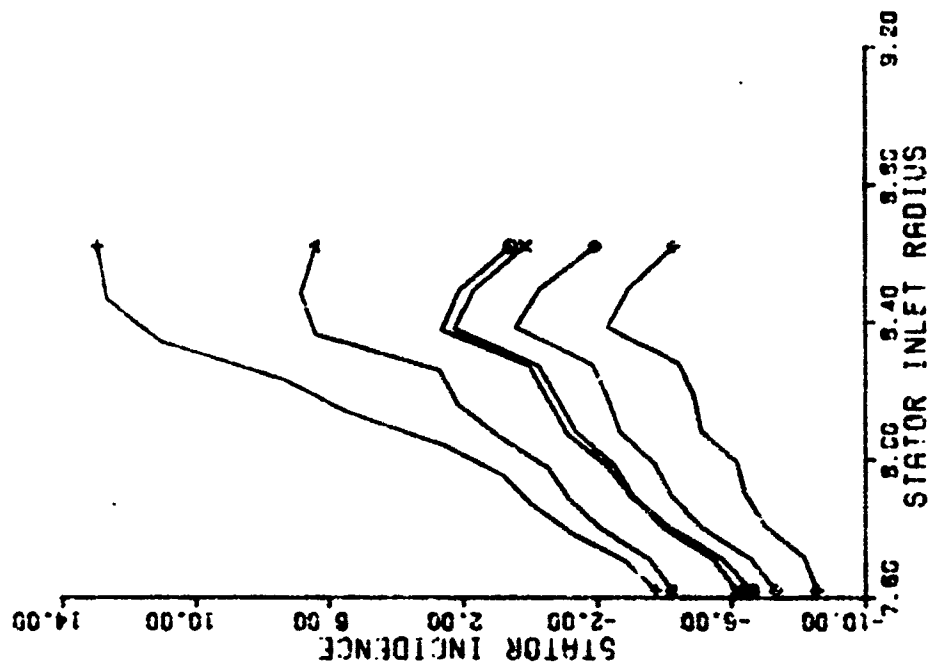


FIGURE 25. ROTOR DEVIATION VS OUTLET RADIUS  
(50% SPEED)

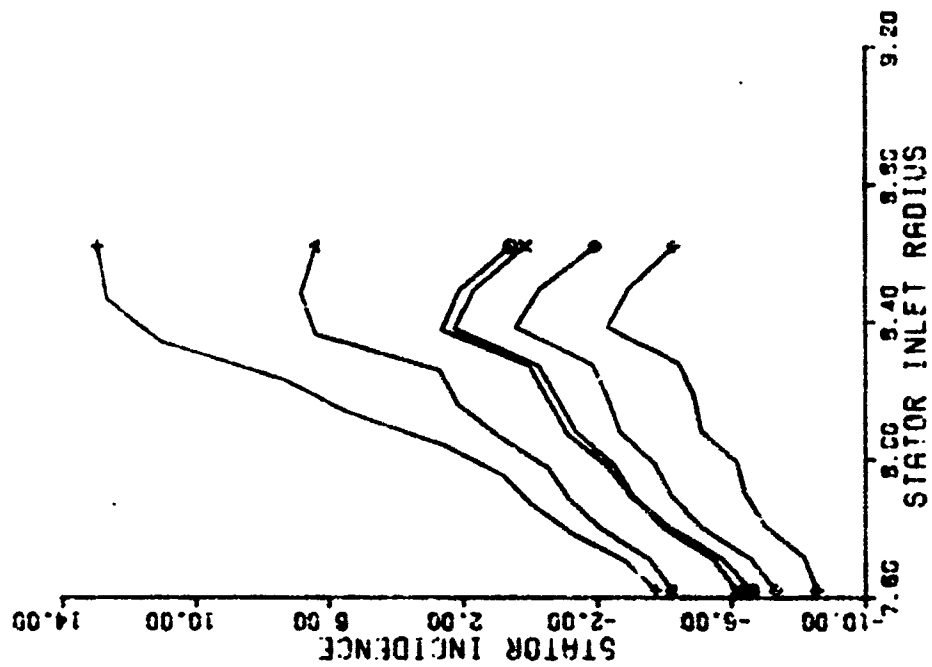


FIGURE 26. STATOR INCIDENCE VS INLET RADIUS  
(50% SPEED)

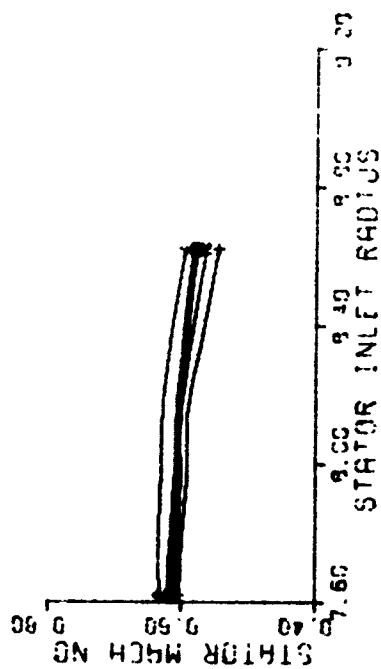


FIGURE 27. STATOR MACH NUMBER VS INLET RADIUS  
(50% SPEED)

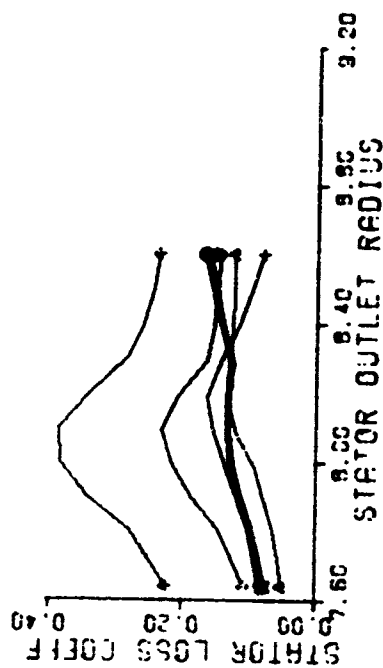


FIGURE 28. STATOR LOSS COEFFICIENT VS OUTLET  
RADIUS (50% SPEED)

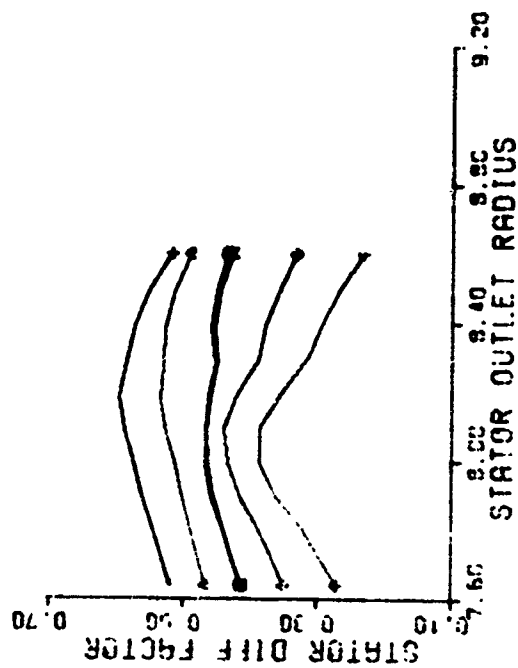


FIGURE 29. STATOR DIFFUSION FACTOR VS OUTLET  
RADIUS (50% SPEED)

TABLE VII

IDENTIFICATION OF SYMBOLS  
FOR 604-SPEED ACROSS-MADE FIGURES

TEST IDENTIFICATION	SYMBOL
212051415060	⊙
212051514360	▽
212051612960	+
212051715560	×
212051815960	◇
212051916360	⬇

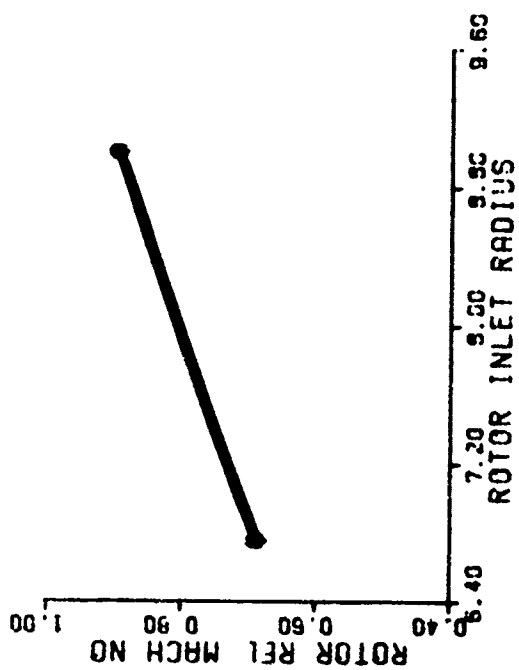


FIGURE 30. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (60% SPEED)

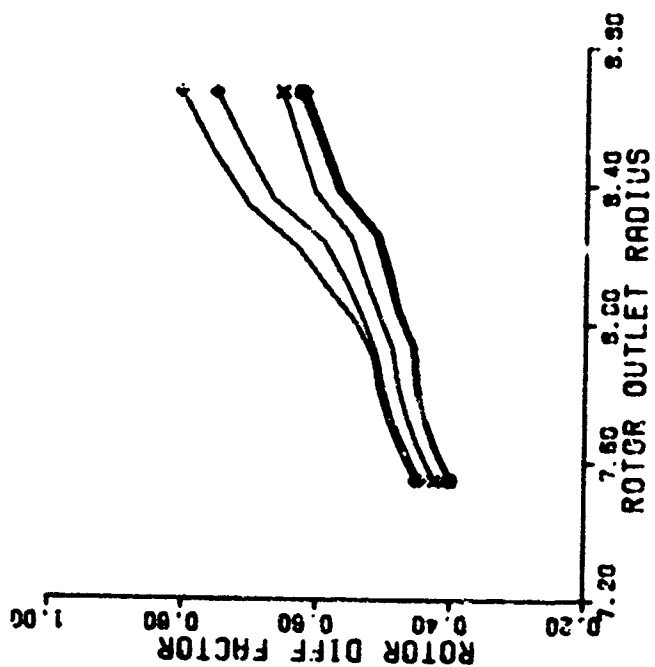


FIGURE 32. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (60% SPEED)

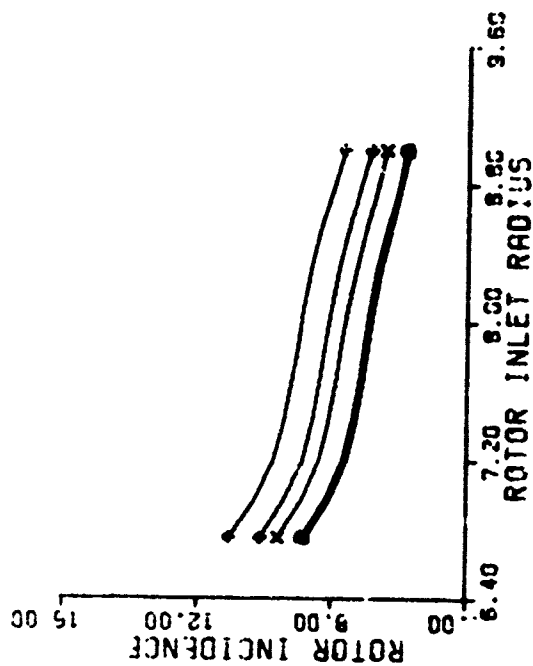


FIGURE 31. ROTOR INCIDENCE VS INLET RADIUS (60% SPEED)

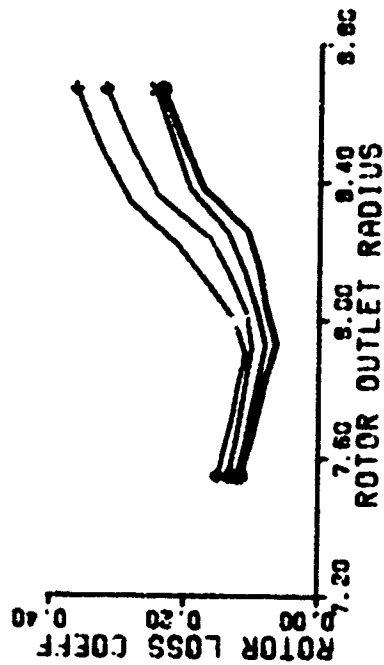


FIGURE 33. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (60% SPEED)

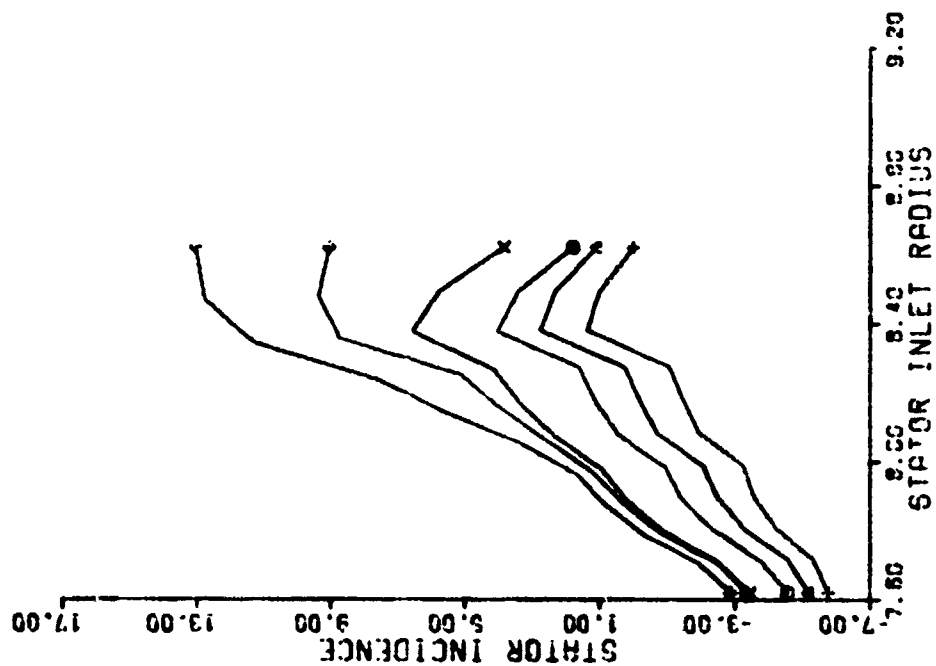


FIGURE 35. STATOR INCIDENCE VS INLET RADIUS (60% SPEED)

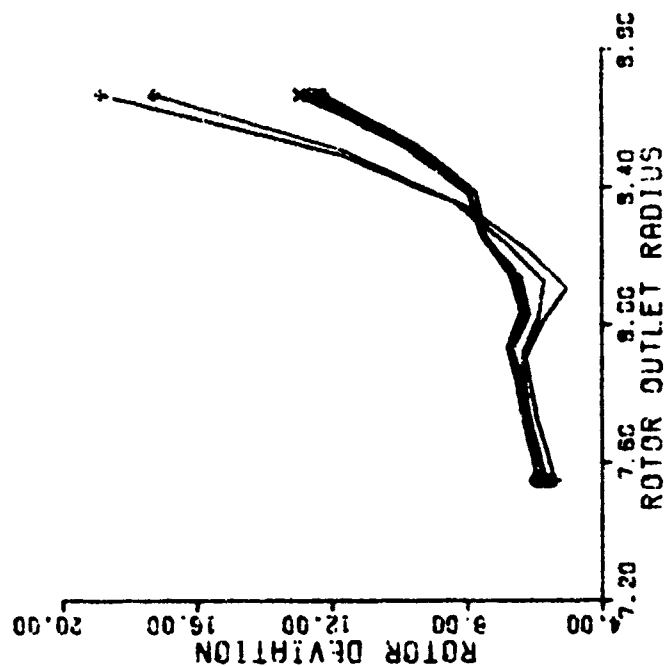


FIGURE 34. ROTOR DEVIATION VS OUTLET RADIUS (60% SPEED)



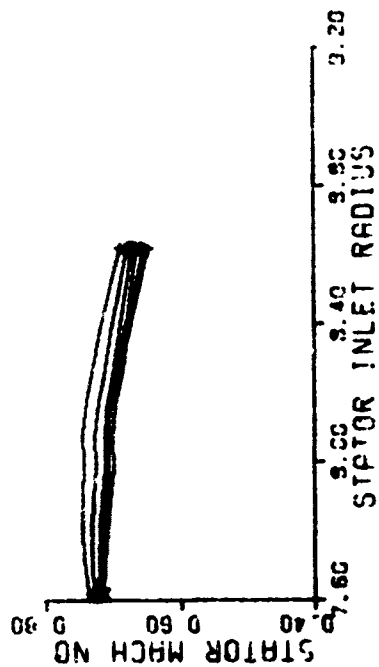


FIGURE 36. STATOR MACH NUMBER VS INLET RADIUS (60% SPEED)

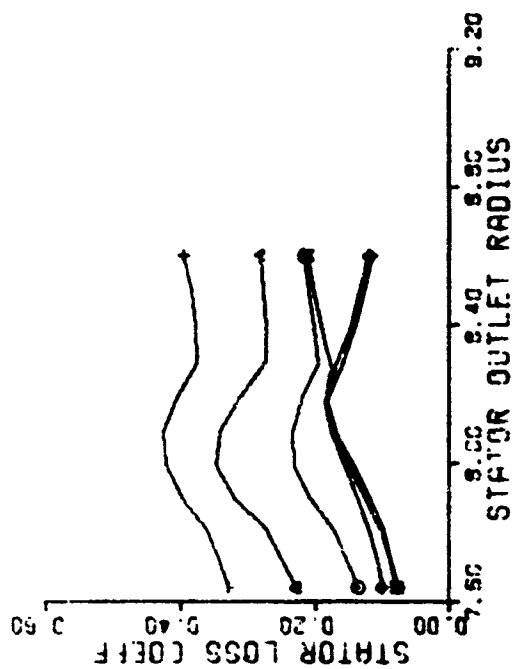


FIGURE 37. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (60% SPEED)

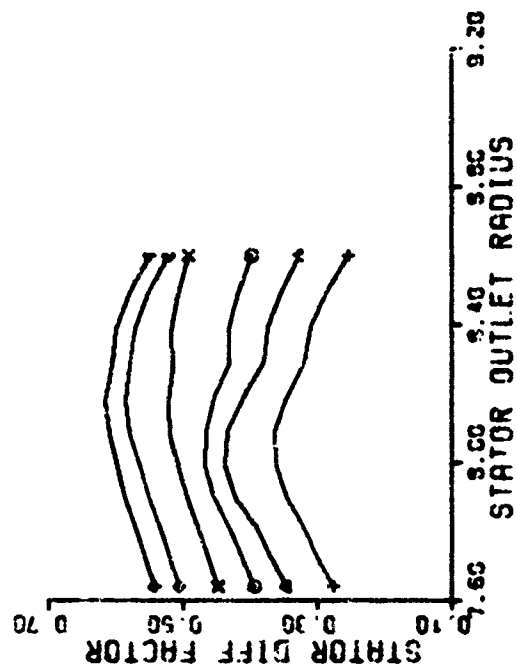


FIGURE 38. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (60% SPEED)

**TABLE VIII**

**IDENTIFICATION OF SYMBOLS  
FOR 704-SPEED ACROSS-BLADE FIGURES**

<b>TEST IDENTIFICATION</b>	<b>SYMBOL</b>
<b>212070215070</b>	<b>⊖</b>
<b>212070314770</b>	<b>▽</b>
<b>212070615070</b>	<b>+</b>
<b>212070715670</b>	<b>×</b>
<b>212070815970</b>	<b>◇</b>
<b>212070916170</b>	<b>↓</b>

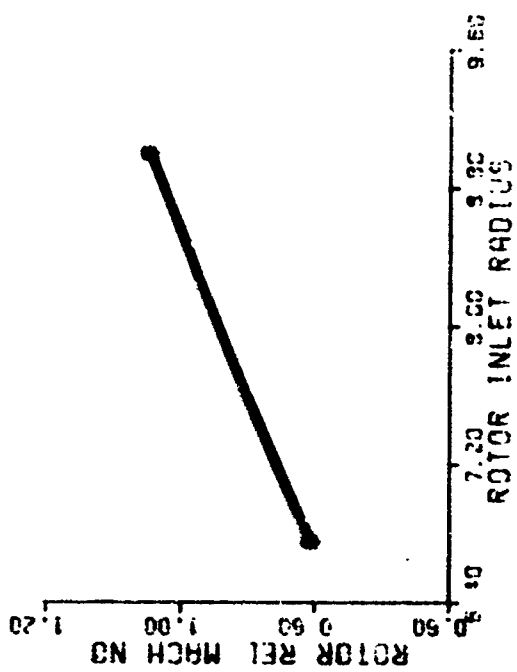


FIGURE 39. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (70% SPEED)

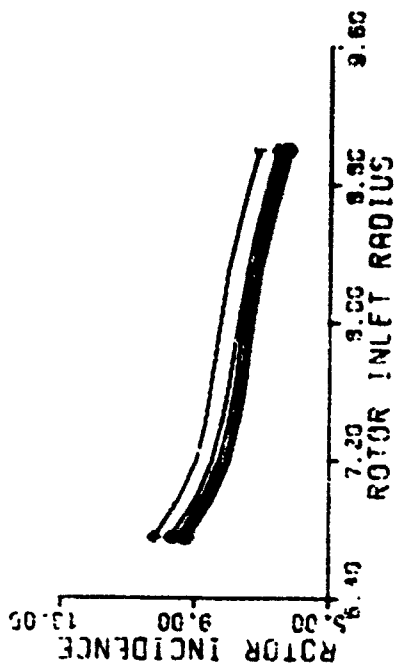


FIGURE 40. ROTOR INCIDENCE VS INLET RADIUS (70% SPEED)

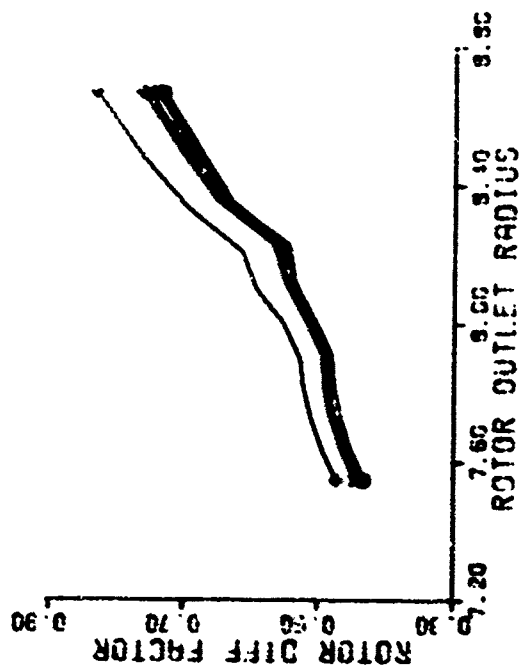


FIGURE 41. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (70% SPEED)

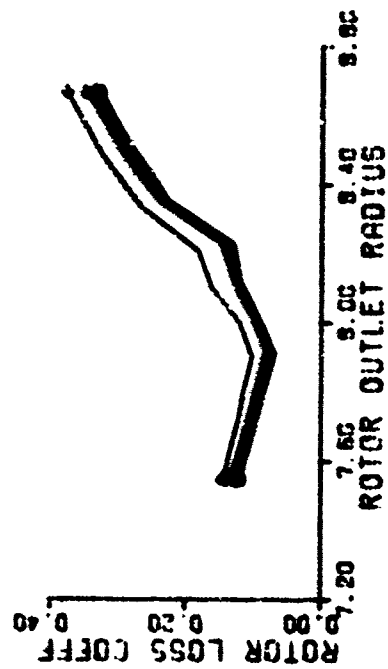


FIGURE 42. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (70% SPEED)

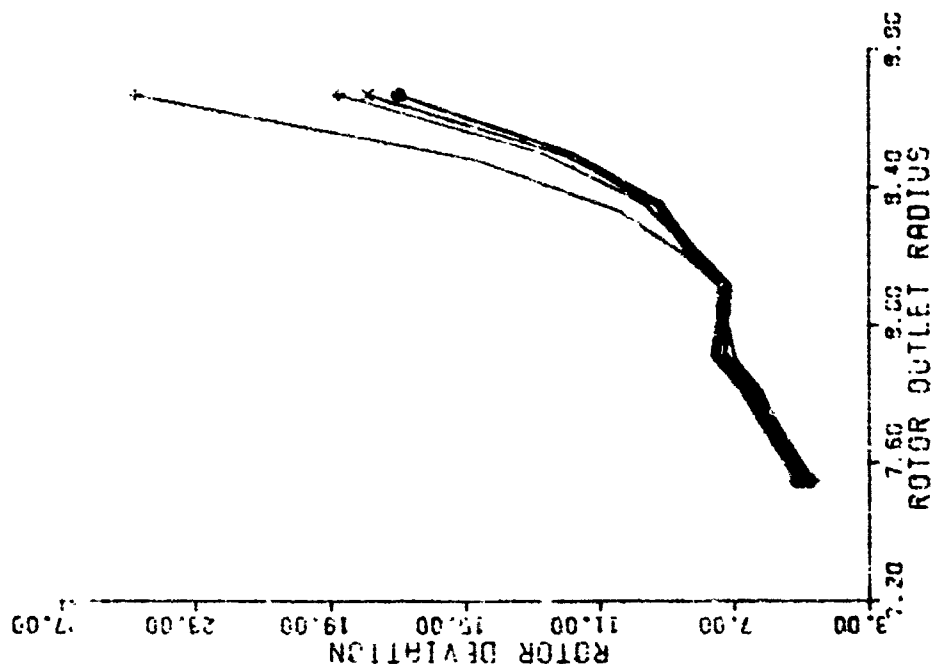


FIGURE 43. ROTOR DEVIATION VS OUTLET RADIUS  
(70% RADIUS)

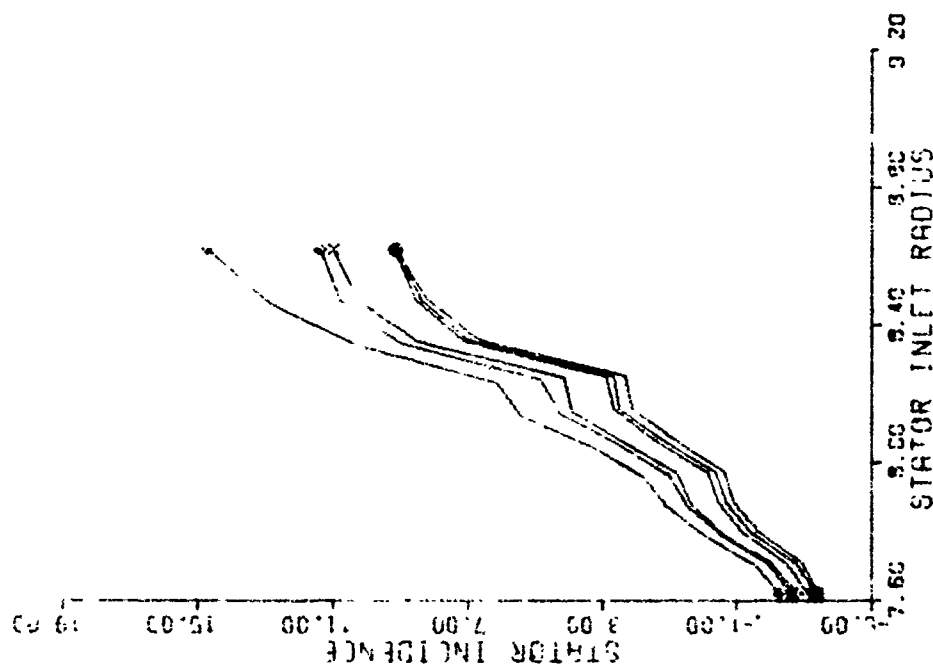


FIGURE 44. STATOR INCIDENCE VS INLET RADIUS  
(70% SPEED)

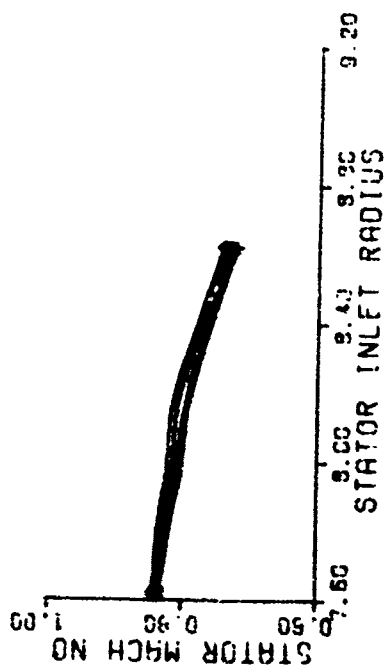


FIGURE 45. STATOR MACH NUMBER VS INLET RADIUS (70% SPEED)

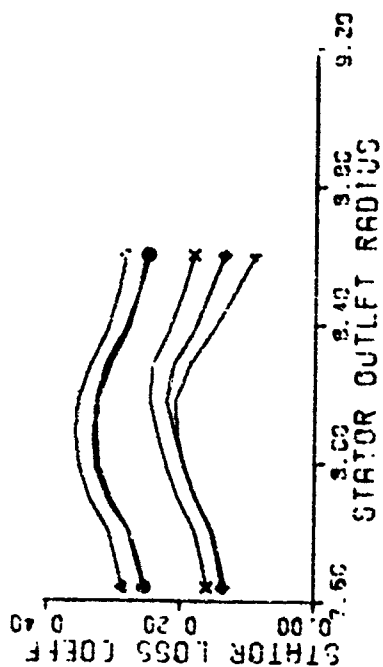


FIGURE 46. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (70% SPEED)

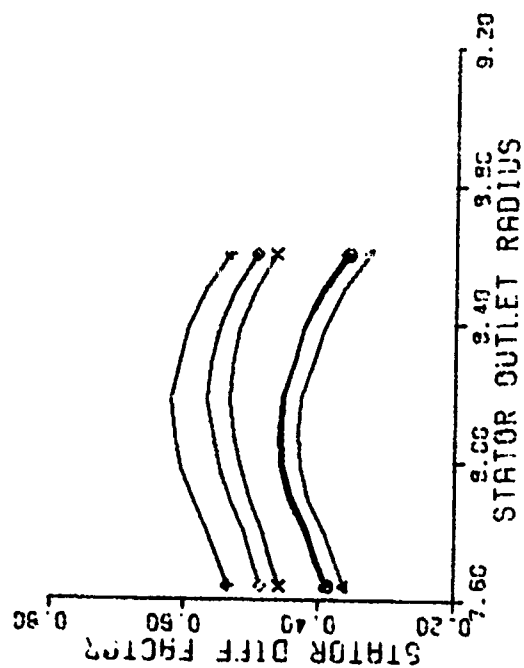


FIGURE 47. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (70% SPEED)

TABLE IX

IDENTIFICATION OF SYMBOLS  
FOR 80%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
212071015080	⊙
212071315080	▽
212071415580	+
212071515980	×

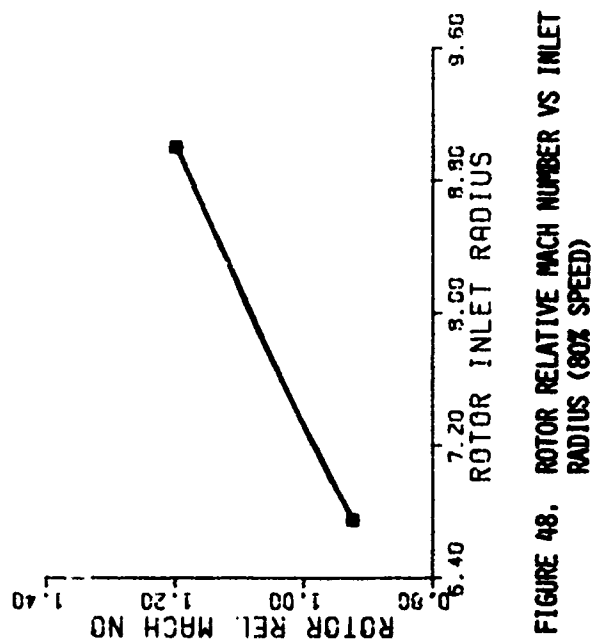


FIGURE 48. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (80% SPEED)

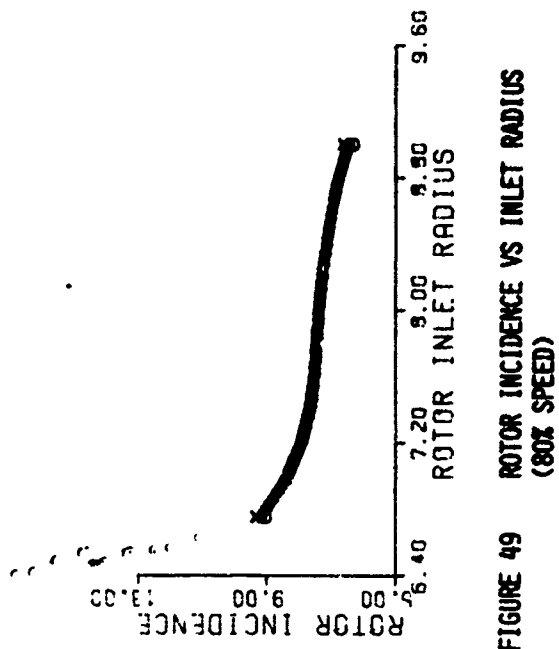


FIGURE 49. ROTOR INCIDENCE VS INLET RADIUS (80% SPEED)

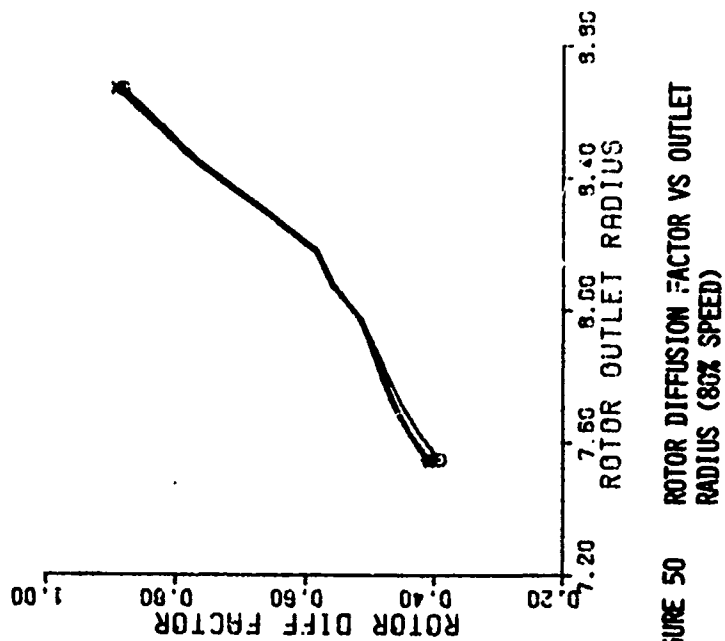


FIGURE 50. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (80% SPEED)

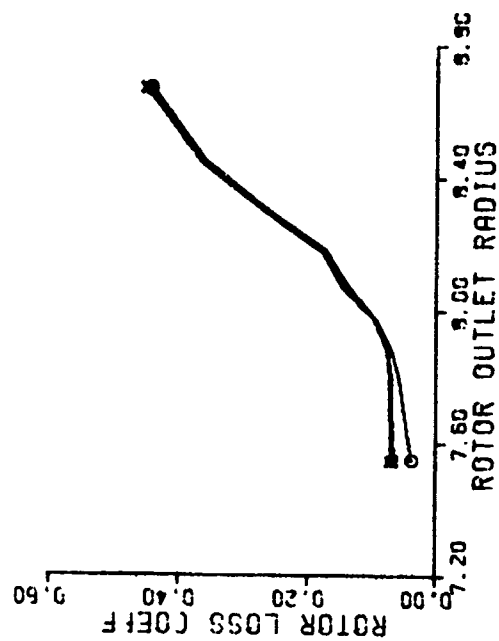


FIGURE 51. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (80% SPEED)

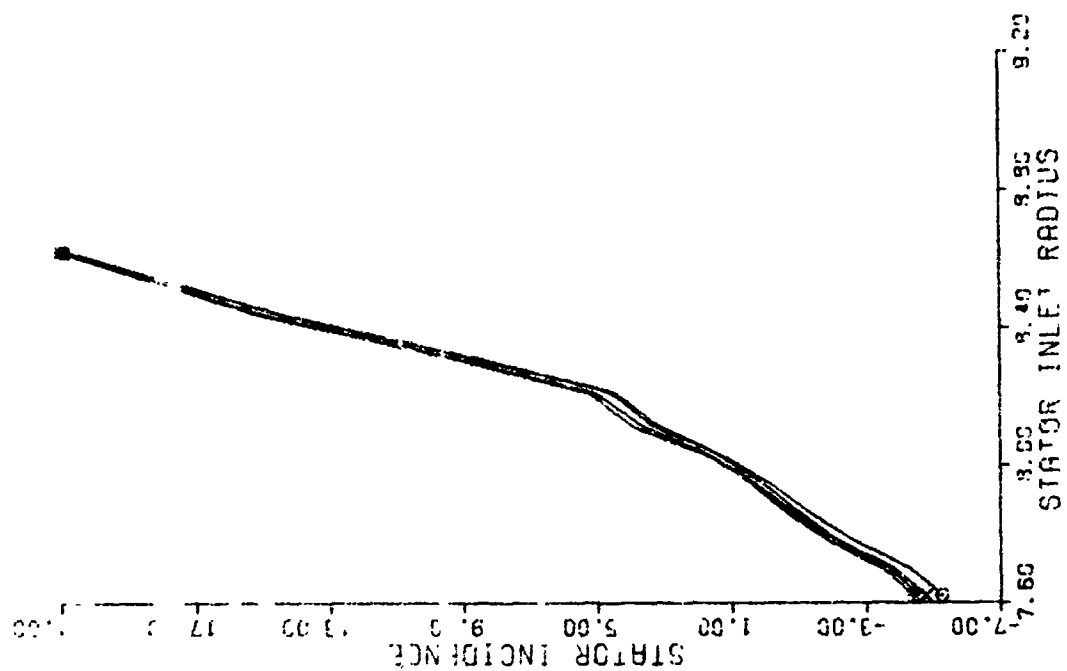


FIGURE 52. ROTOR DEVIATION VS OUTLET RADIUS  
(80% SPEED)

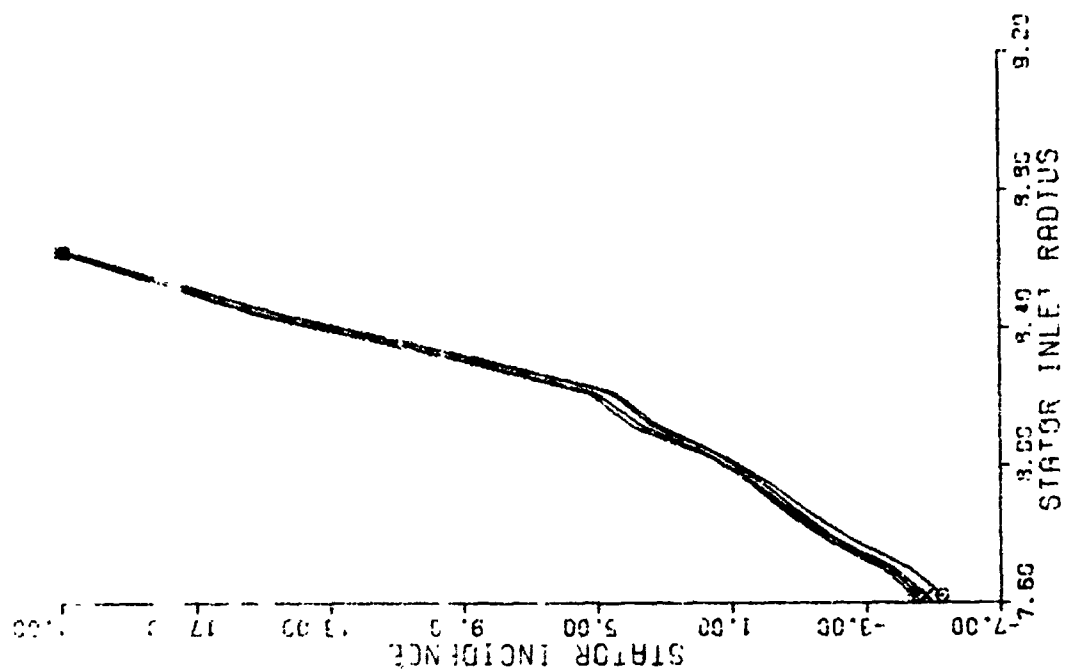


FIGURE 53. STATOR INCIDENCE VS INLET RADIUS  
(80% SPEED)



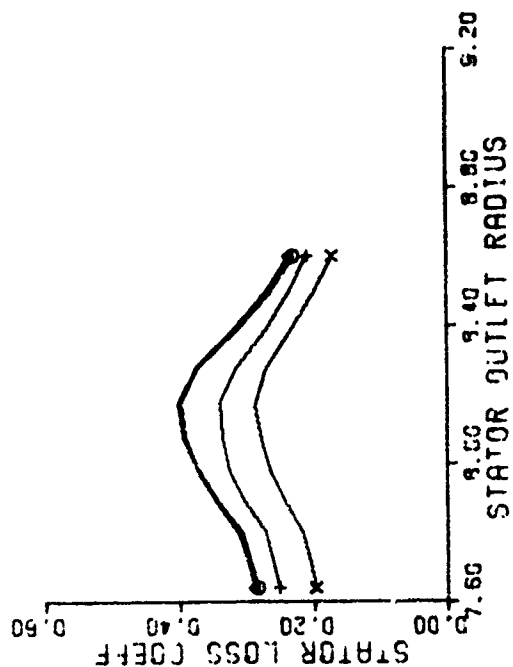


FIGURE 54. STATOR MACH NUMBER VS INLET RADIUS (80% SPEED)

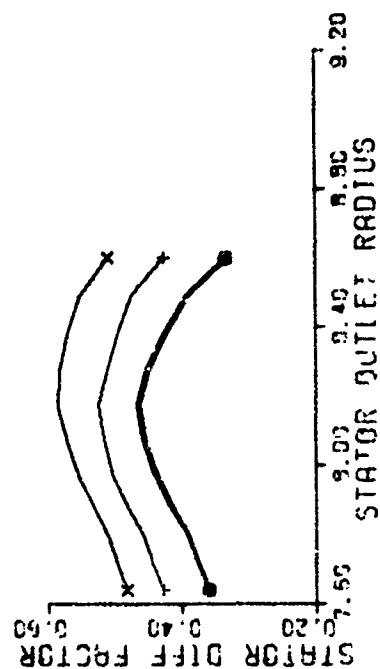


FIGURE 55. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (80% SPEED)

FIGURE 55. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (80% SPEED)

TABLE X

IDENTIFICATION OF SYMBOLS  
FOR 85%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
301180915685	①
301181015885	∇
301180615085	⊥
301180815385	×

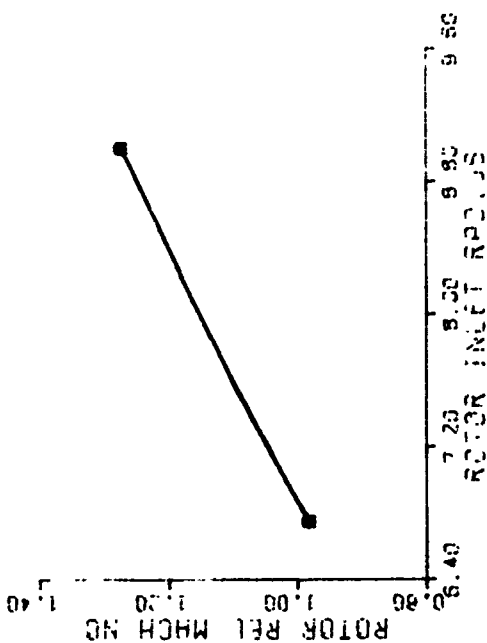


FIGURE 57. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (85% SPEED)

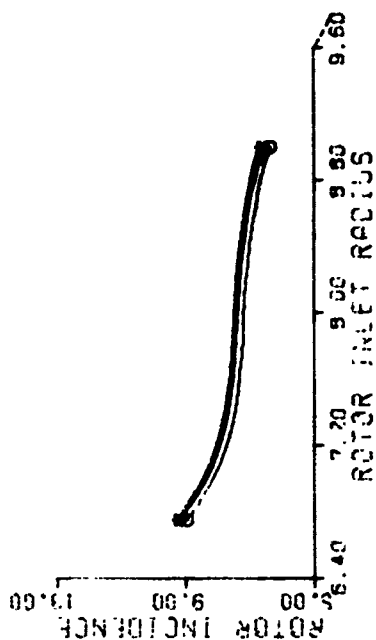


FIGURE 58. ROTOR INCIDENCE VS INLET RADIUS (85% SPEED)

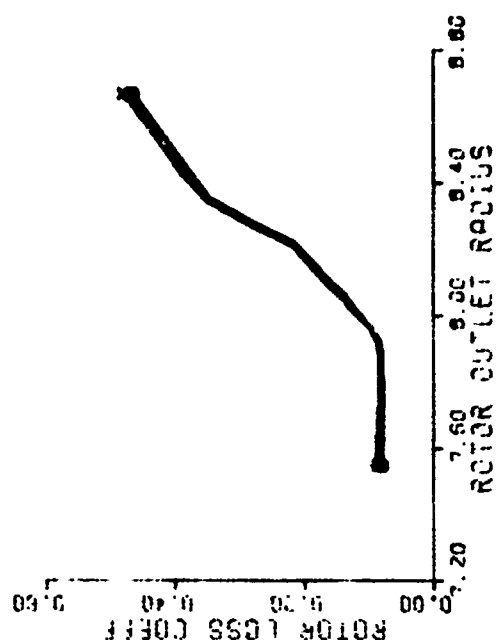
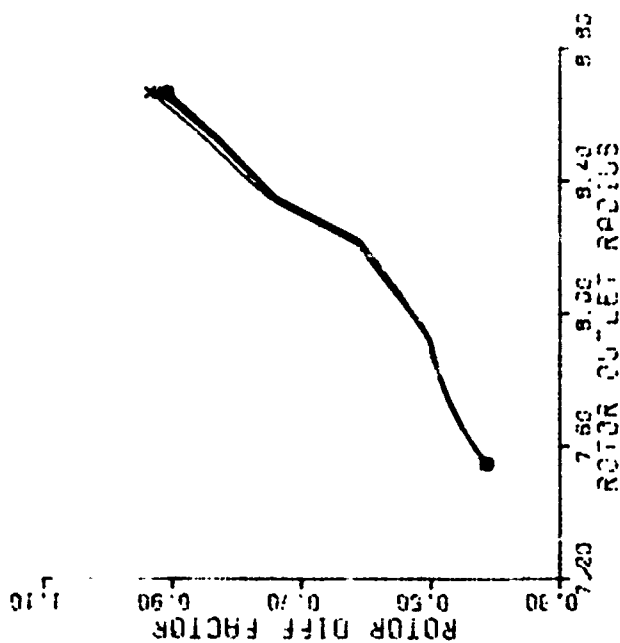


FIGURE 60. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (85% SPEED)

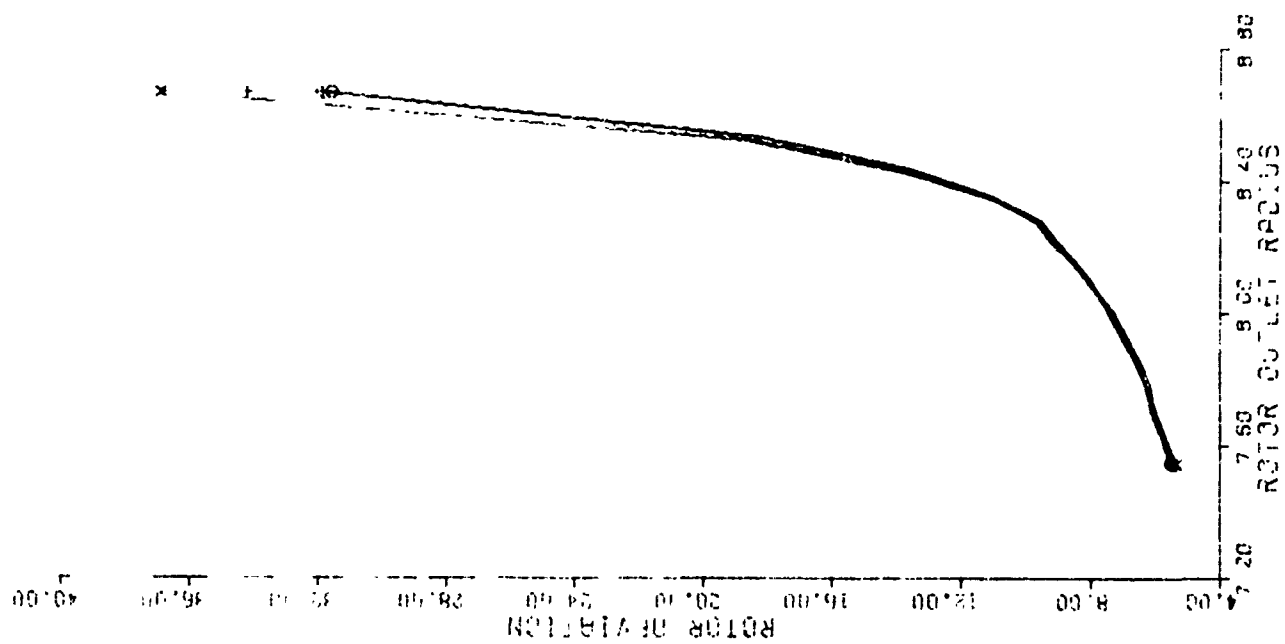


FIGURE 61. ROTOR DEVIATION VS OUTLET RADIUS  
(85% SPEED)

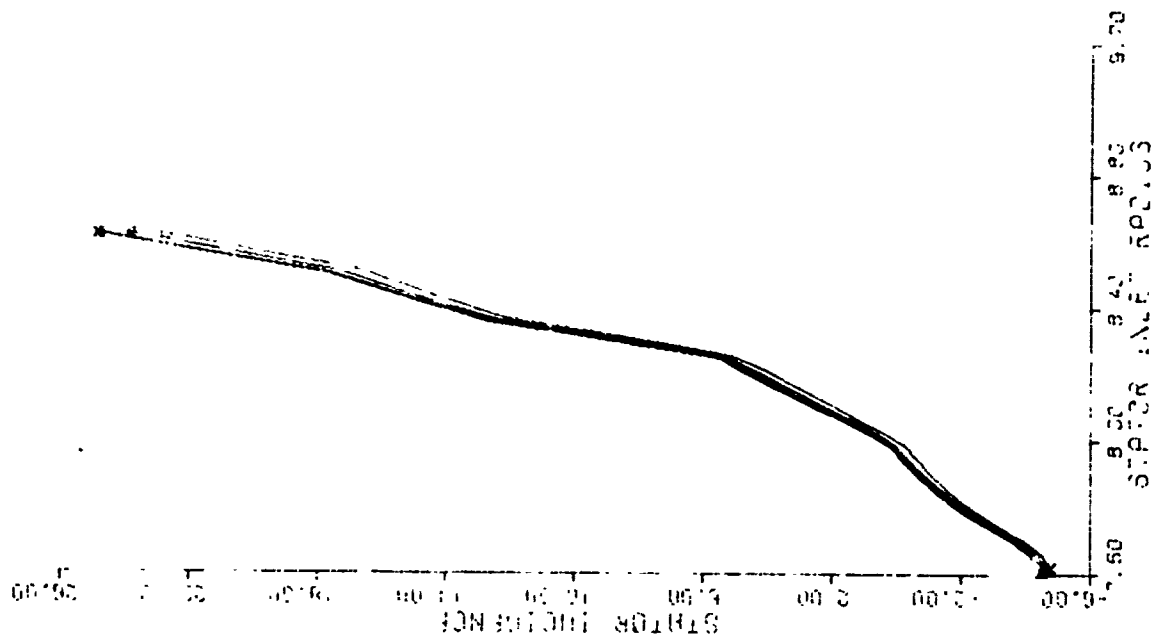


FIGURE 62. STATOR INCIDENCE VS INLET RADIUS  
(85% SPEED)

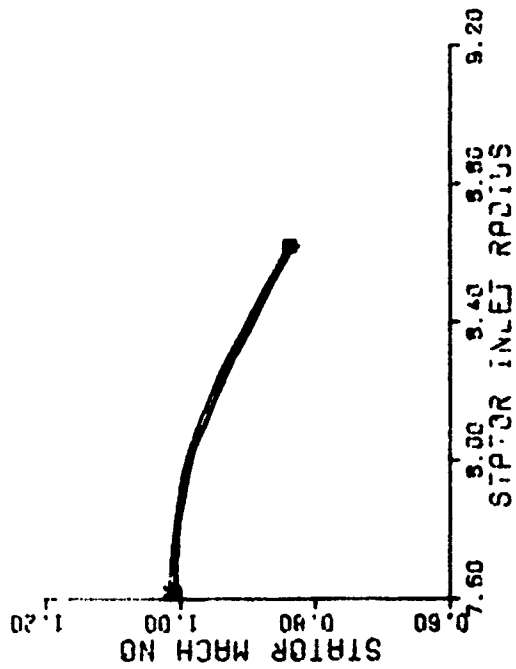


FIGURE 63. STATOR MACH NUMBER VS INLET RADIUS (85% SPEED)

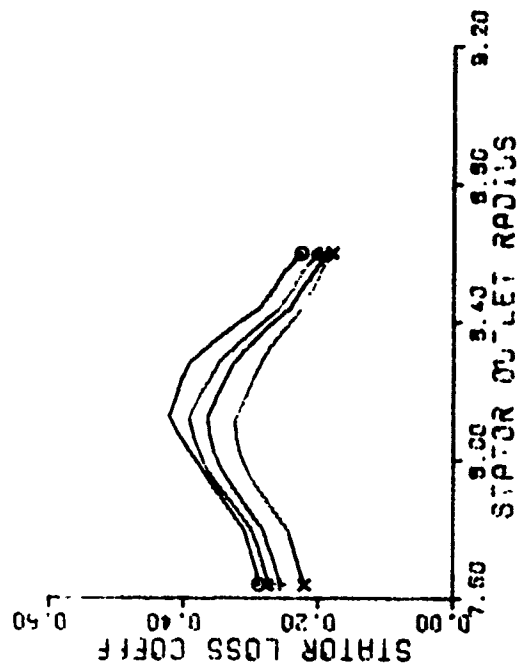


FIGURE 64. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (85% SPEED)

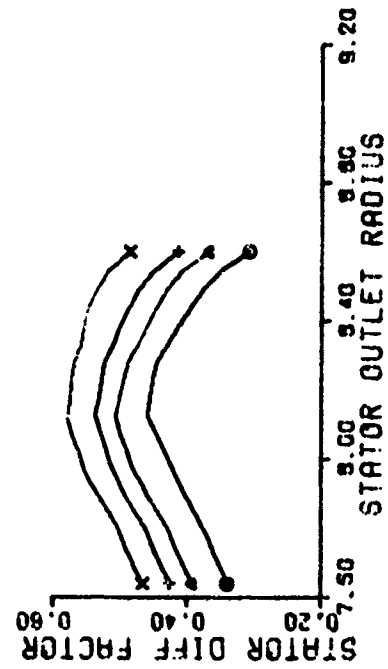


FIGURE 65. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (85% SPEED)

TABLE XI  
IDENTIFICATION OF SYMBOLS  
FOR 90°-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
301181515590	⊙
301181615790	▽
301181715690	+
301181415290	×

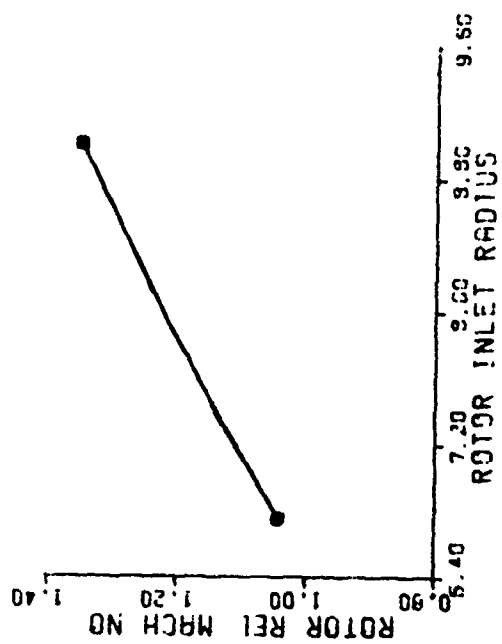


FIGURE 66. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (90% SPEED)

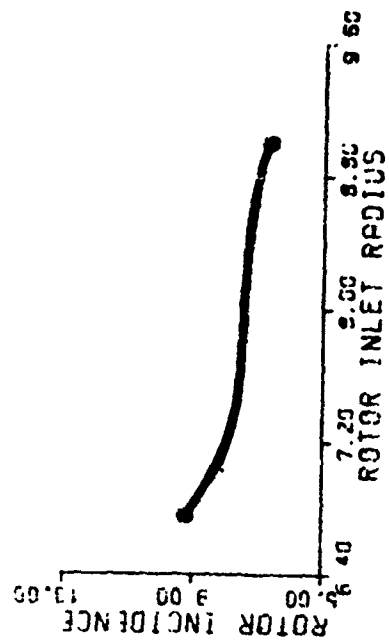


FIGURE 67. ROTOR INCIDENCE VS INLET RADIUS (90% SPEED)

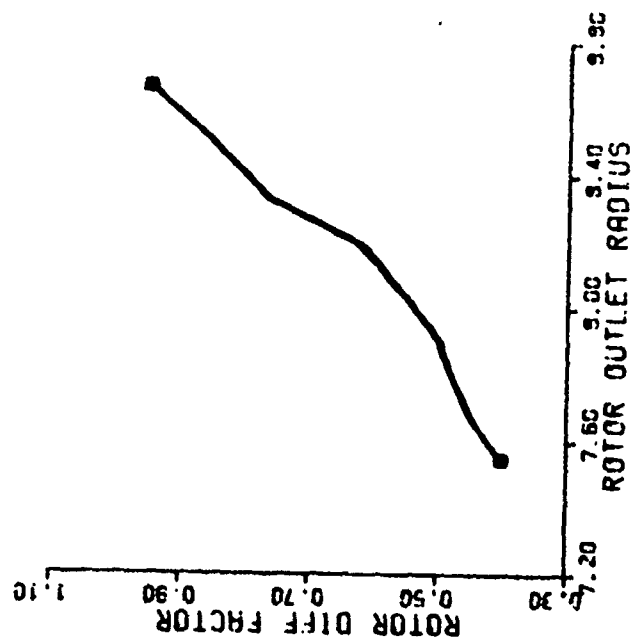


FIGURE 68. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (90% SPEED)

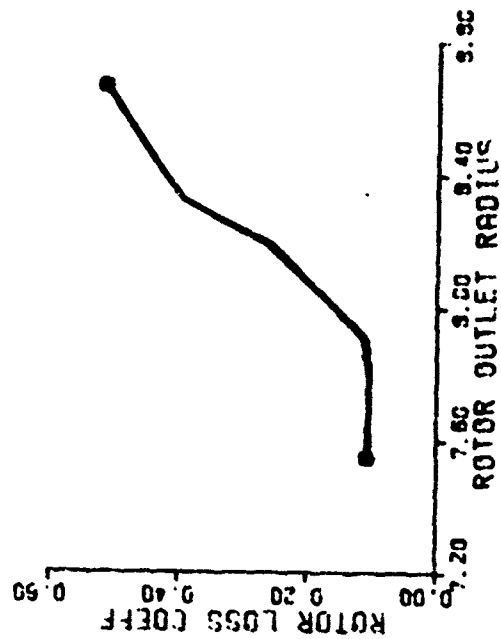


FIGURE 69. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (90% SPEED)

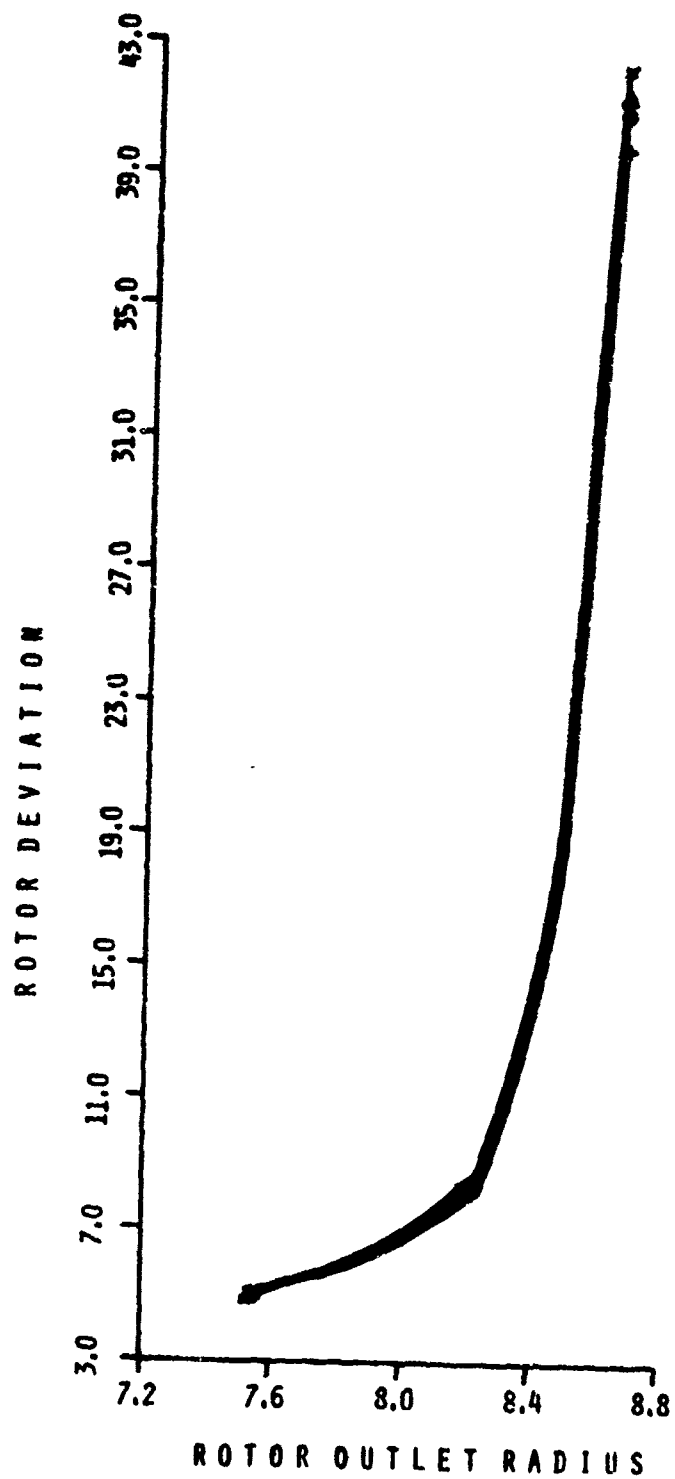


FIGURE 70. ROTOR DEVIATION VS OUTLET RADIUS  
(90% SPEED)



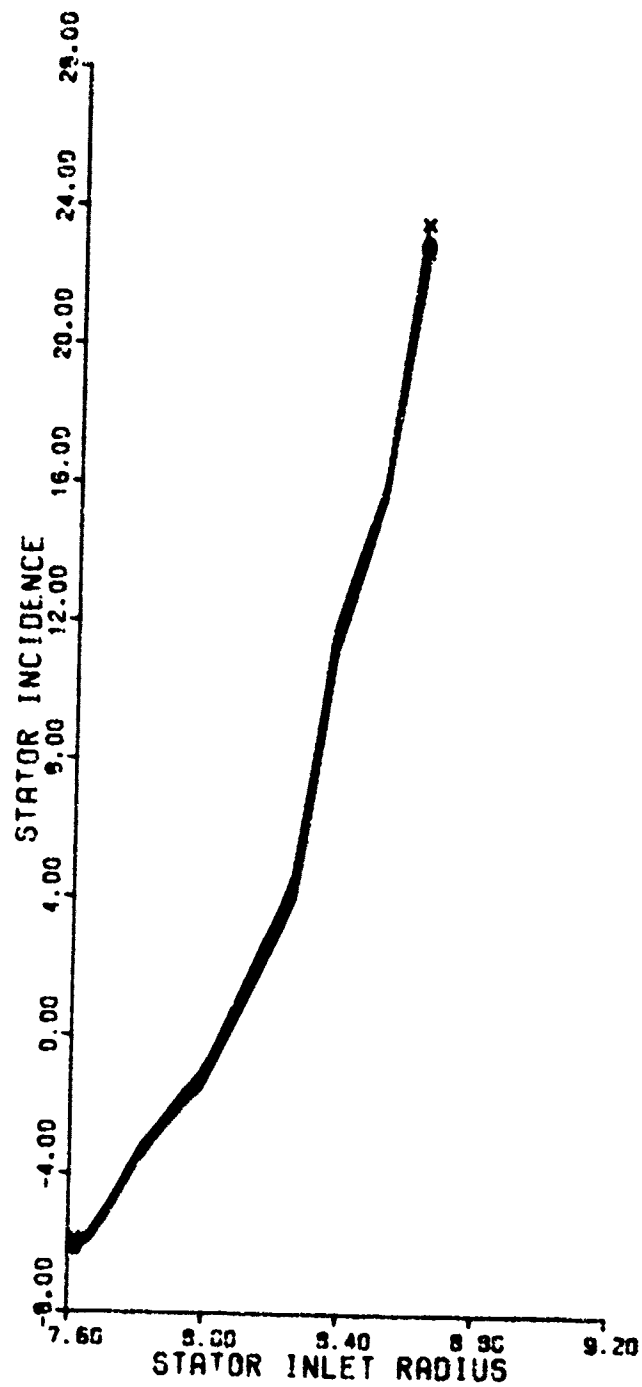


FIGURE 71. STATOR INCIDENCE VS INLET RADIUS  
(90% SPEED)

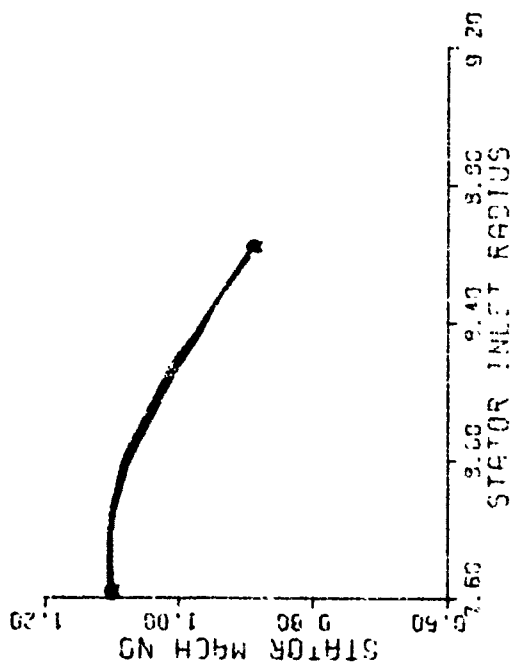


FIGURE 72. STATOR MACH NUMBER VS INLET RADIUS (90% SPEED)

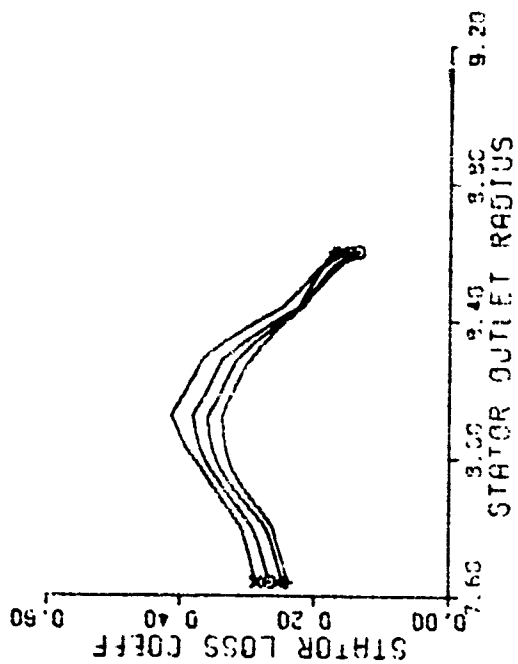


FIGURE 73. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (90% SPEED)

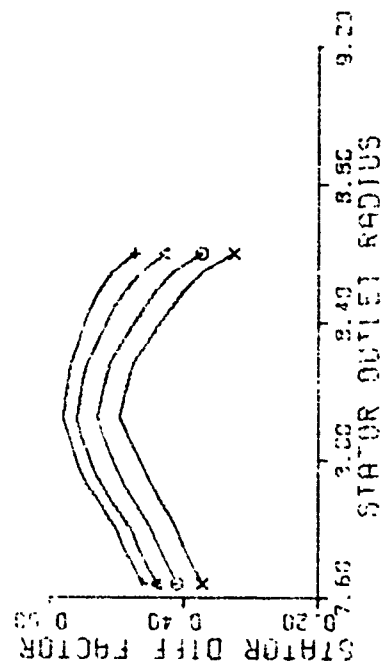


FIGURE 74. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (90% SPEED)

**TABLE XII**

**IDENTIFICATION OF SYMBOLS  
FOR 950-SPEED ACROSS-BLADE FIGURES**

<b>TEST IDENTIFICATION</b>	<b>SYMBOL</b>
301230615095	①
301230415395	▽
301230515695	+

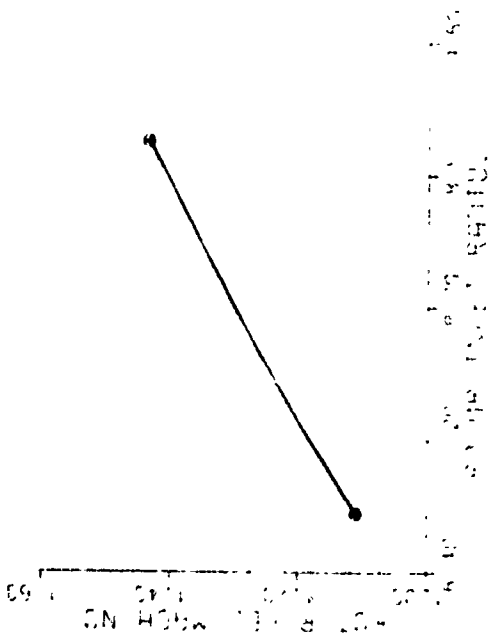


FIGURE 75. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (95% SPEED)

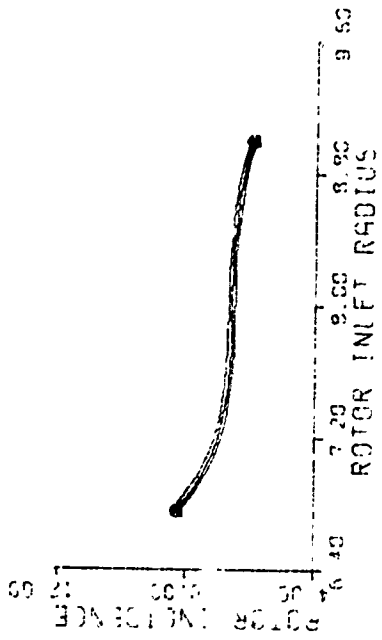


FIGURE 76. ROTOR INCIDENCE VS INLET RADIUS (95% SPEED)

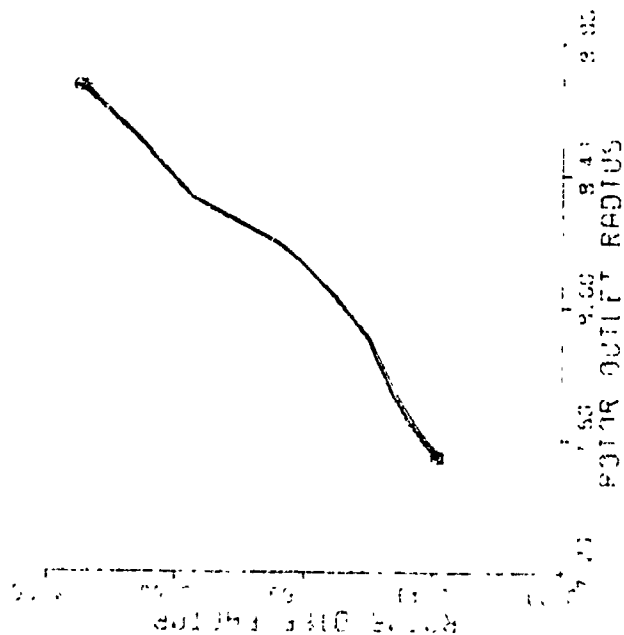


FIGURE 77. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (95% SPEED)

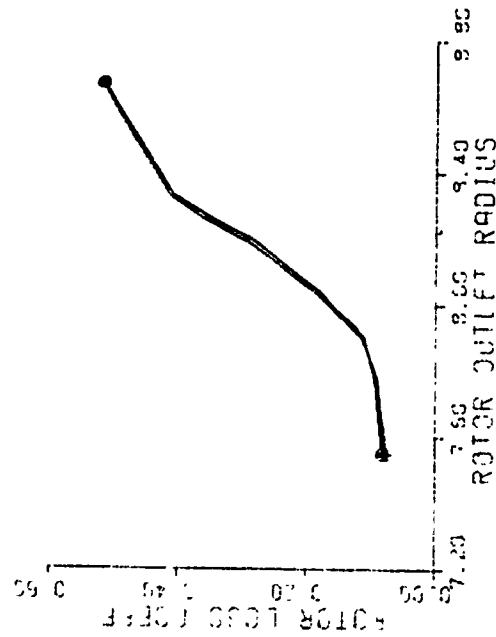


FIGURE 78. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (95% SPEED)

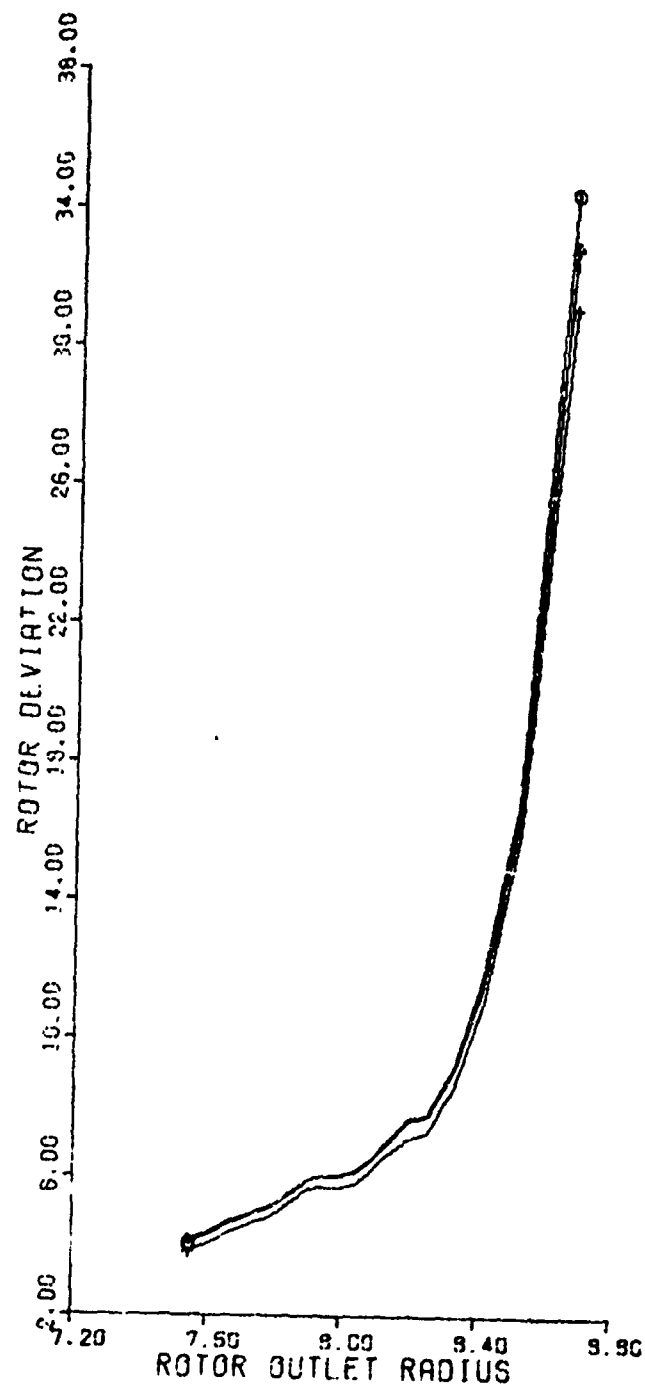


FIGURE 79. ROTOR DEVIATION VS OUTLET RADIUS  
(95% SPEED)

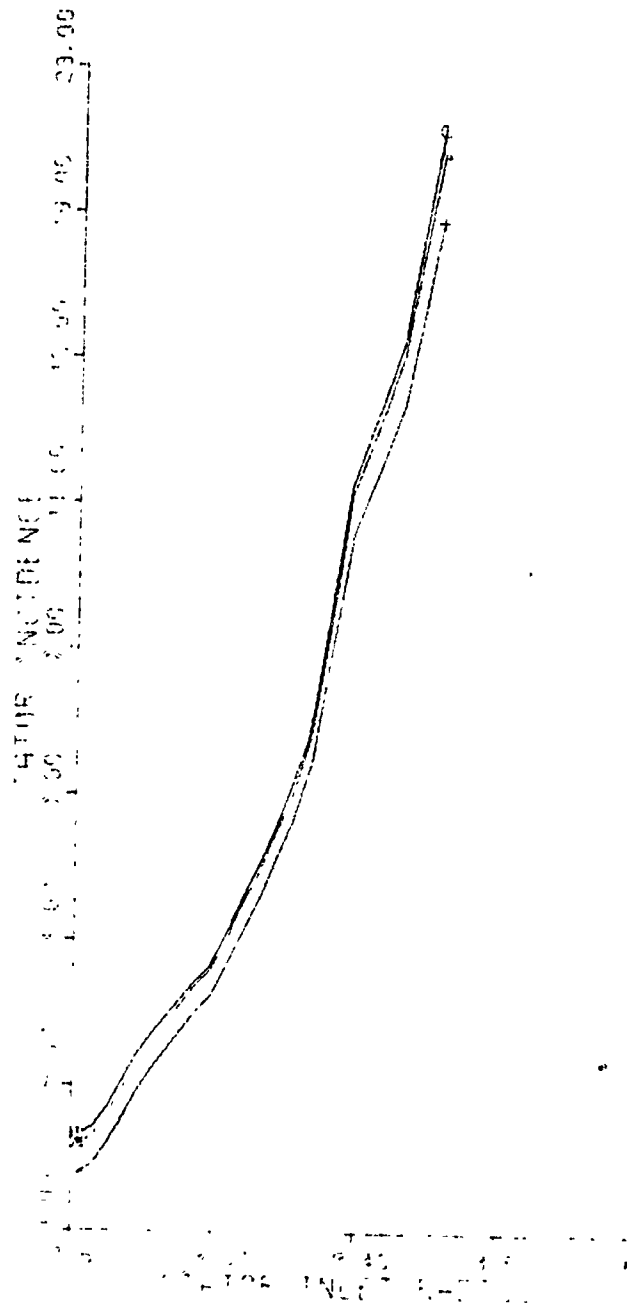


FIGURE 80. STATOR INCIDENCE VS INLET RADIUS  
(95% SPEED)

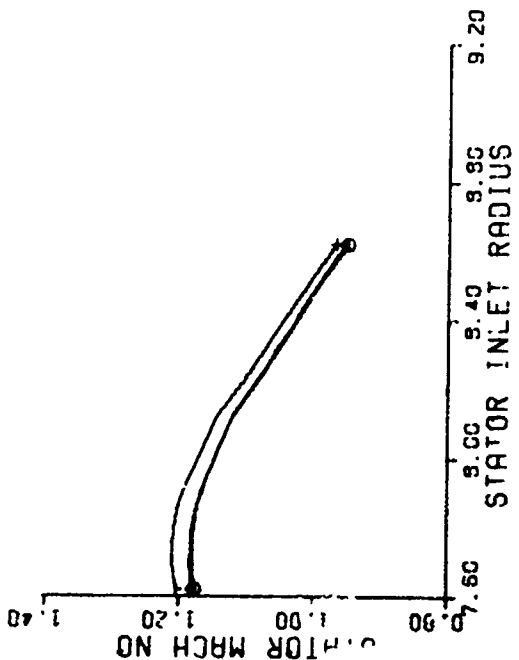


FIGURE 81. STATOR MACH NUMBER VS INLET RADIUS (95% SPEED)

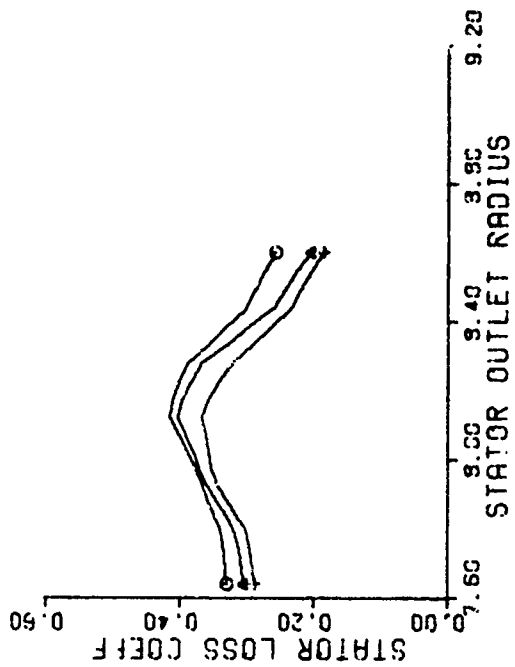


FIGURE 82. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (95% SPEED)

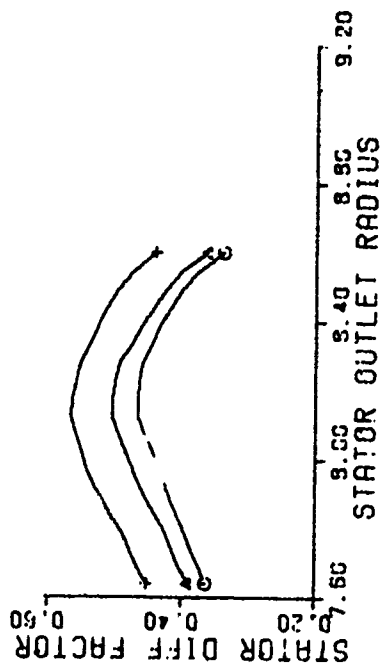


FIGURE 83. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (95% SPEED)

TABLE XIII

IDENTIFICATION OF SYMBOLS  
FOR 100%-SPEED ACROSS-BLADE FIGURES

TEST IDENTIFICATION	SYMBOL
301231515600	⊙
301231615700	▽
301231315200	+
301231415400	×



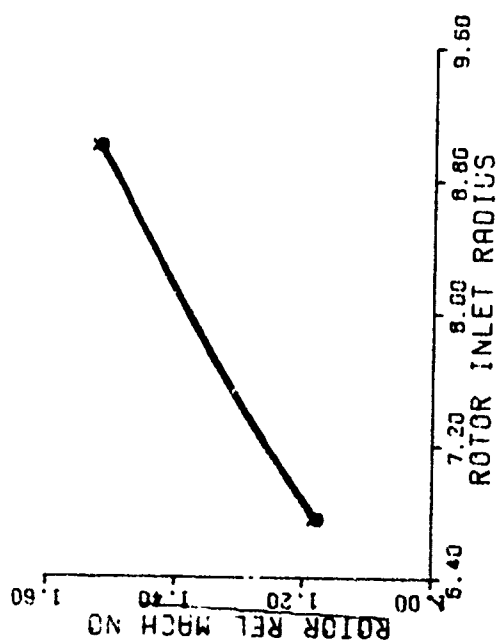


FIGURE 84. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (100% SPEED)

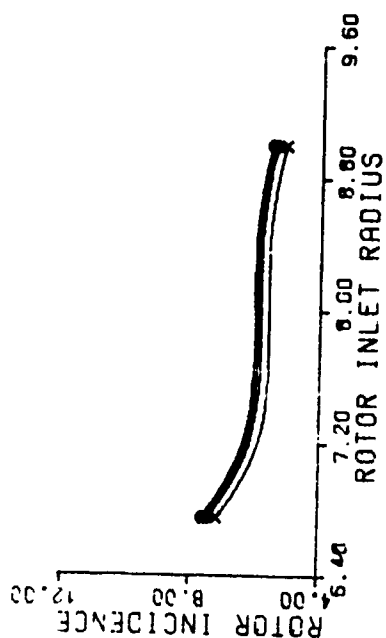


FIGURE 85. ROTOR INCIDENCE VS INLET RADIUS (100% SPEED)

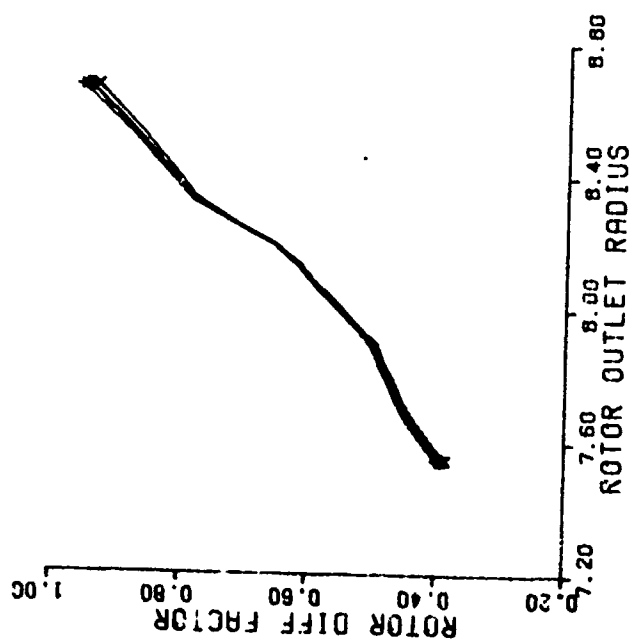


FIGURE 86. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (100% SPEED)

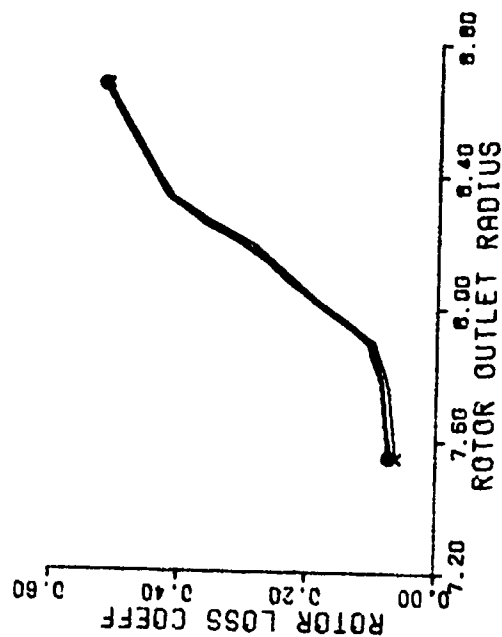


FIGURE 87. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (100% SPEED)

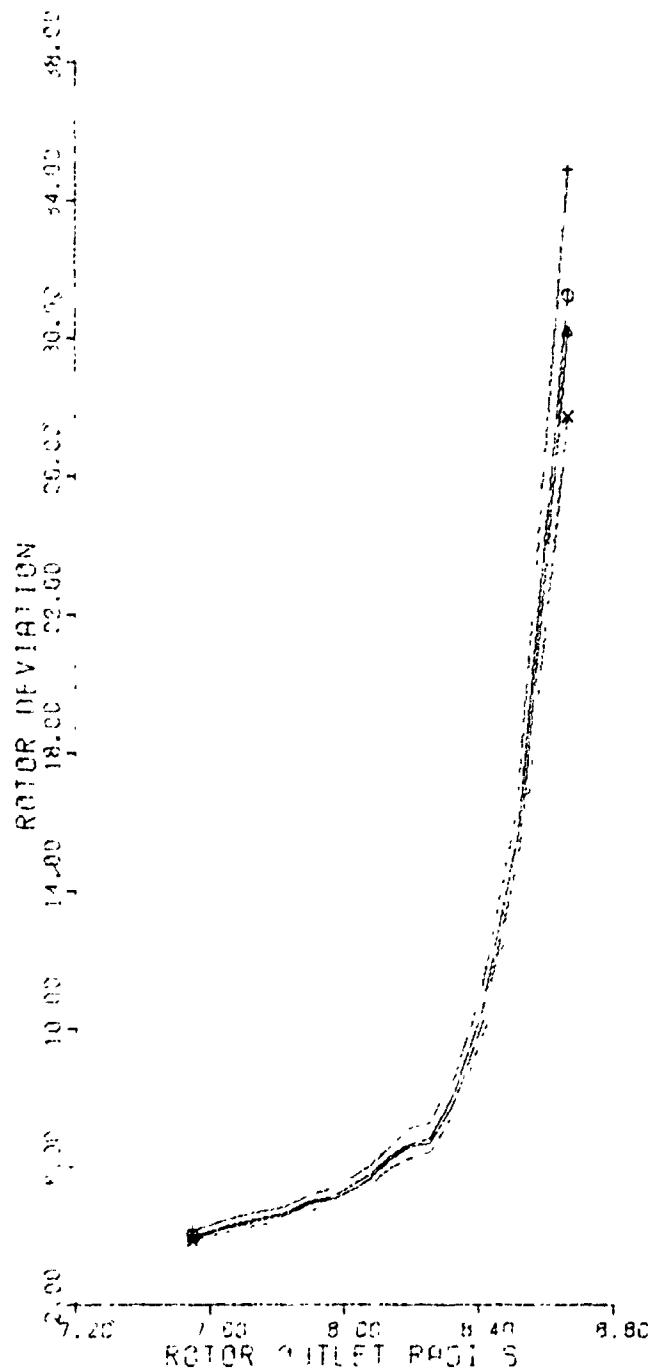


FIGURE 88. ROTOR DEVIATION VS OUTLET RADIUS  
(100% SPEED)

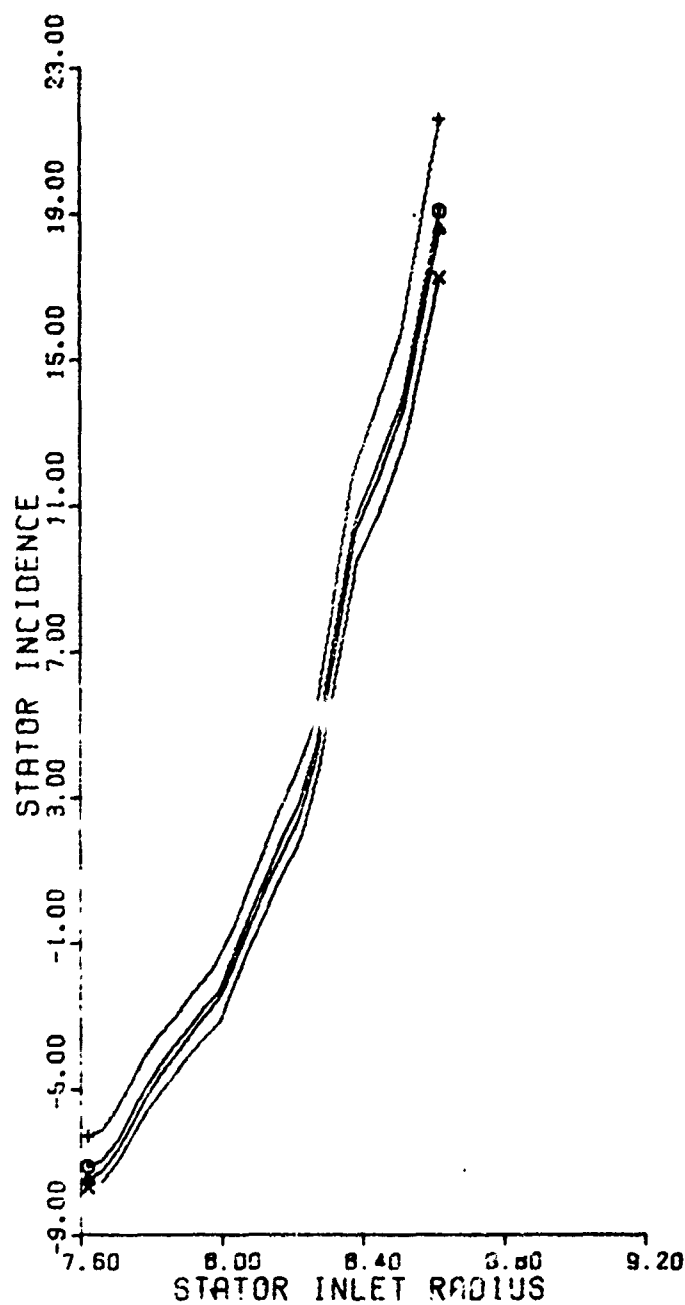


FIGURE 89. STATOR INCIDENCE VS INLET RADIUS  
(100% SPEED)

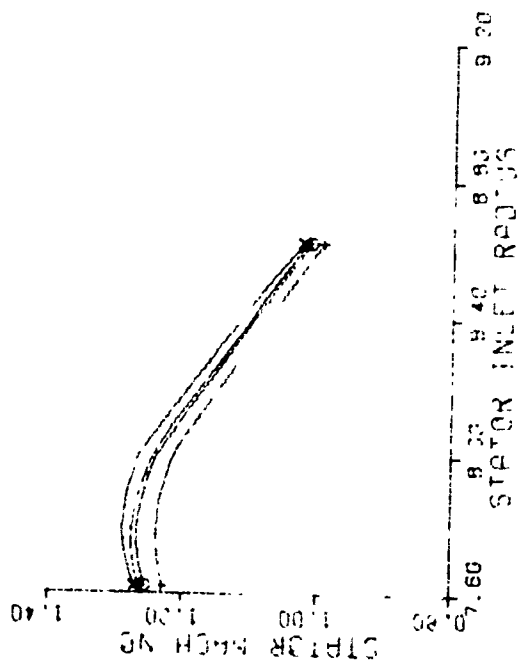


FIGURE 90. STATOR MACH NUMBER VS INLET RADIUS  
(100% SPEED)

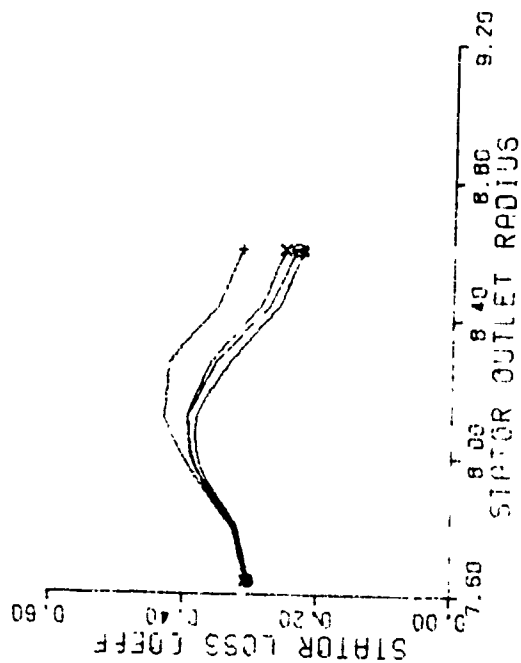


FIGURE 91. STATOR LOSS COEFFICIENT VS OUTLET  
RADIUS (100% SPEED)

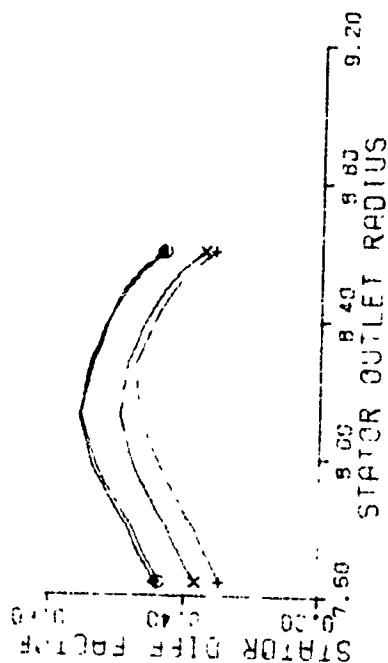


FIGURE 92. STATOR DIFFUSION FACTOR VS OUTLET  
RADIUS (100% SPEED)

**TABLE XIV**

**IDENTIFICATION OF SYMBOLS  
FOR 1024-SPEED ACROSS-BLADE FIGURES**

<b>TEST IDENTIFICATION</b>	<b>SYMBOL</b>
<b>301240815302</b>	<b>⊙</b>
<b>301240915602</b>	<b>▽</b>

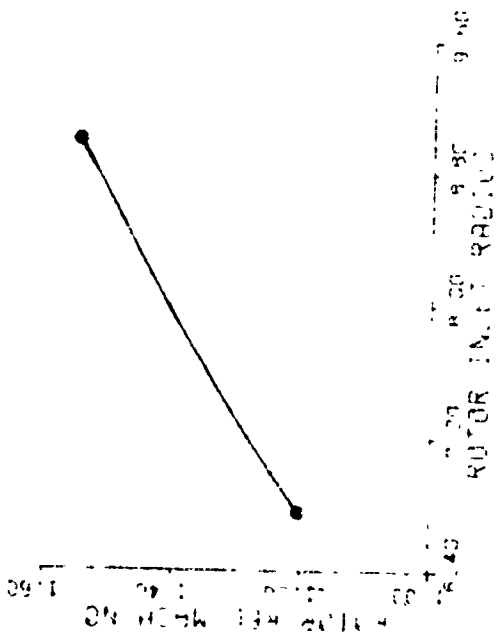


FIGURE 93. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (102% SPEED)

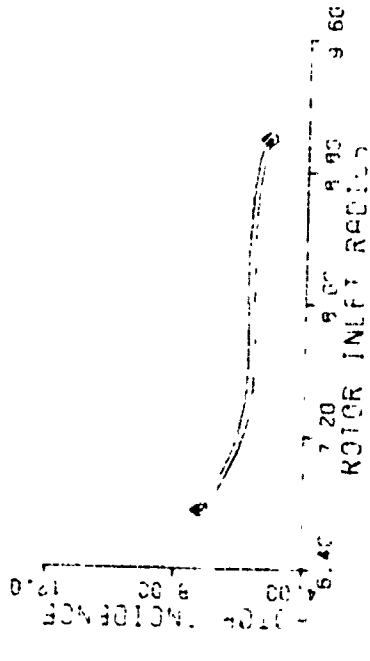


FIGURE 94. ROTOR INCIDENCE VS INLET RADIUS (102% SPEED)

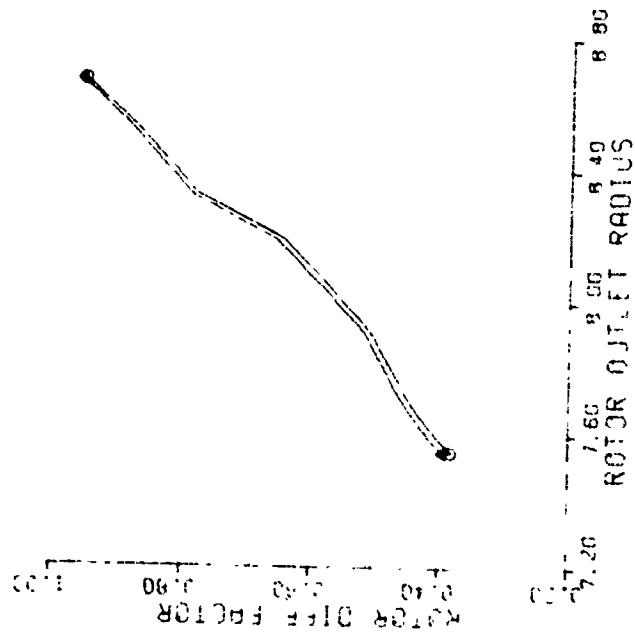


FIGURE 95. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (102% SPEED)

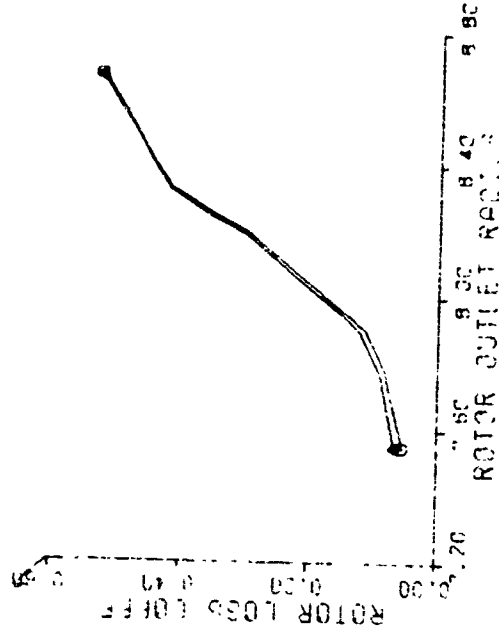


FIGURE 96. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (102% SPEED)

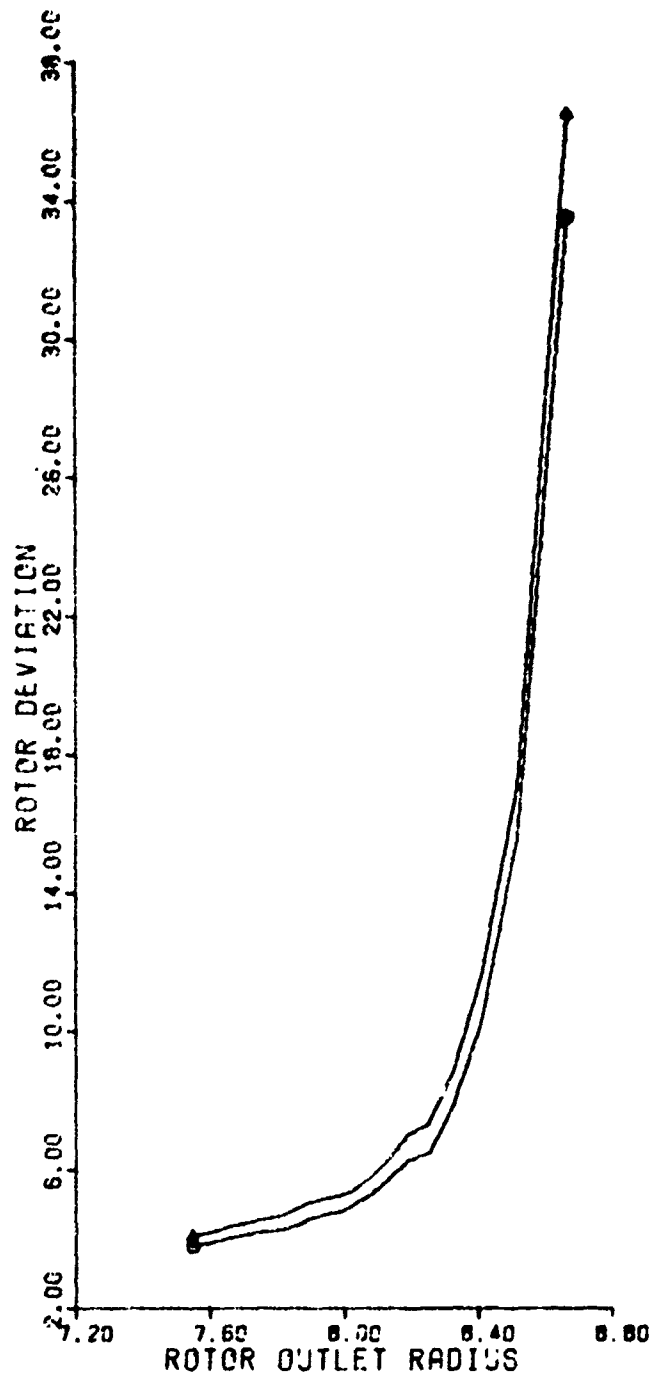


FIGURE 97. ROTOR DEVIATION VS OUTLET RADIUS  
(102% SPEED)

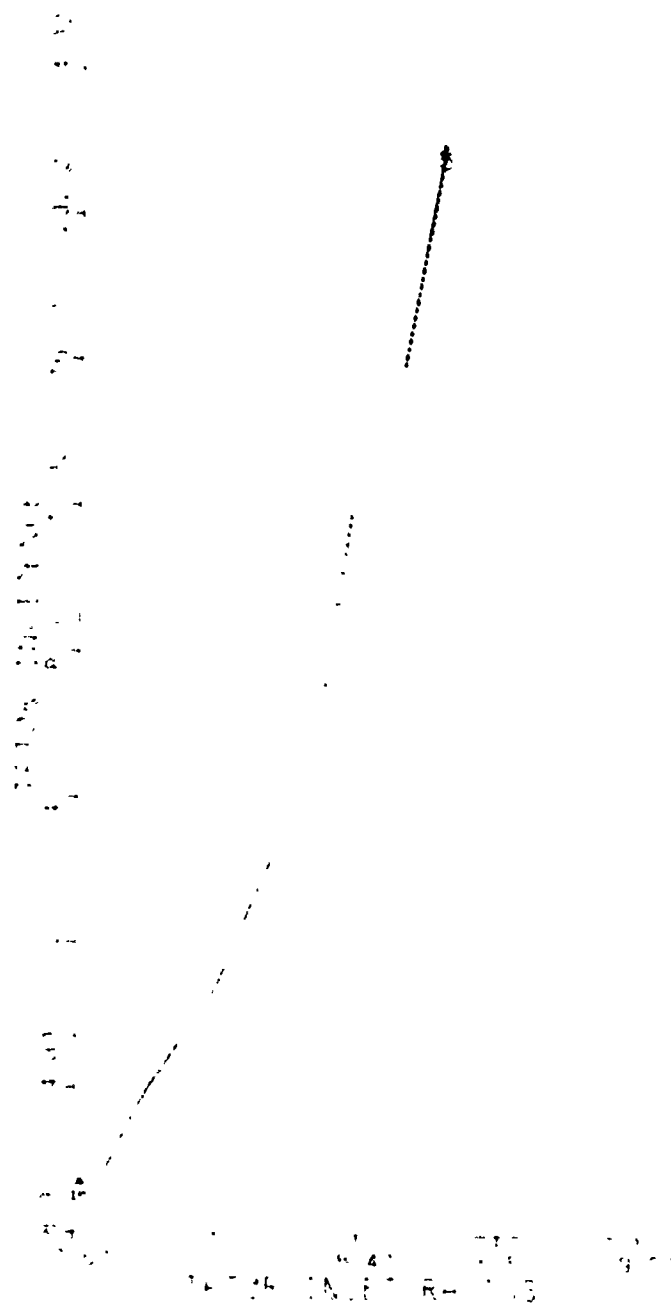


FIGURE 98. STATOR INCIDENCE VS INLET RADIUS  
(102% SPEED)



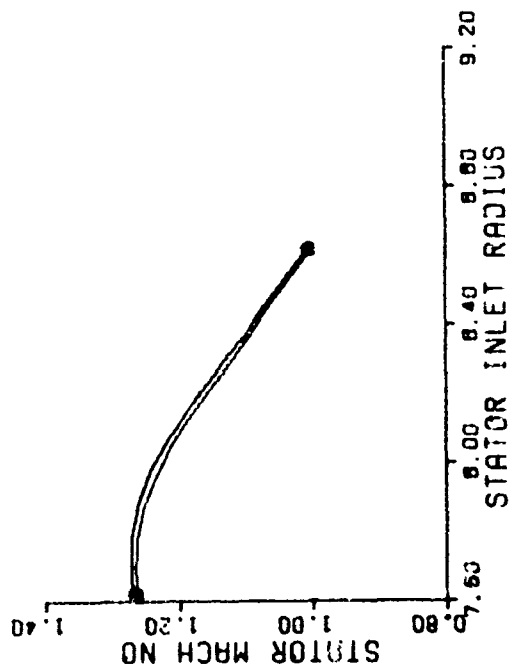


FIGURE 99. STATOR MACH NUMBER VS INLET RADIUS  
(102% SPEED)

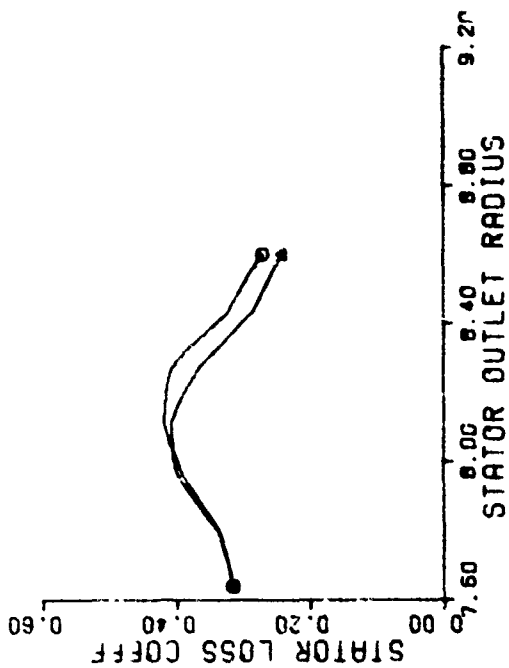


FIGURE 100. STATOR LOSS COEFFICIENT VS OUTLET  
RADIUS (102% SPEED)

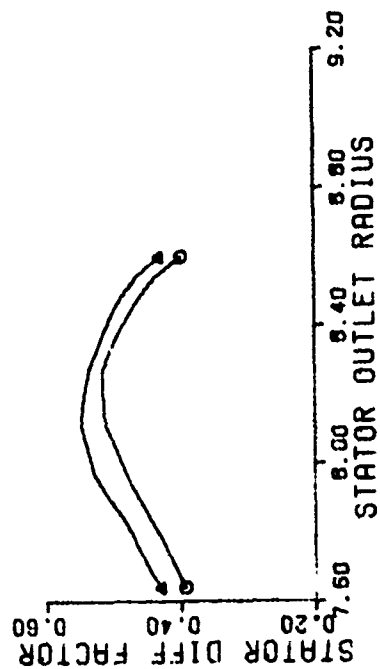


FIGURE 101. STATOR DIFFUSION FACTOR VS OUTLET  
RADIUS (10% SPEED)

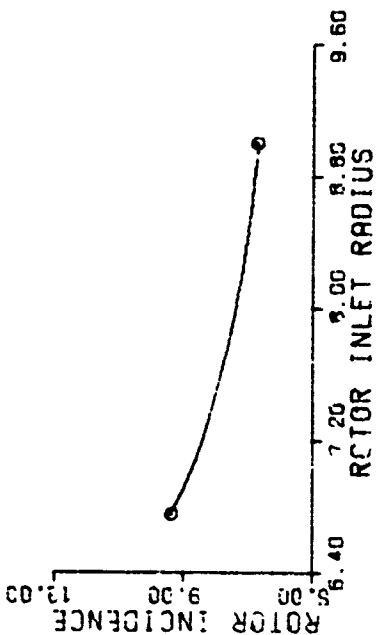


FIGURE 103. ROTOR INCIDENCE VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

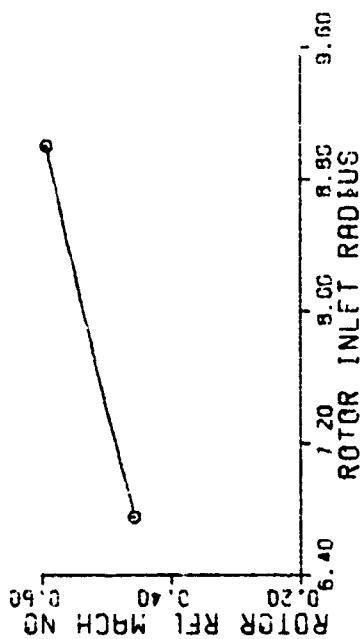


FIGURE 102. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

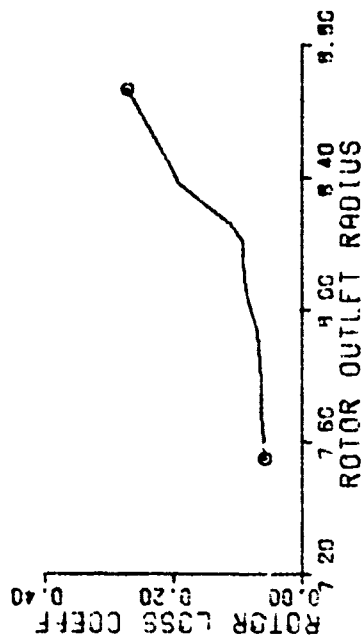


FIGURE 105. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

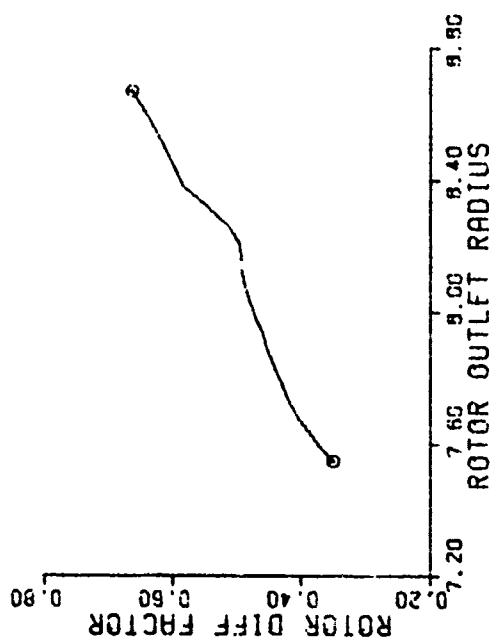


FIGURE 104. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

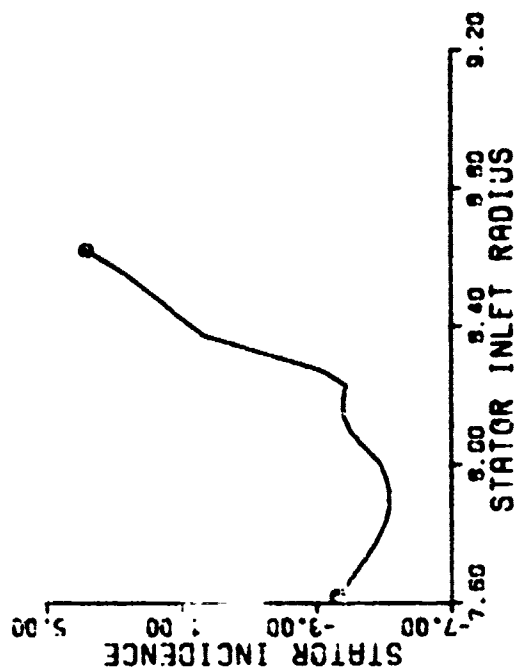


FIGURE 107. STATOR INCIDENCE VS INLET RADIUS (WITHIN-  
BLADE ANALYSIS, 40% SPEED)

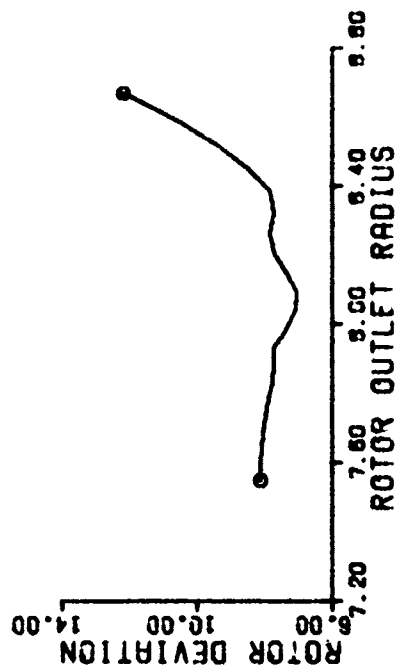


FIGURE 106. ROTOR DEVIATION VS OUTLET RADIUS (WITHIN-  
BLADE ANALYSIS, 40% SPEED)

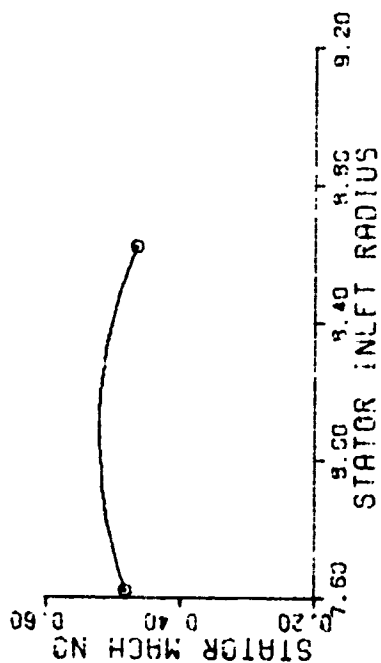


FIGURE 108. STATOR MACH NUMBER VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

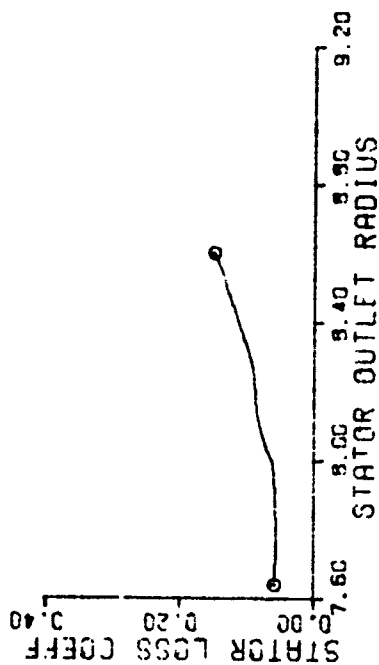


FIGURE 109. STATOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

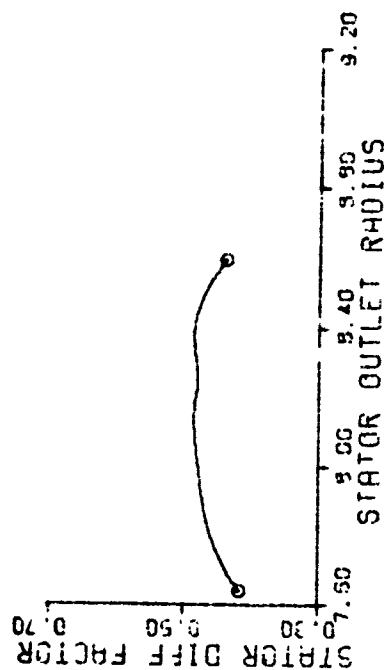


FIGURE 110. STATOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 40% SPEED)

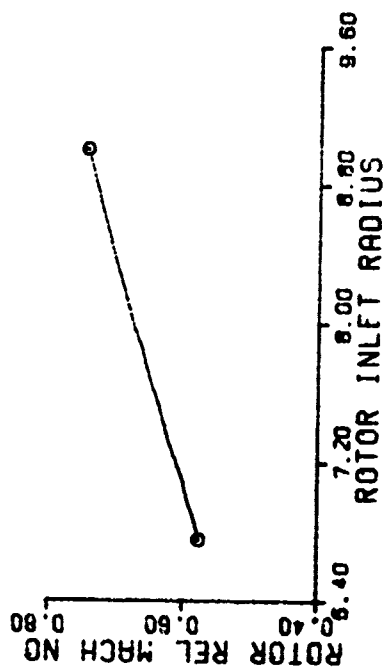


FIGURE 111. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS (WITHIN BLADE ANALYSIS, 50% SPEED)

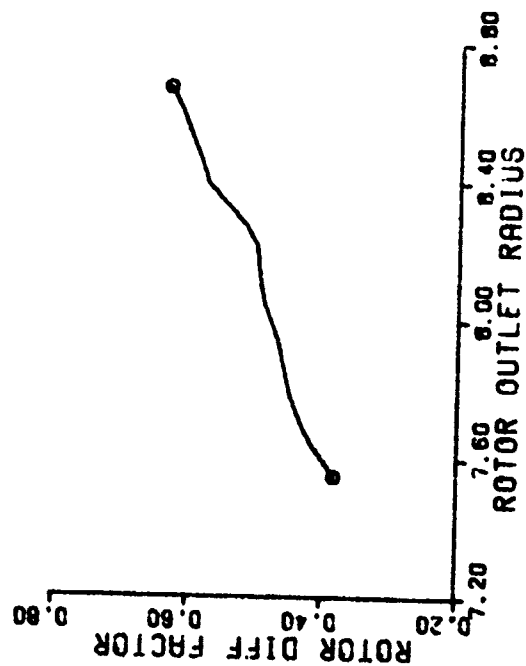


FIGURE 113. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 50% SPEED)

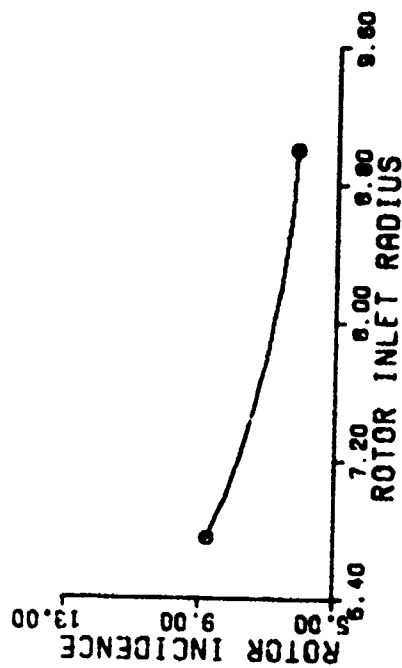


FIGURE 112. ROTOR INCIDENCE VS INLET RADIUS (WITHIN-BLADE ANALYSIS, 50% SPEED)

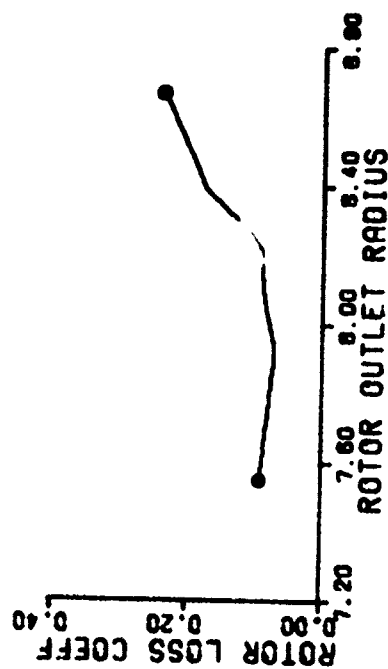


FIGURE 114. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS (WITHIN-BLADE ANALYSIS, 50% SPEED)

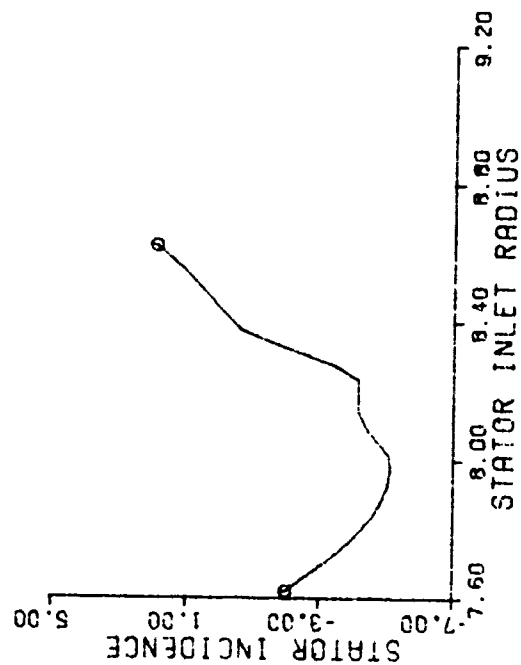


FIGURE 116. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 50% SPEED)

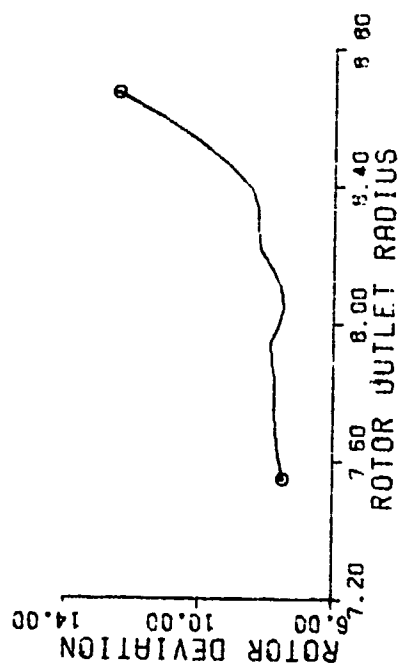


FIGURE 115. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 50% SPEED)

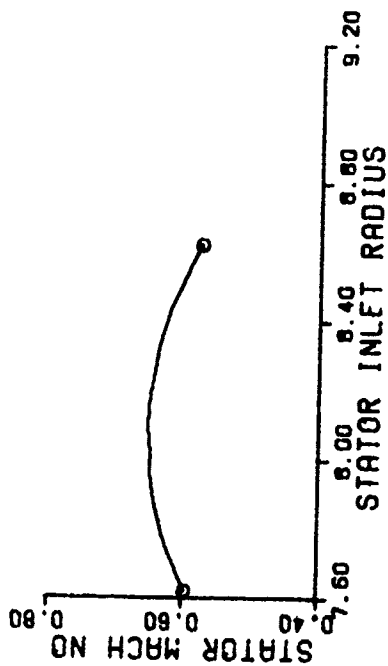


FIGURE 117. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 50% SPEED)

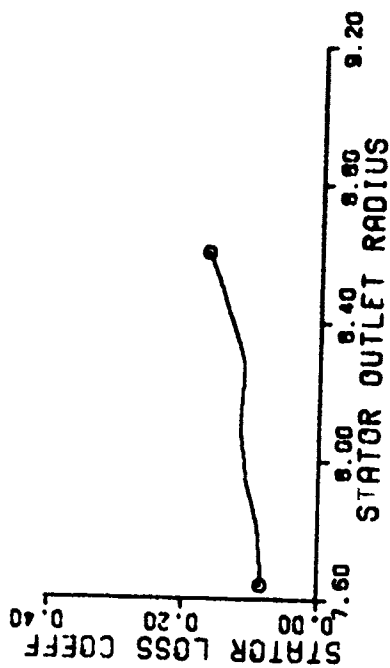


FIGURE 118. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 50% SPEED)

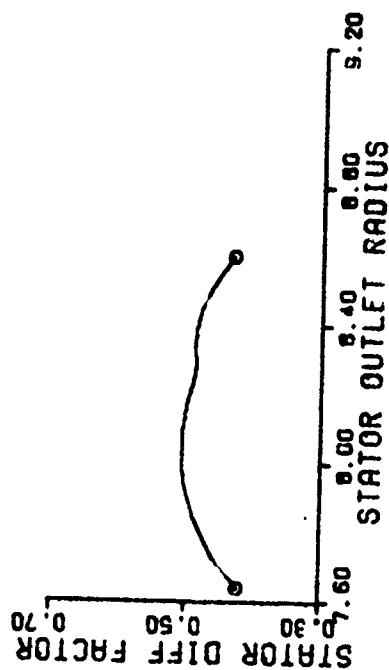


FIGURE 119. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 50% SPEED)

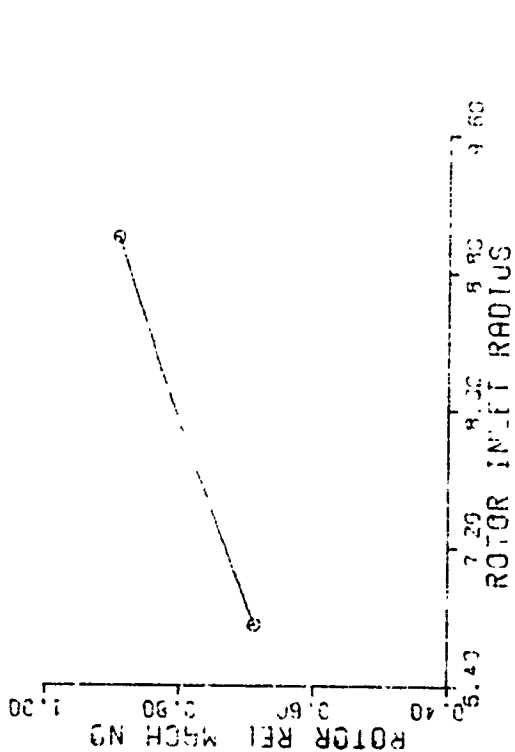


FIGURE 120. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

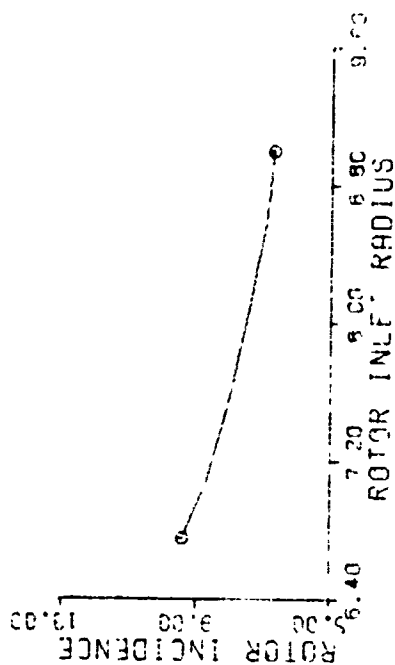


FIGURE 121. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

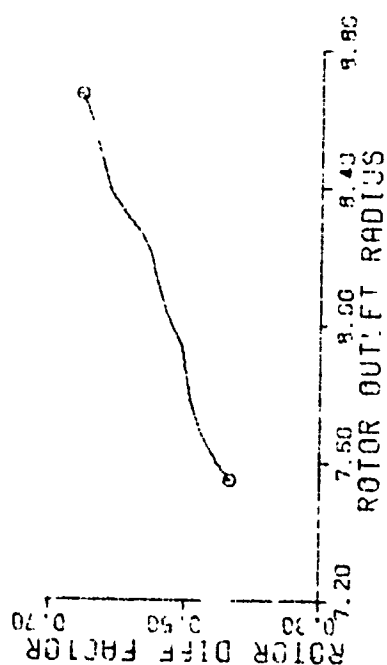


FIGURE 122. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

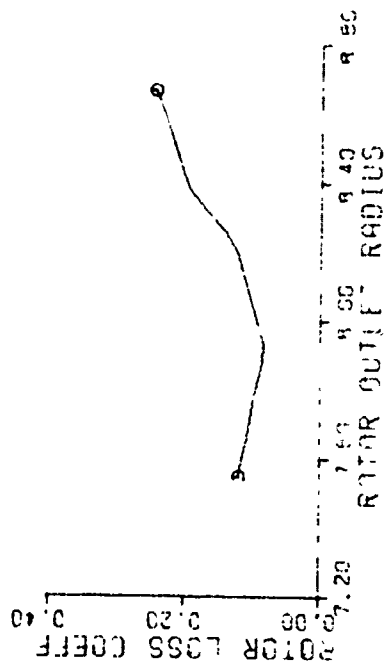


FIGURE 123. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)



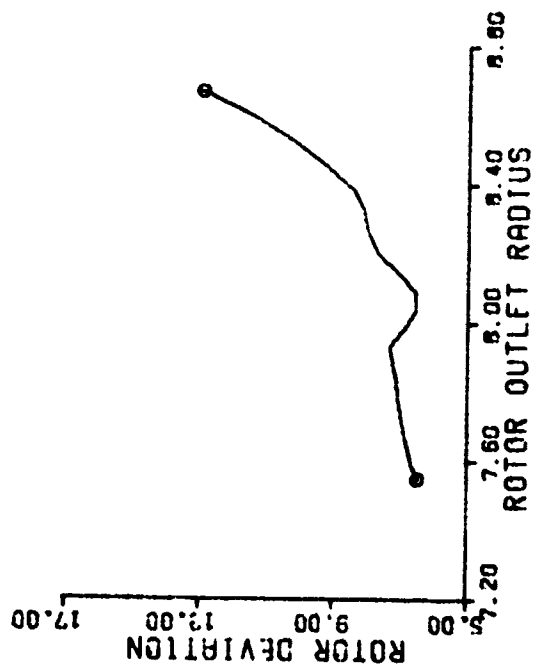


FIGURE 124. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

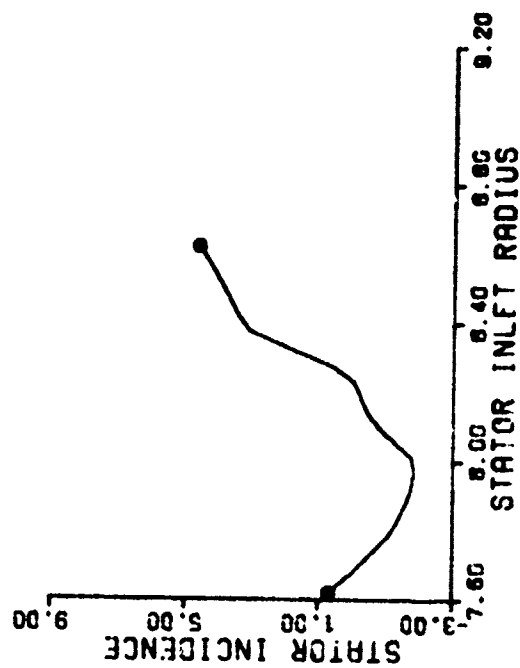


FIGURE 125. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

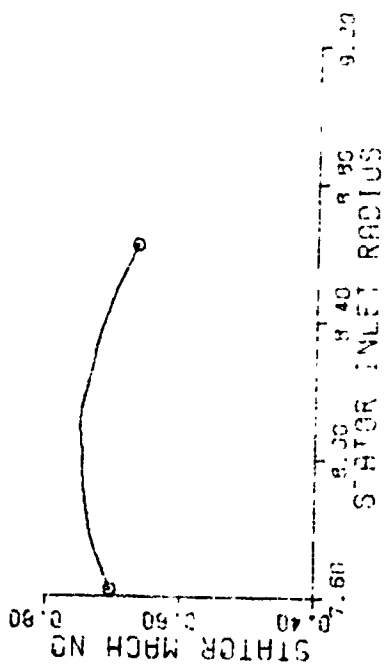


FIGURE 126. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

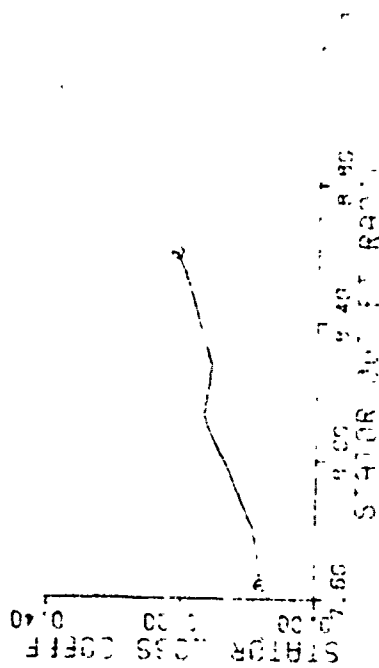


FIGURE 127. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

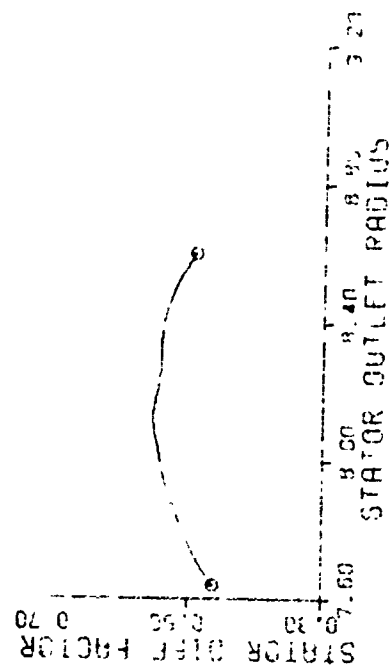


FIGURE 128. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 60% SPEED)

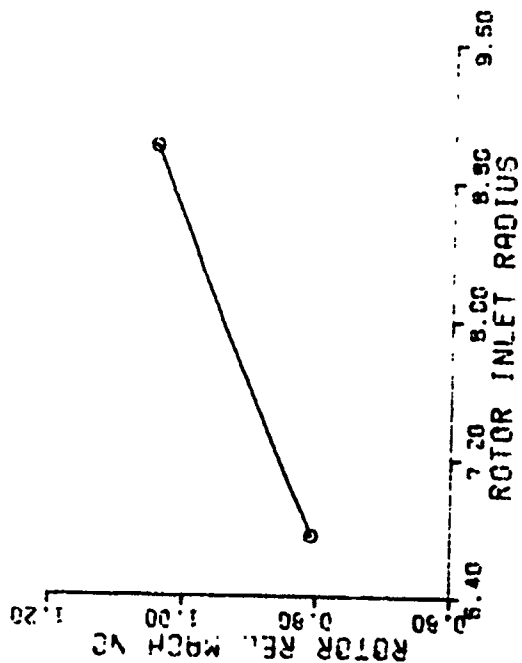


FIGURE 129. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

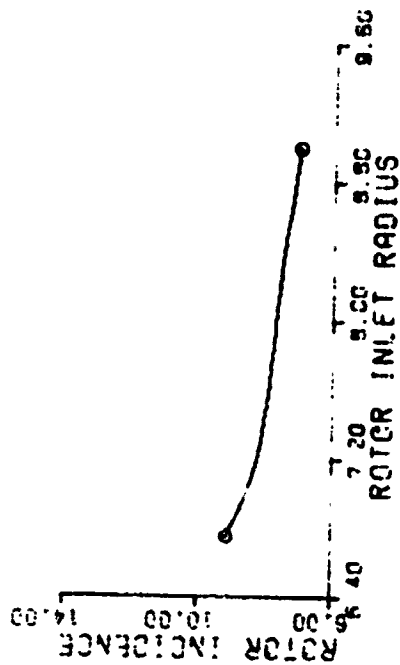


FIGURE 130. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

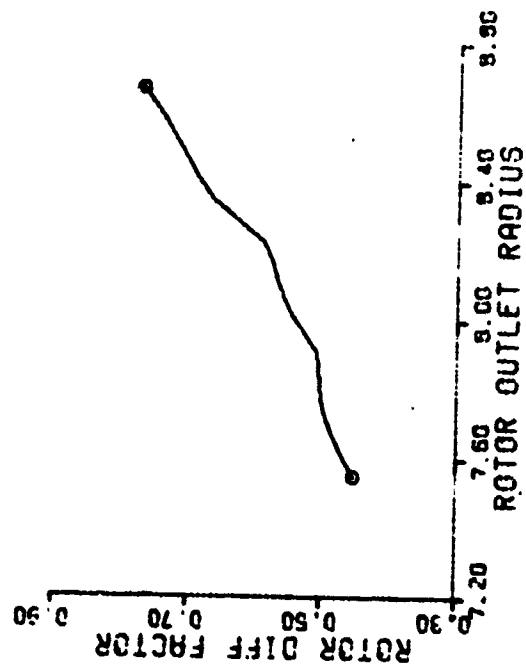


FIGURE 131. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

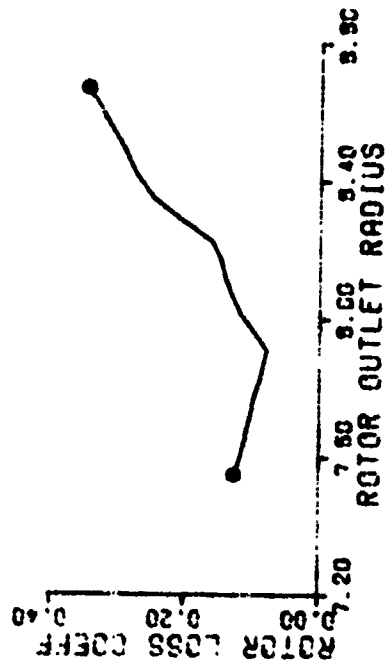


FIGURE 132. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

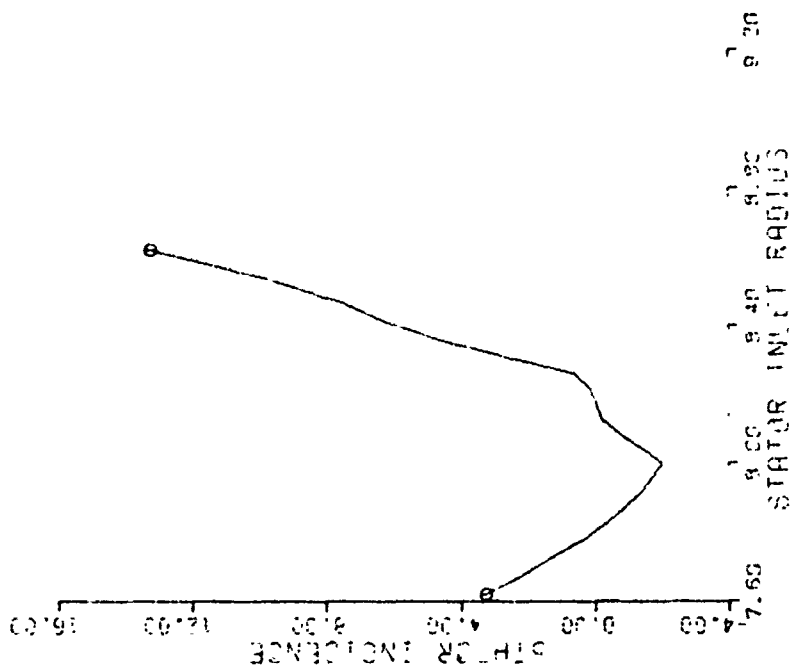


FIGURE 133. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

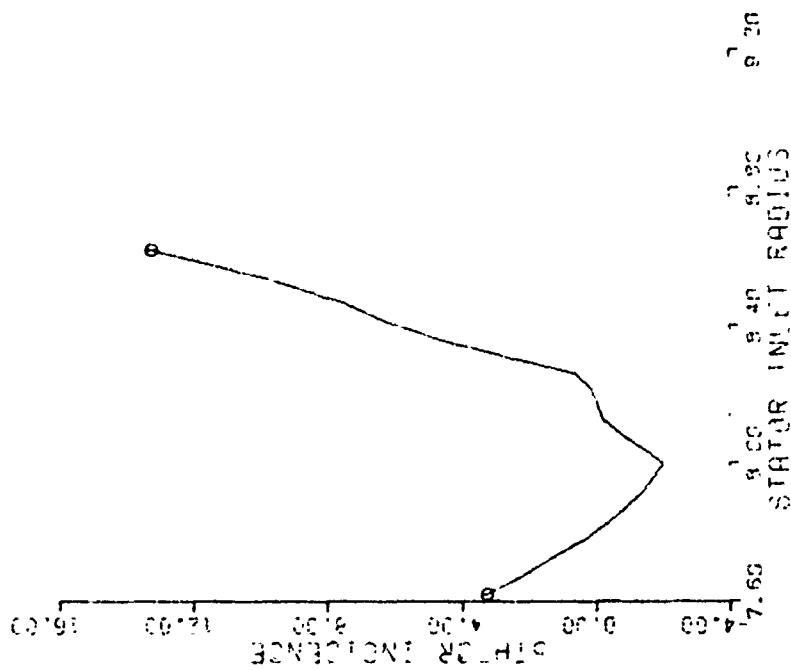


FIGURE 134. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

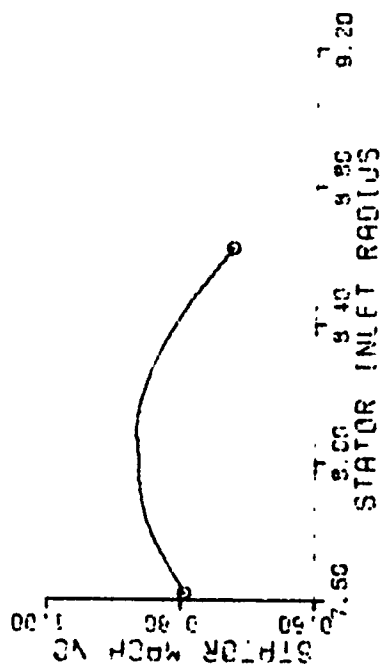


FIGURE 135. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

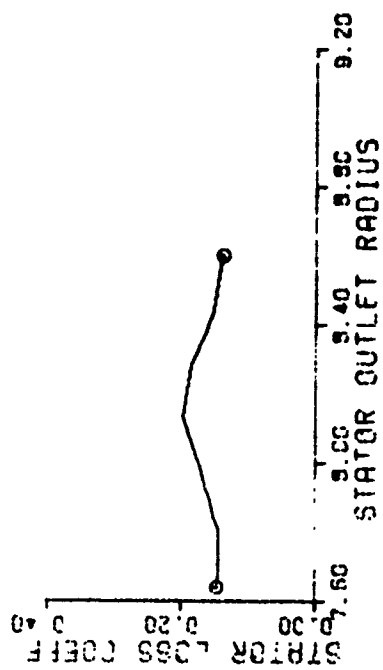


FIGURE 136. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

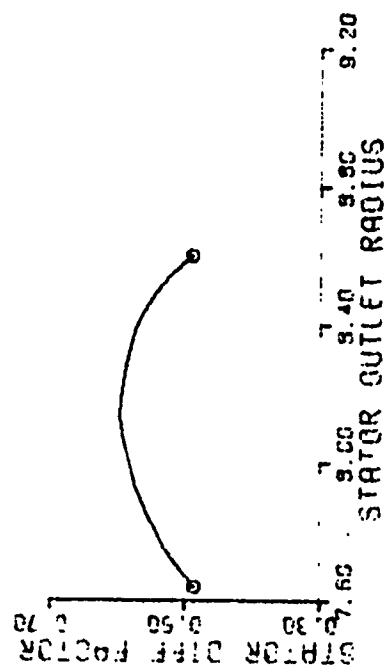


FIGURE 137. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 70% SPEED)

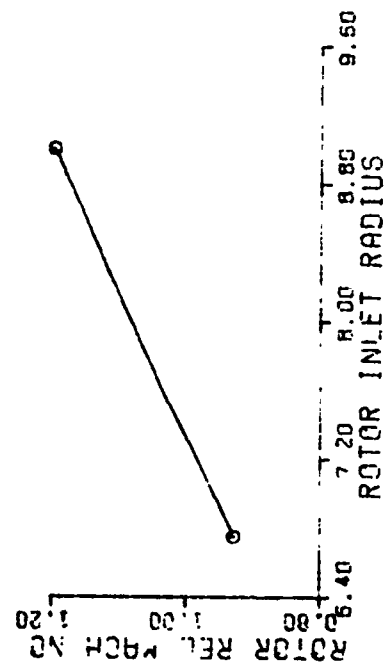


FIGURE 138. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

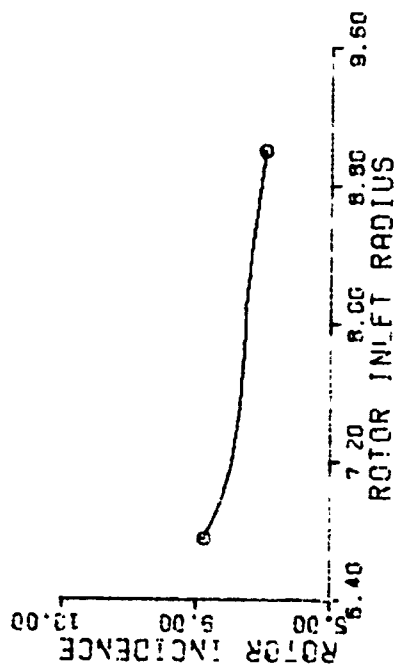


FIGURE 139. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

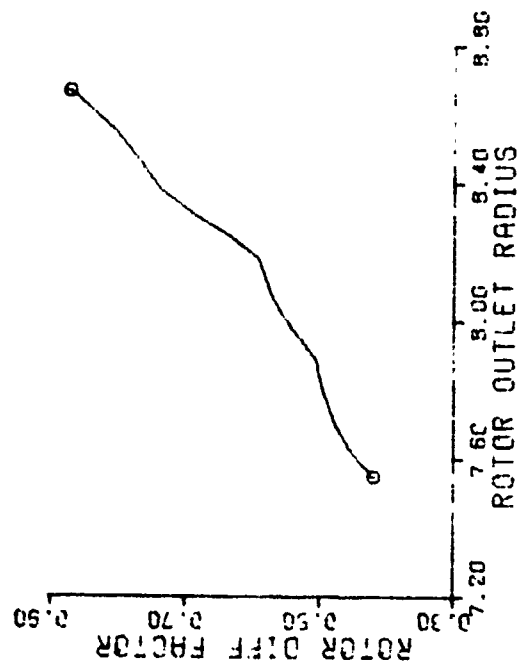


FIGURE 140. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

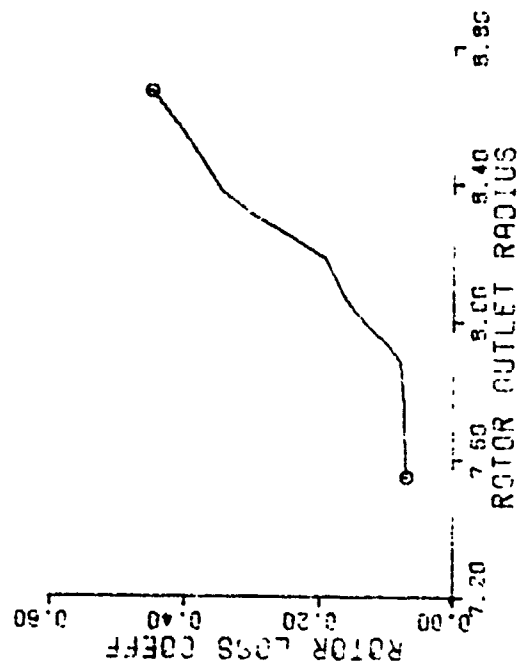


FIGURE 141. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

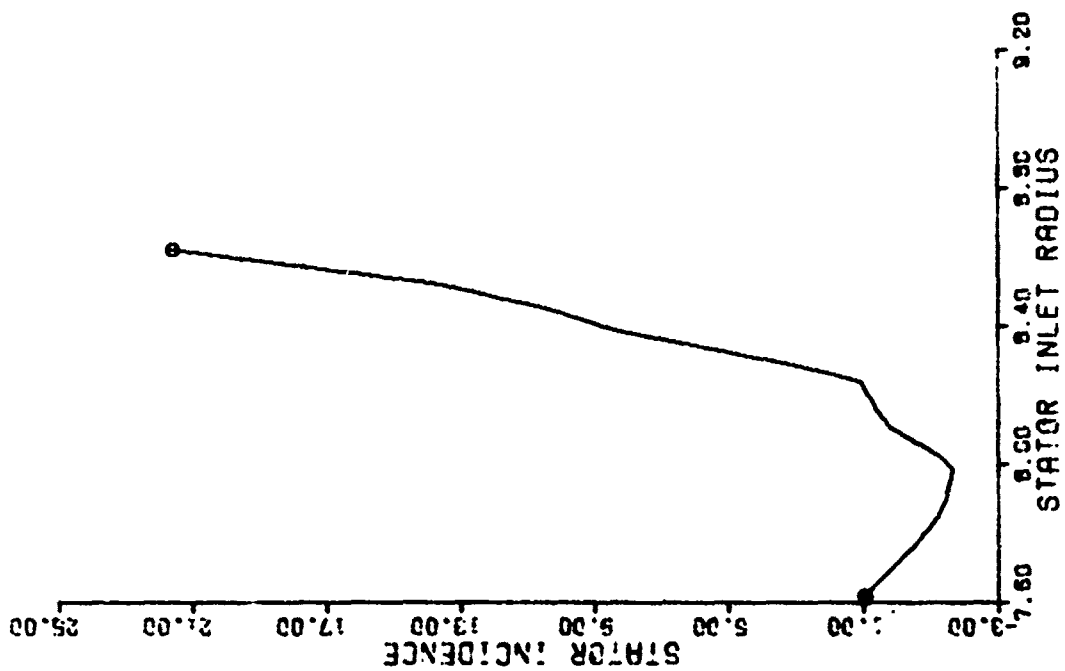


FIGURE 143. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

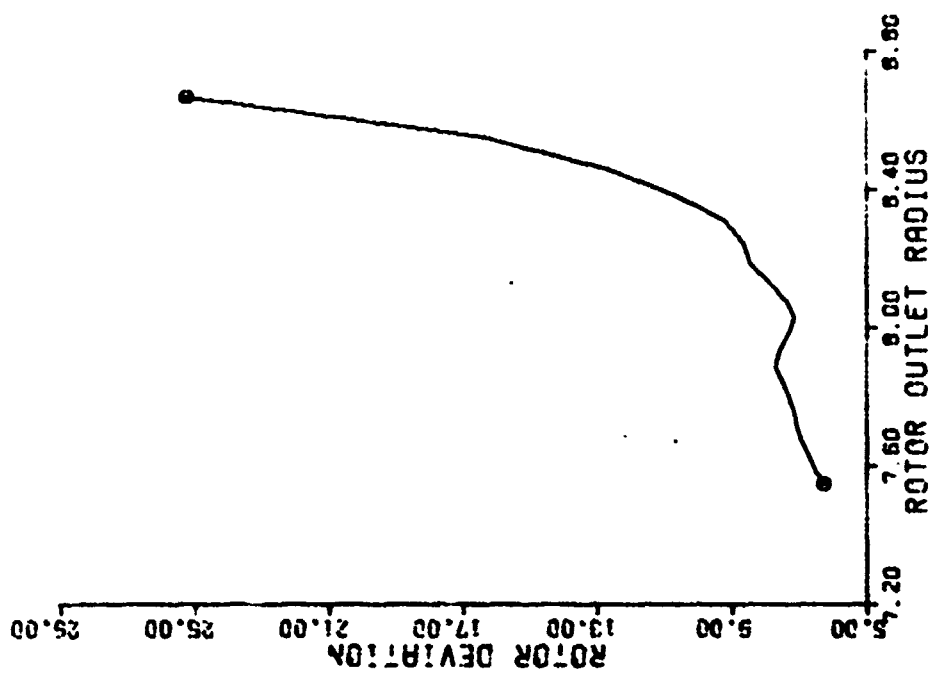


FIGURE 142. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

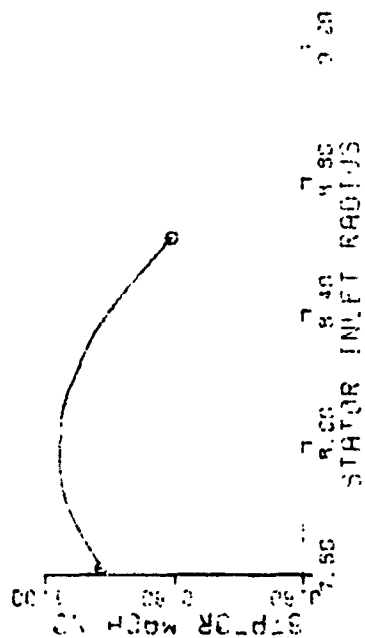


FIGURE 141. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

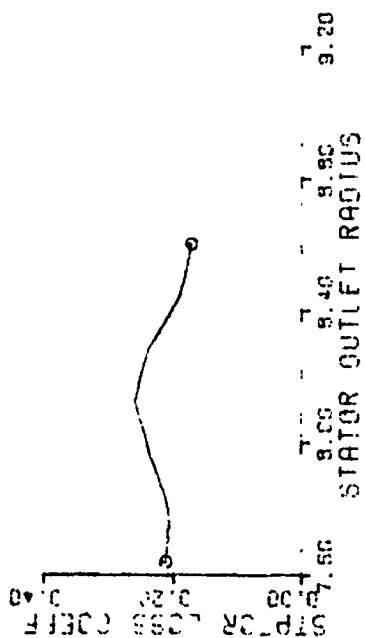


FIGURE 145. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)

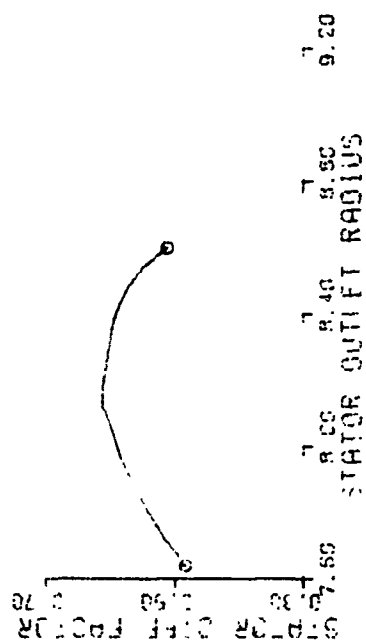


FIGURE 146. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 80% SPEED)



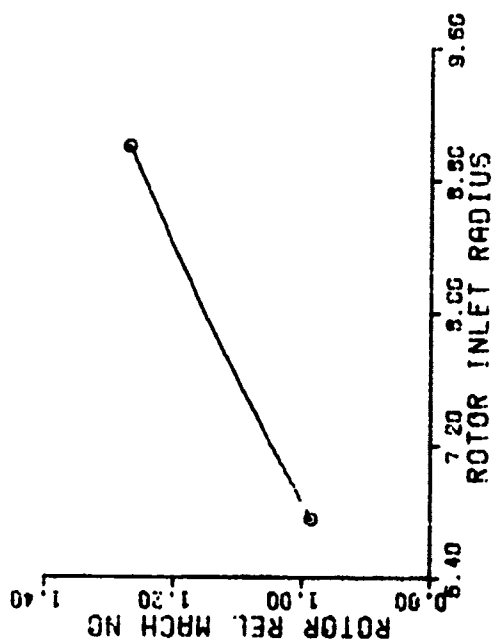


FIGURE 147. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

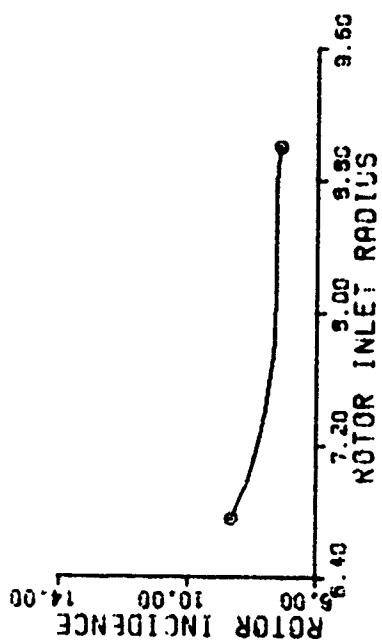


FIGURE 148. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

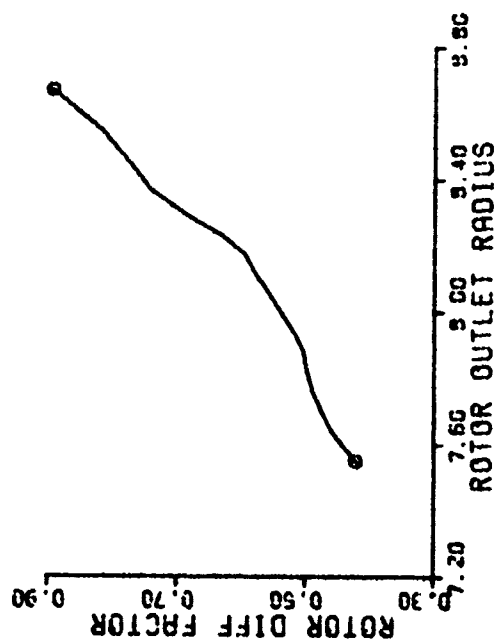


FIGURE 149. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

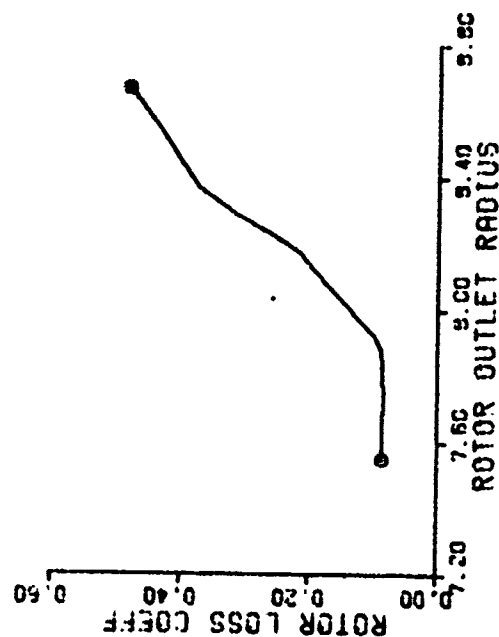


FIGURE 150. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

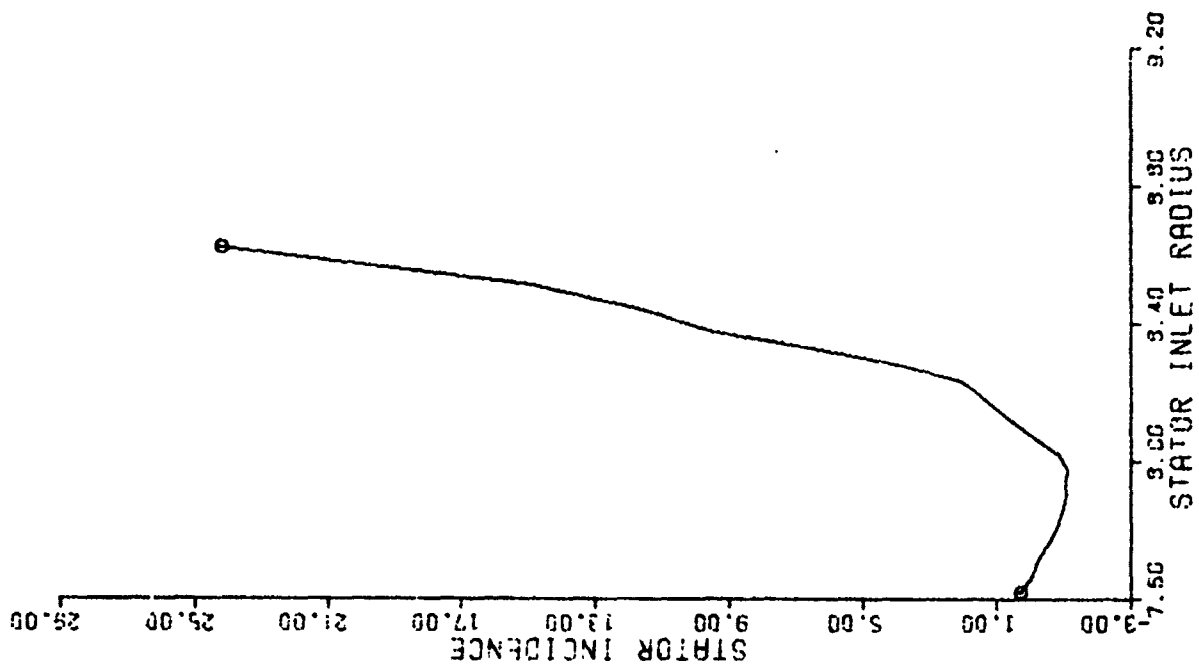


FIGURE 151. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

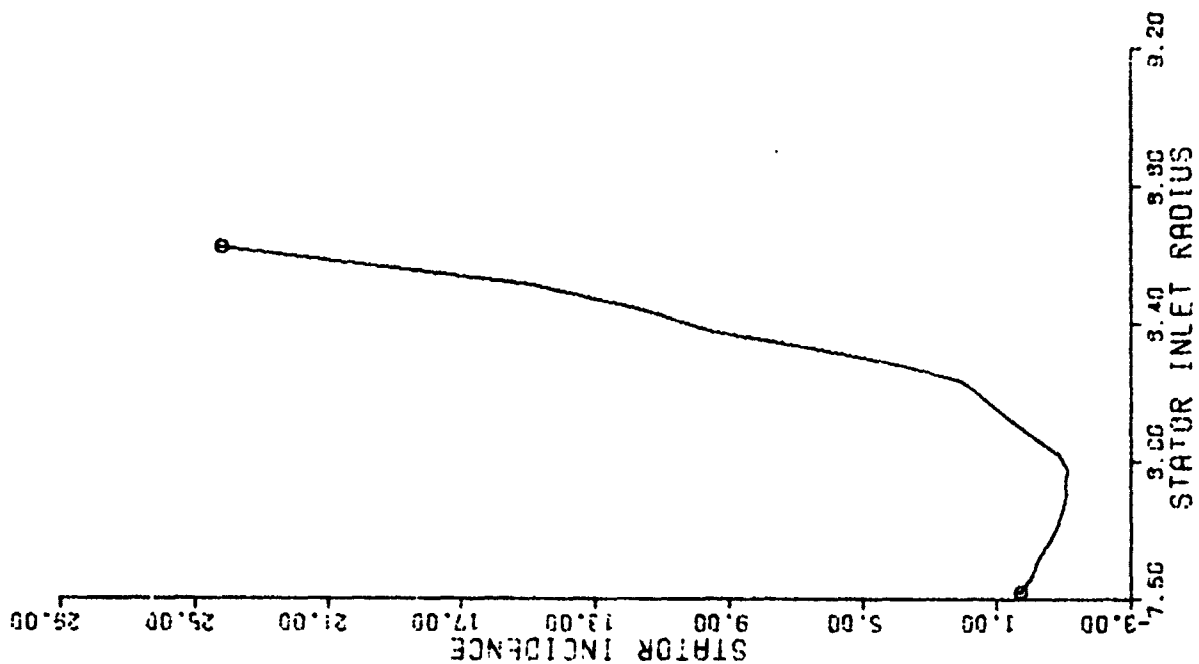


FIGURE 152. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

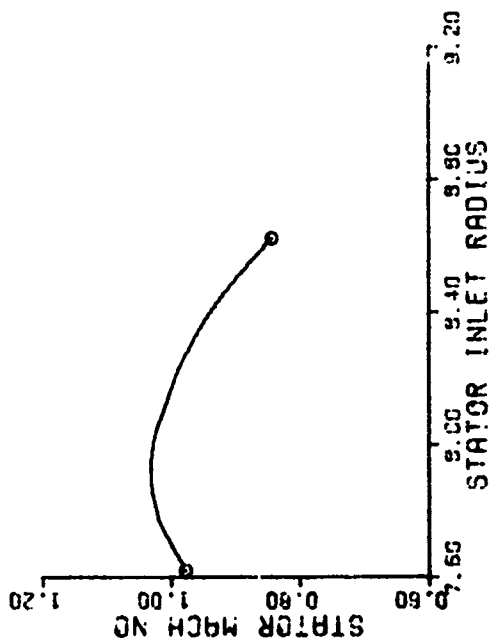


FIGURE 153. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

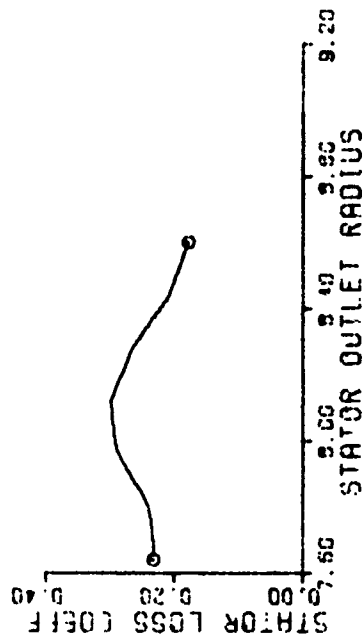


FIGURE 154. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

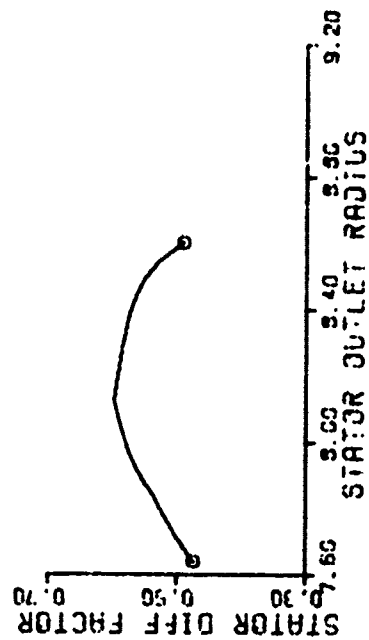


FIGURE 155. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 85% SPEED)

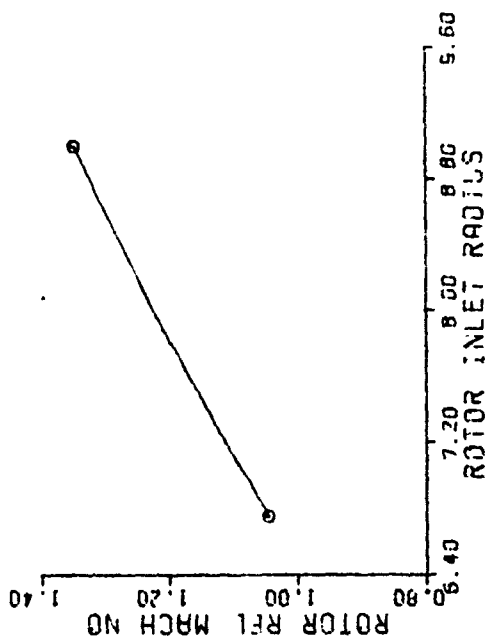


FIGURE 156. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

FIGURE 157. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

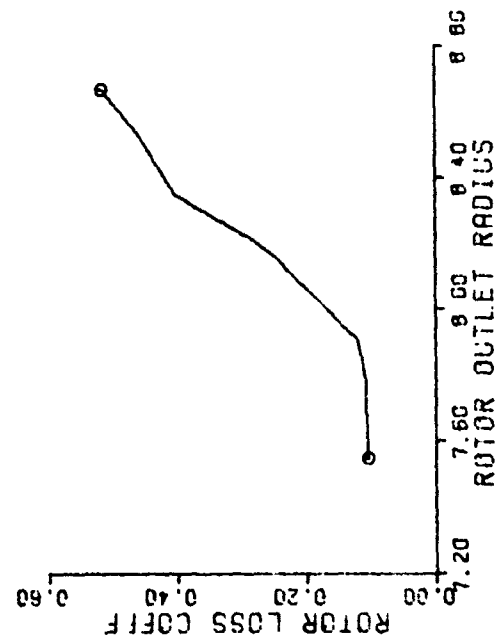
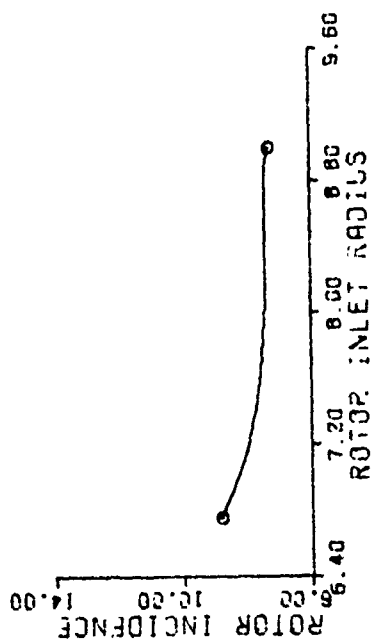


FIGURE 159. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

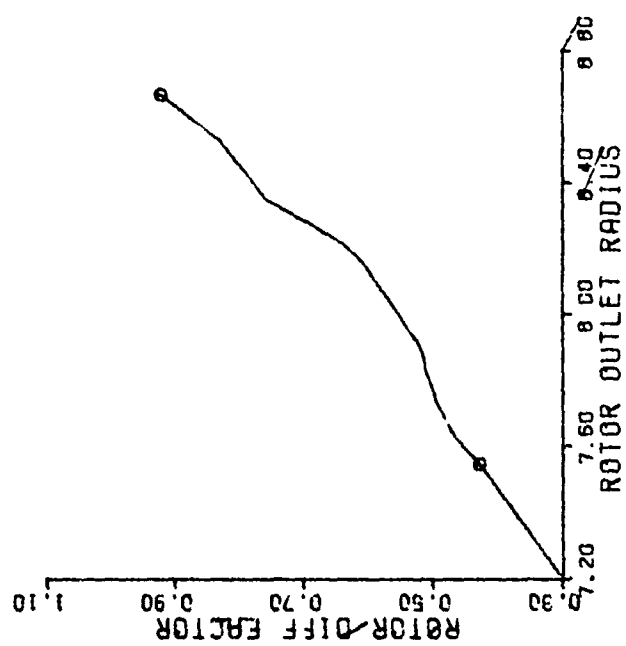


FIGURE 158. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

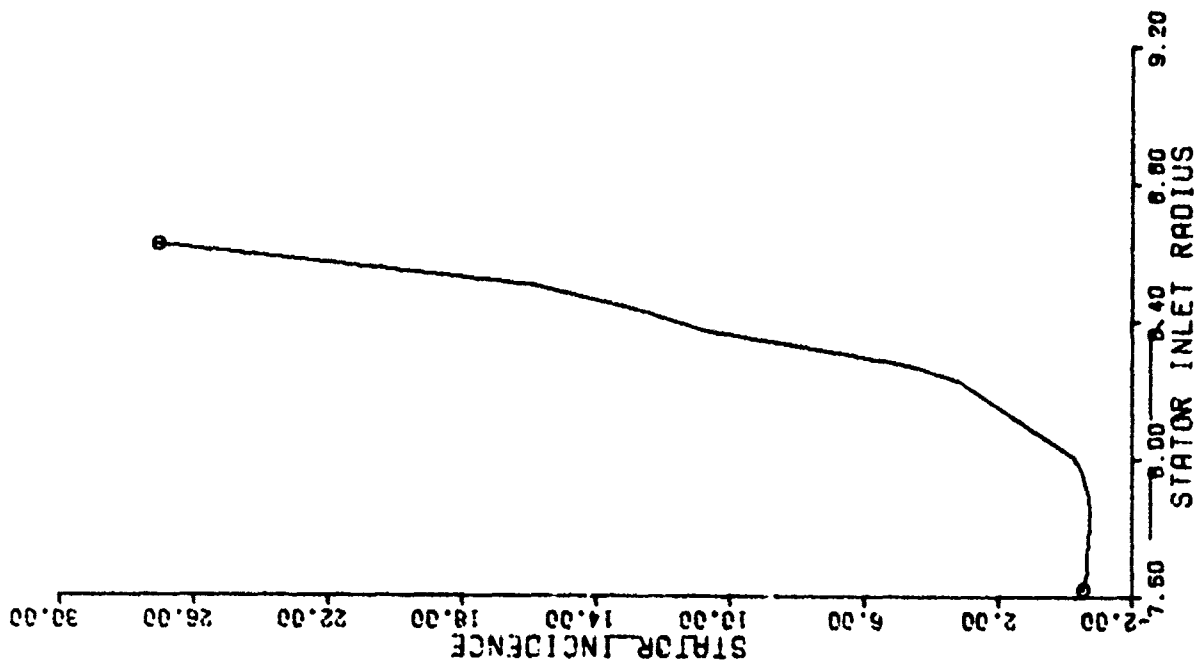


FIGURE 161. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

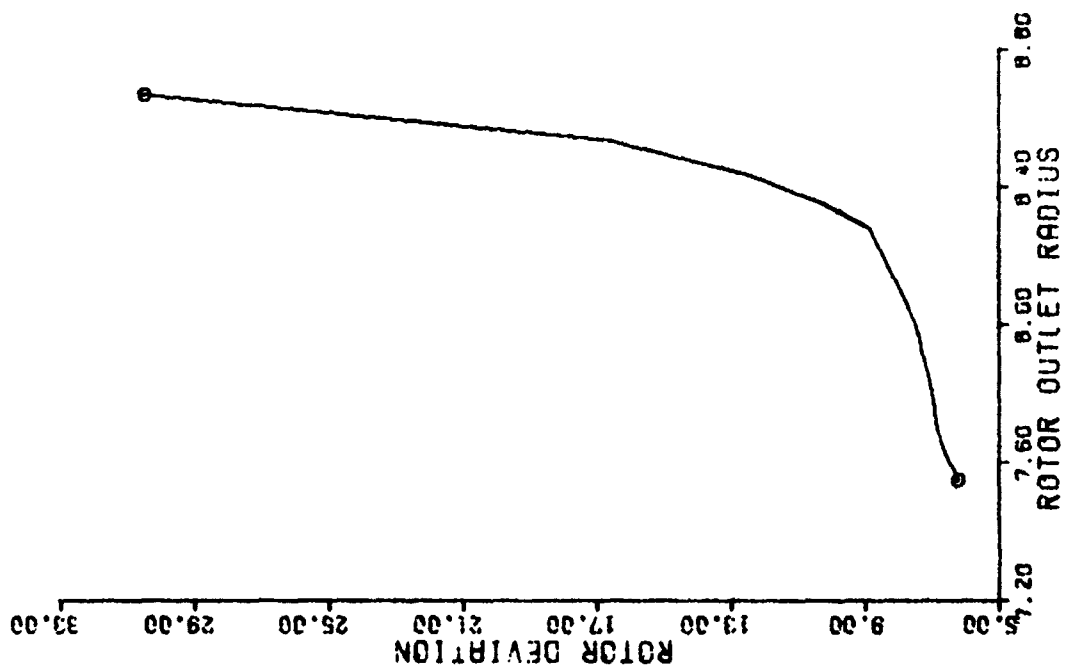


FIGURE 160. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

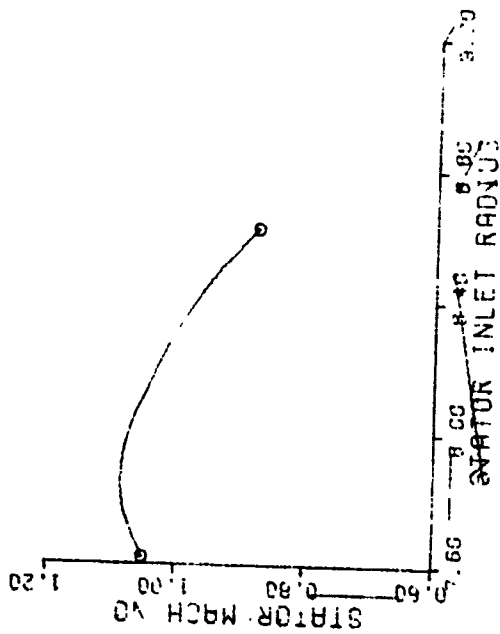


FIGURE 162. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

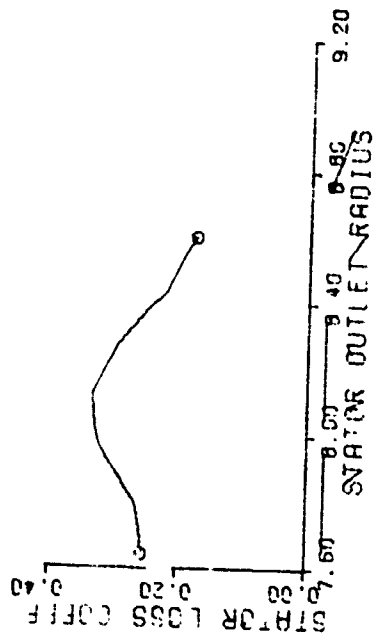


FIGURE 163. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

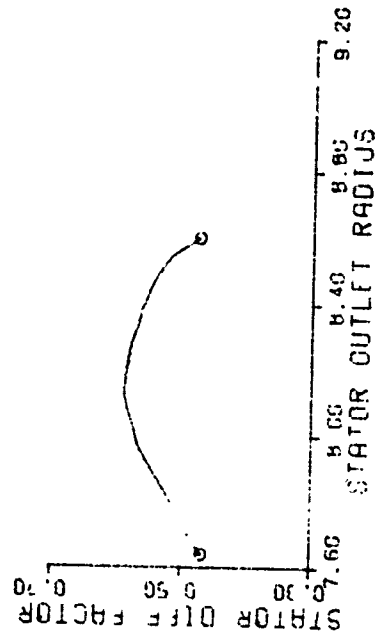


FIGURE 164. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 90% SPEED)

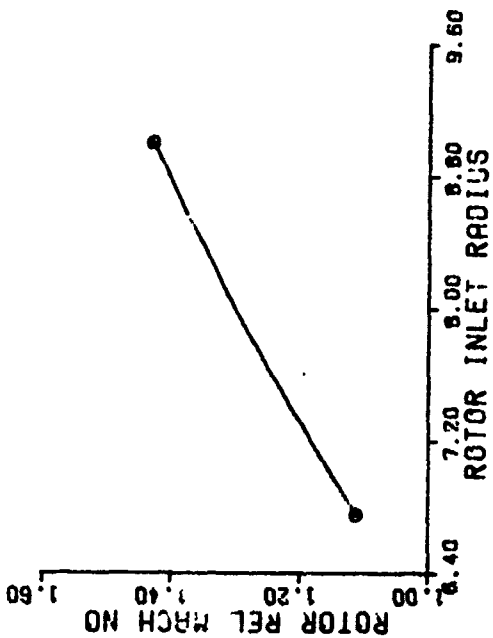


FIGURE 165. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

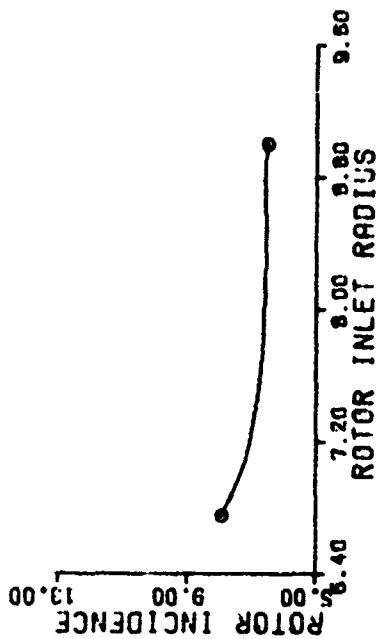


FIGURE 166. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

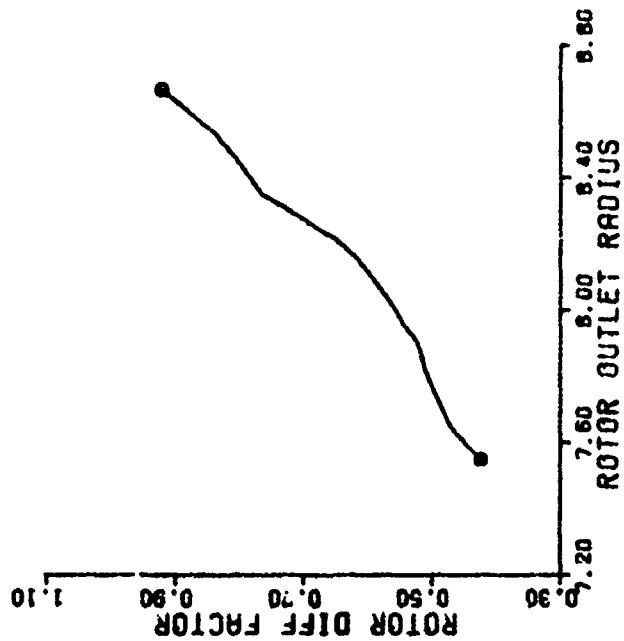


FIGURE 167. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

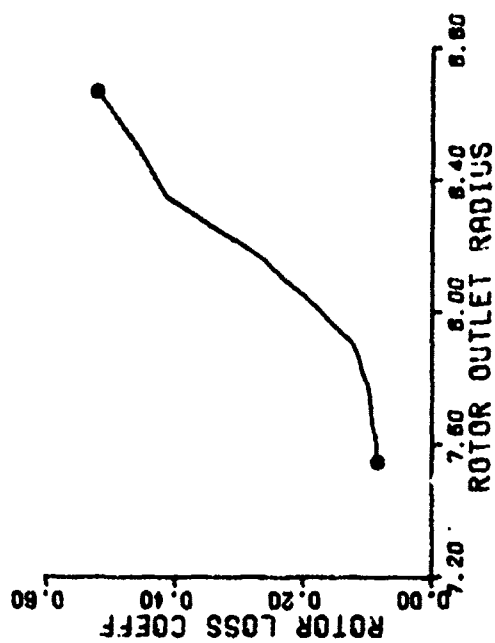


FIGURE 168. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

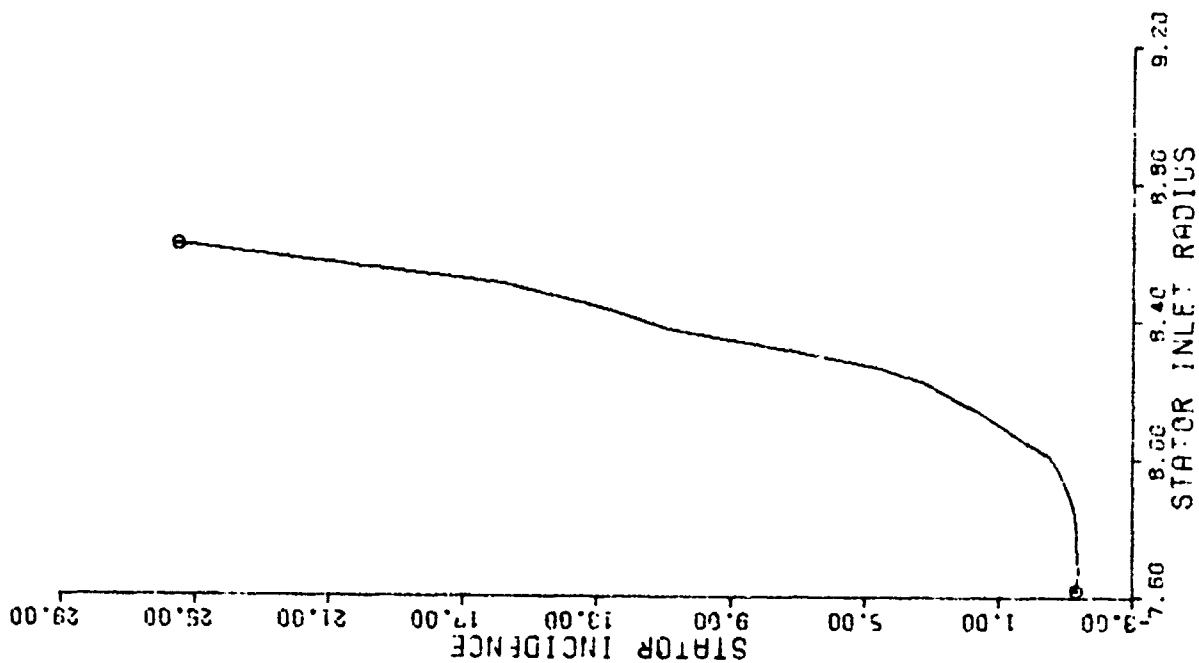


FIGURE 170. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

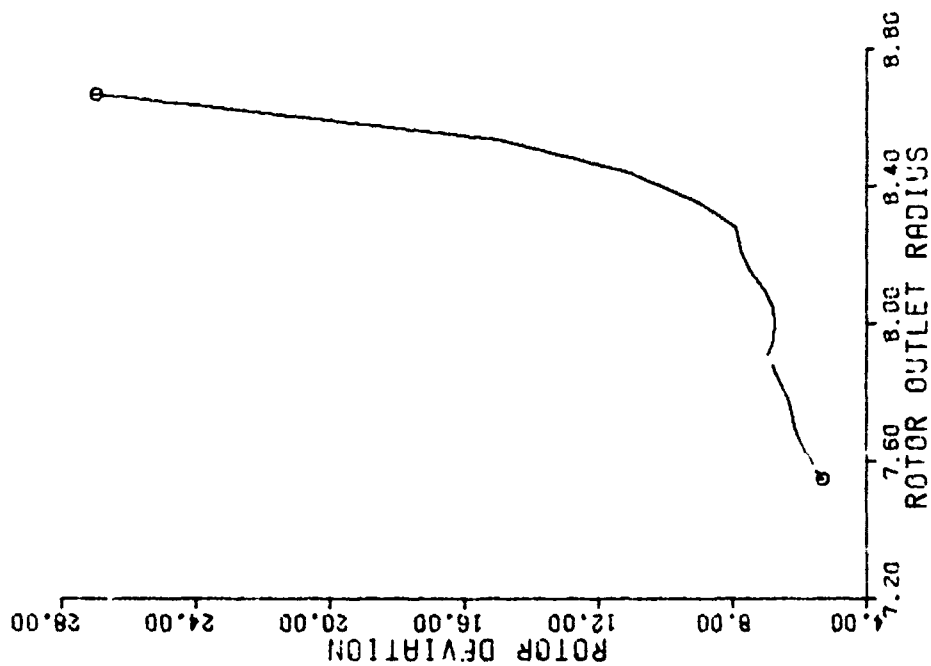


FIGURE 169. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)



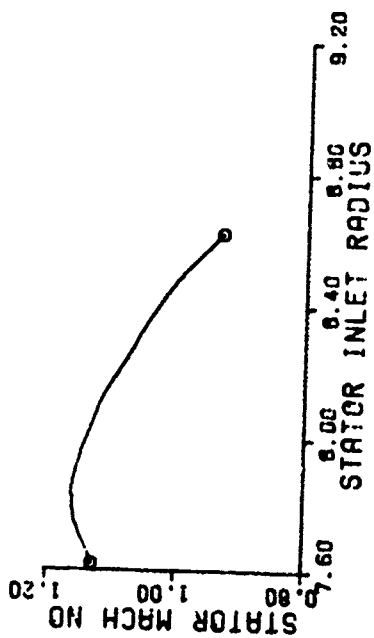


FIGURE 171. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

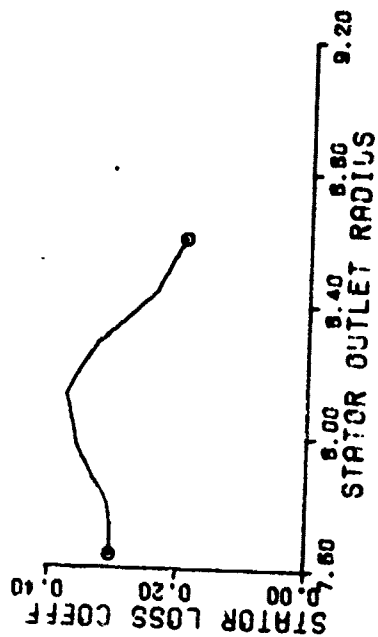


FIGURE 172. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

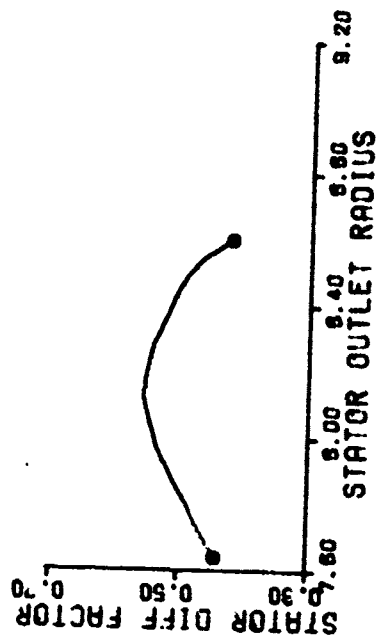


FIGURE 173. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 95% SPEED)

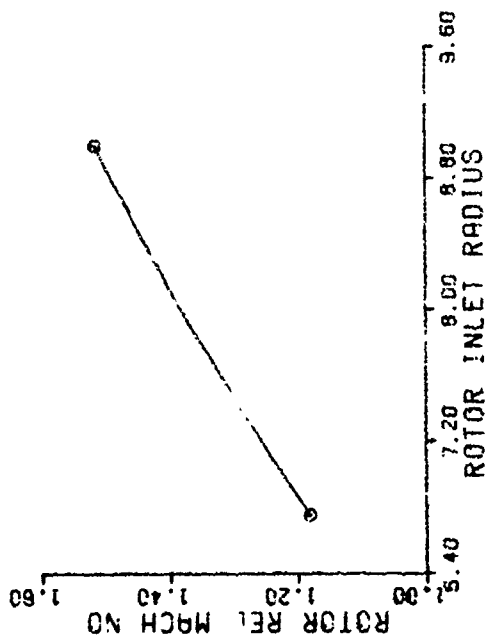


FIGURE 174. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

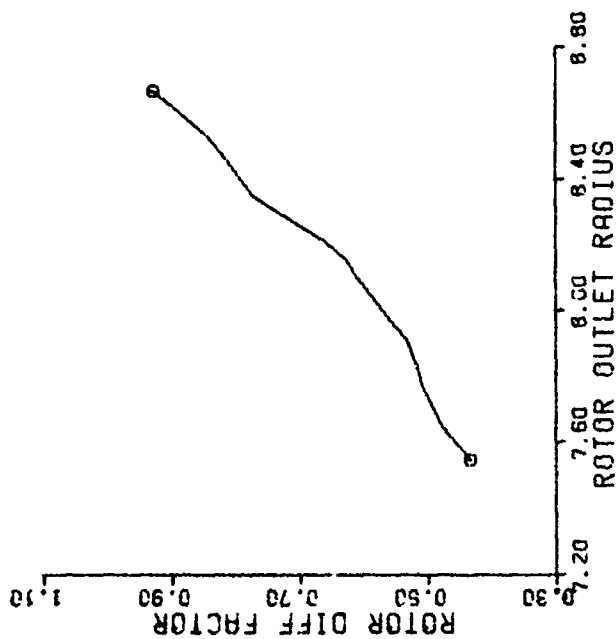


FIGURE 176. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

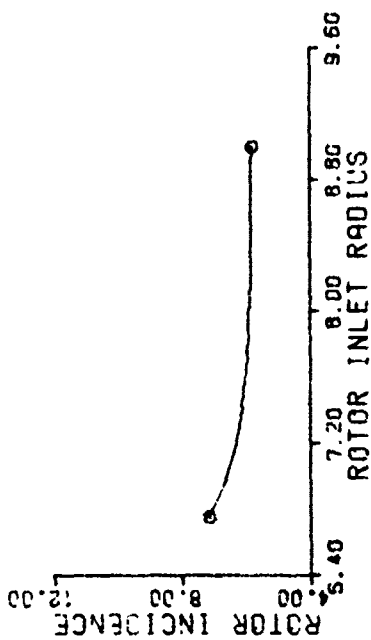


FIGURE 175. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

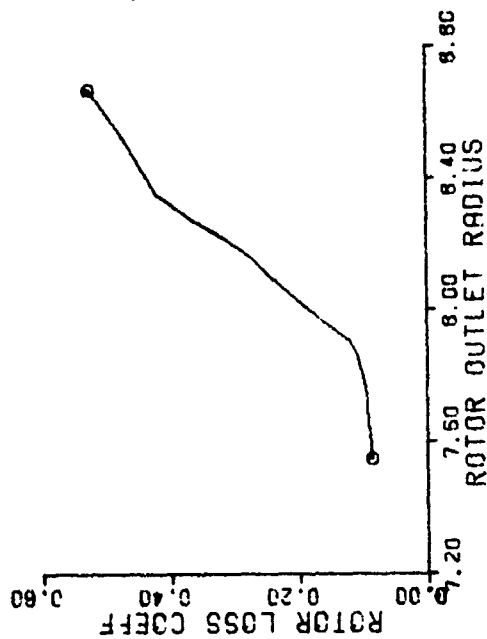


FIGURE 177. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

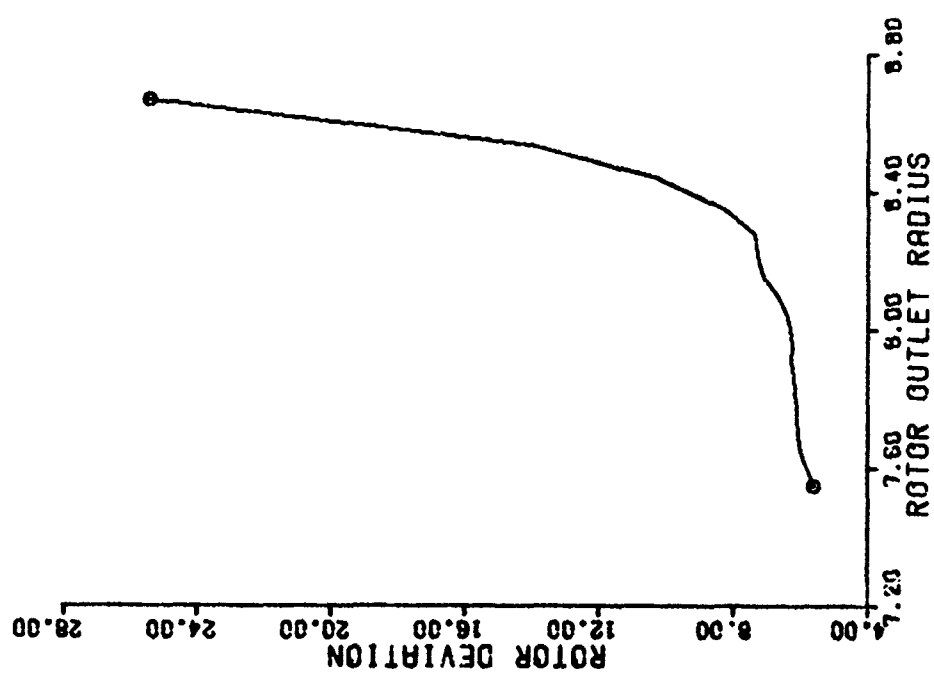


FIGURE 178. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

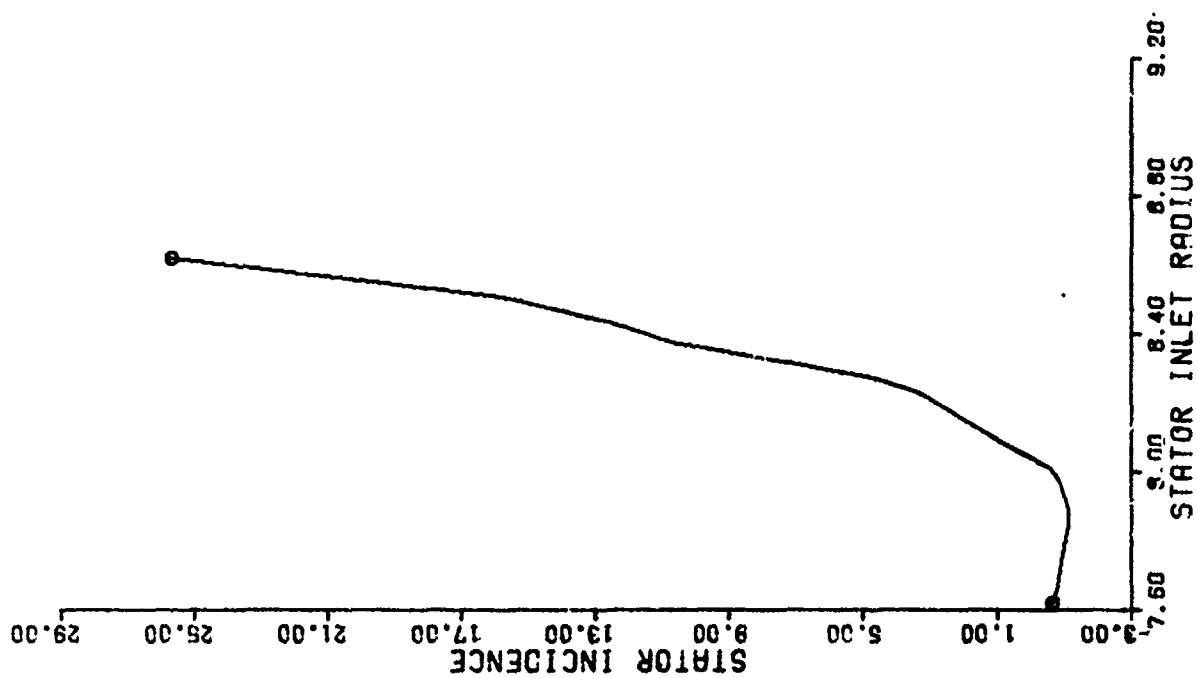


FIGURE 179. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

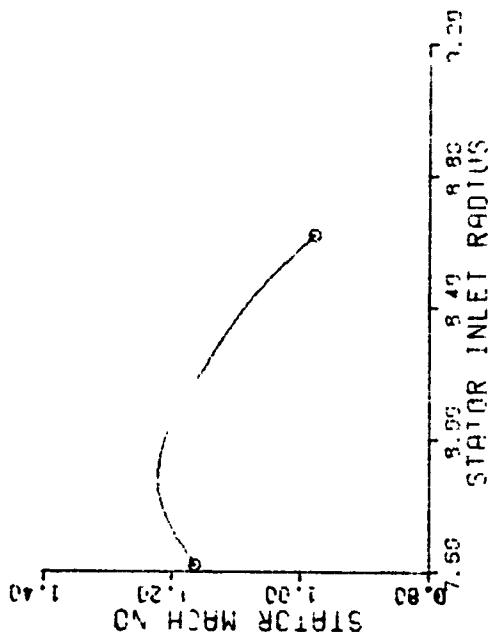


FIGURE 180. STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

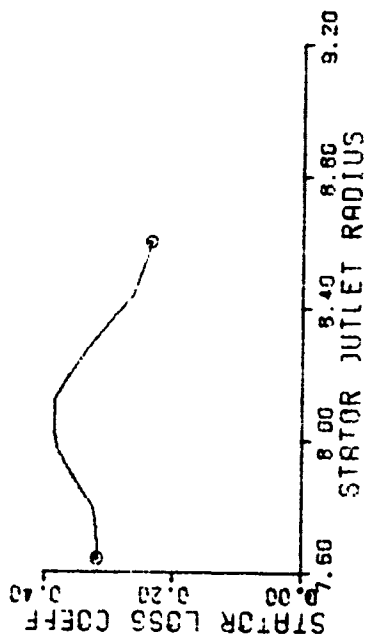


FIGURE 181. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

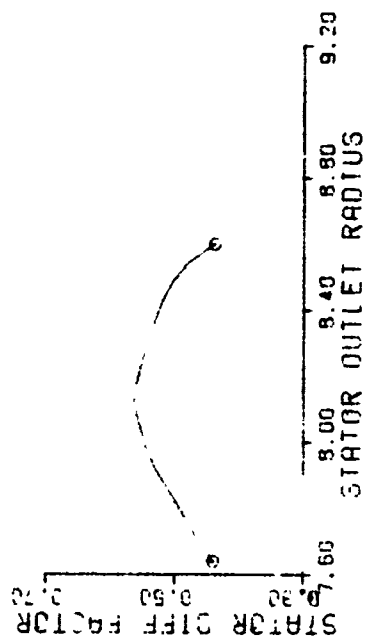


FIGURE 182. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

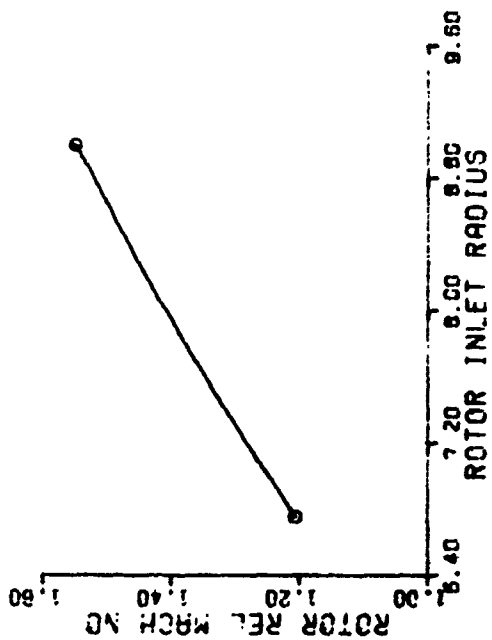


FIGURE 183. ROTOR RELATIVE MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

18

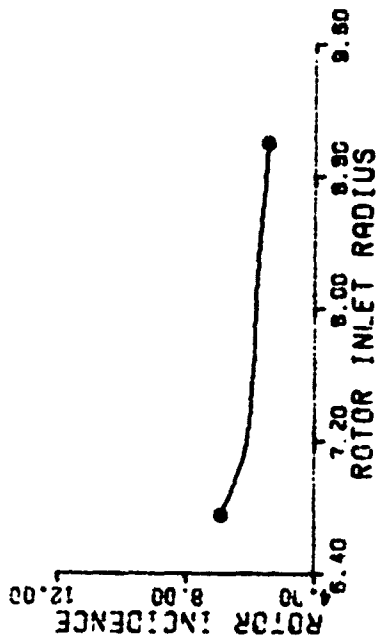


FIGURE 184. ROTOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

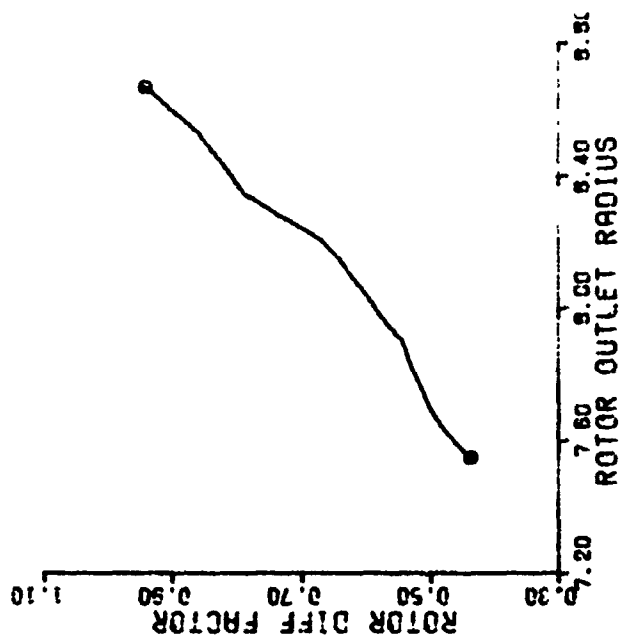


FIGURE 185. ROTOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

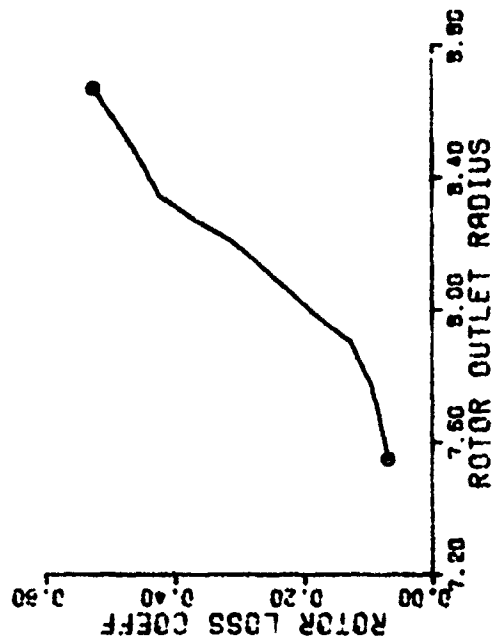


FIGURE 186. ROTOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 100% SPEED)

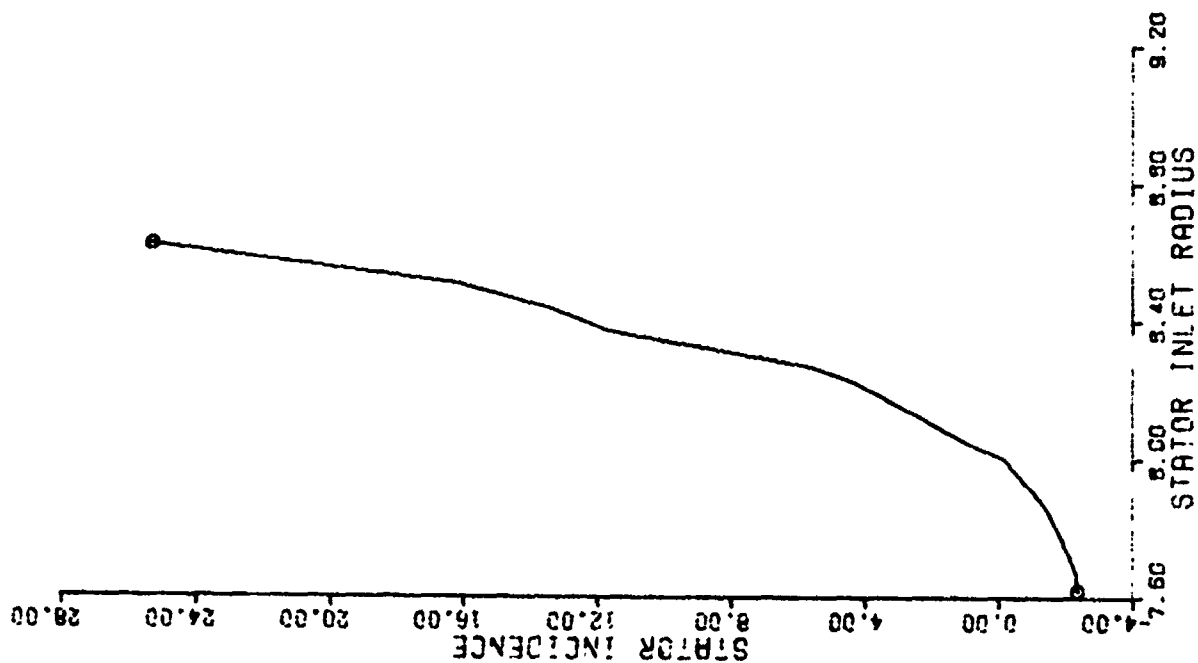


FIGURE 187. ROTOR DEVIATION VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 102% SPEED)

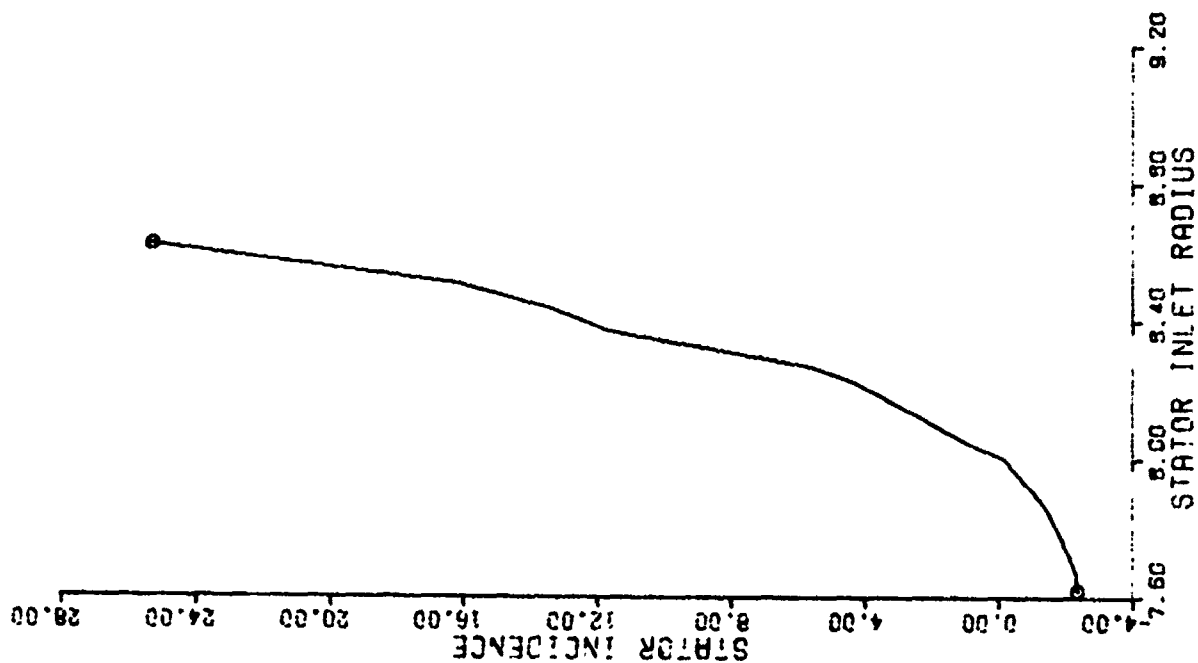


FIGURE 188. STATOR INCIDENCE VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 102% SPEED)

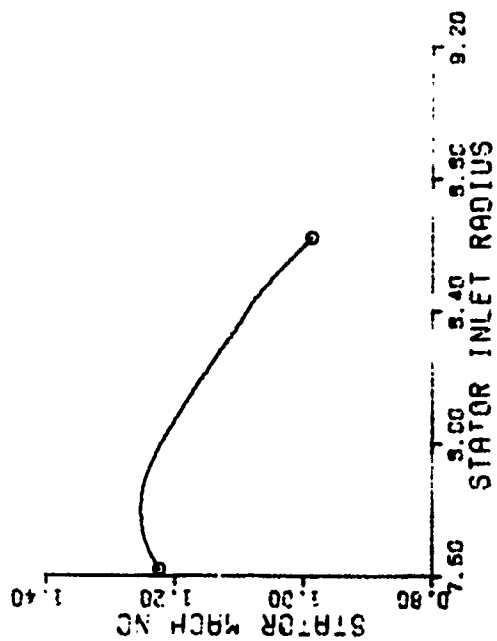


FIGURE 189 STATOR MACH NUMBER VS INLET RADIUS  
(WITHIN-BLADE ANALYSIS, 102% SPEED)

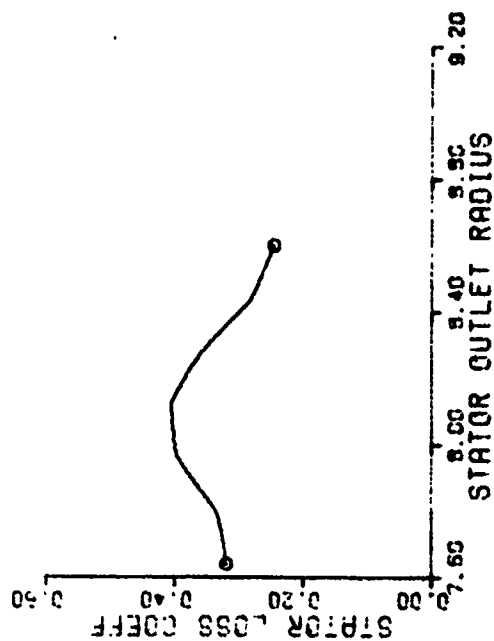


FIGURE 190. STATOR LOSS COEFFICIENT VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 102% SPEED)

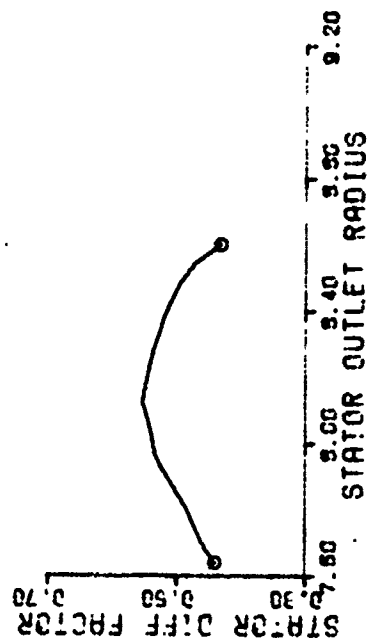


FIGURE 191. STATOR DIFFUSION FACTOR VS OUTLET RADIUS  
(WITHIN-BLADE ANALYSIS, 102% SPEED)

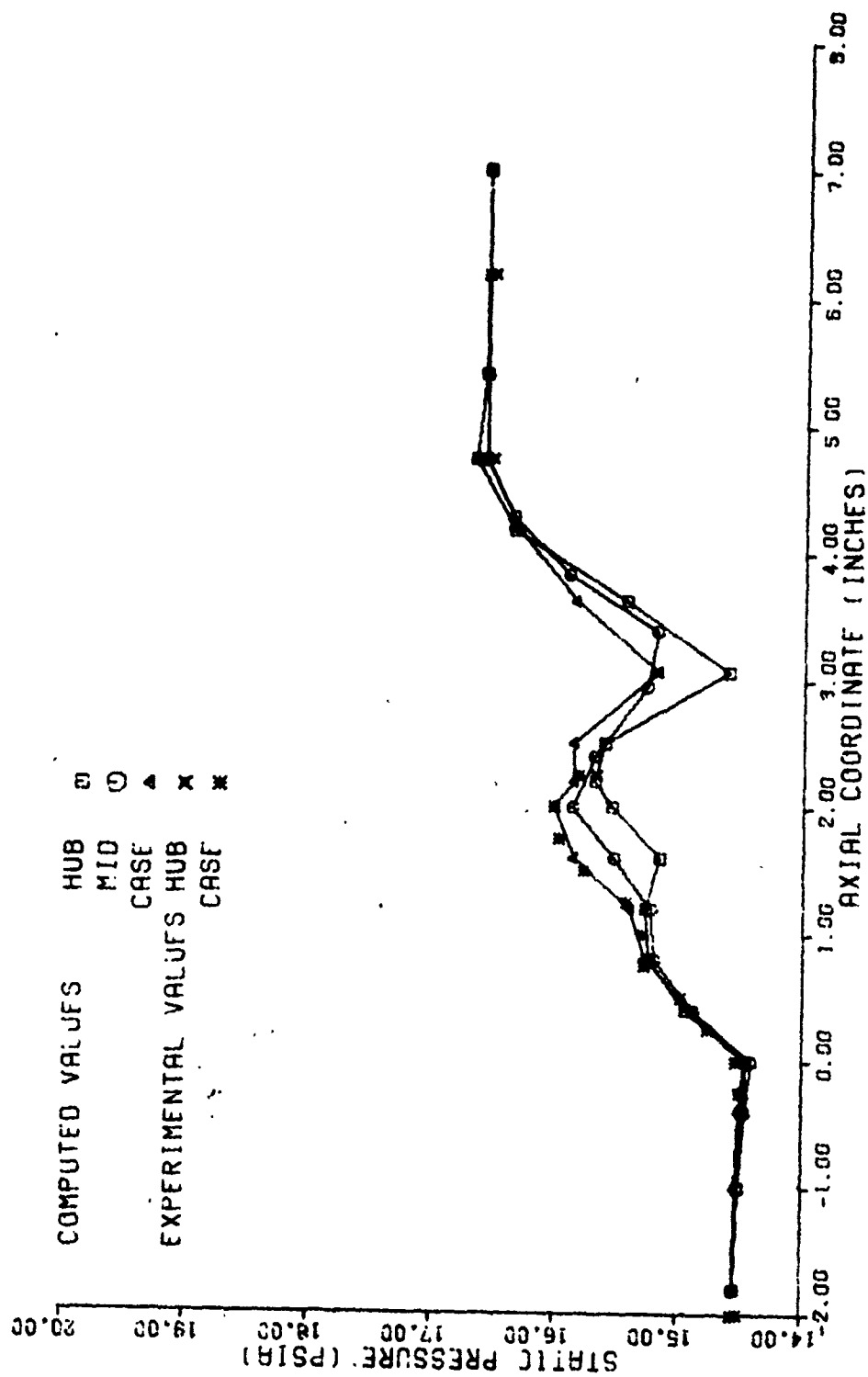


FIGURE 192. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 40% SPEED)



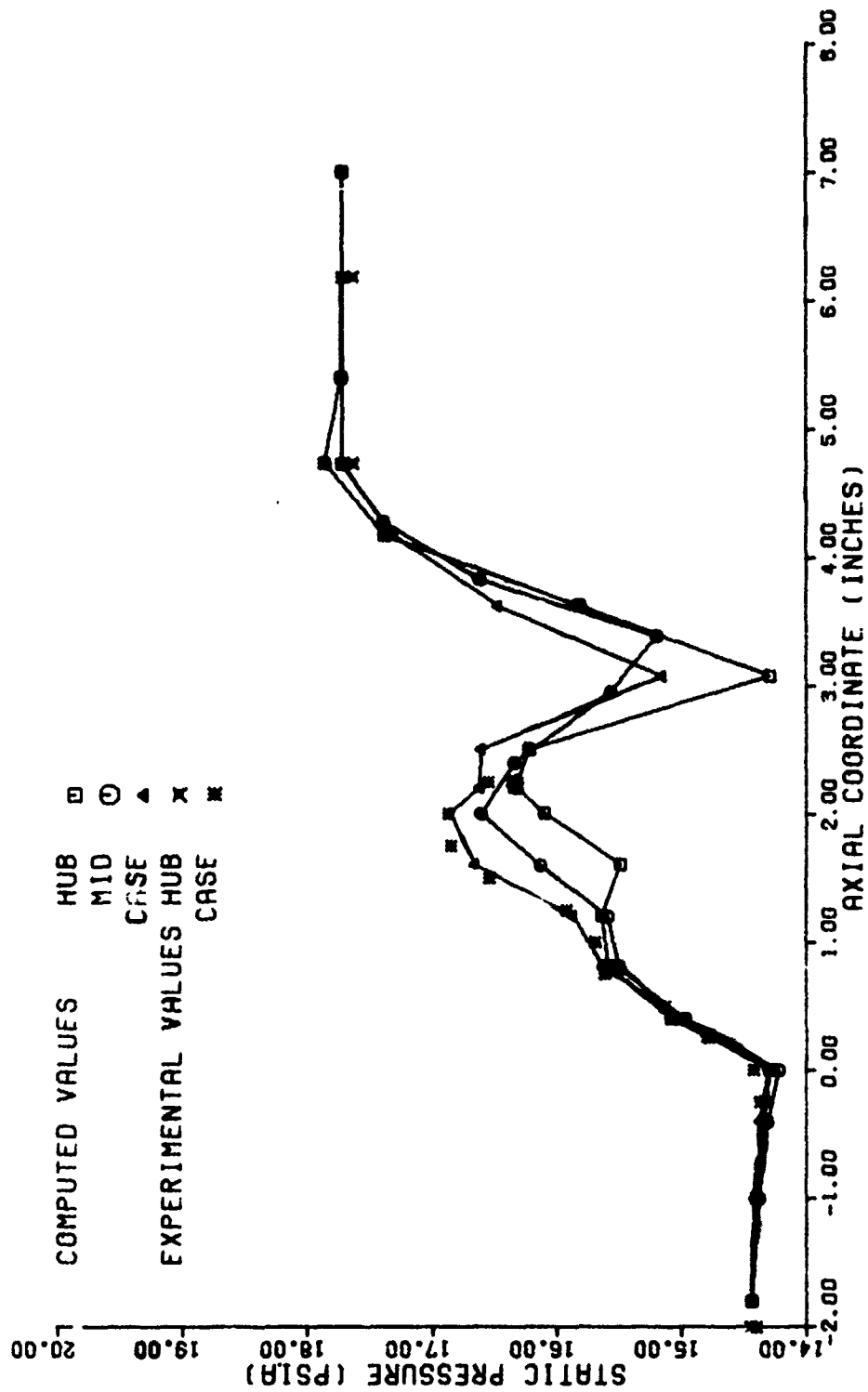


FIGURE 193. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 50% SPEED)

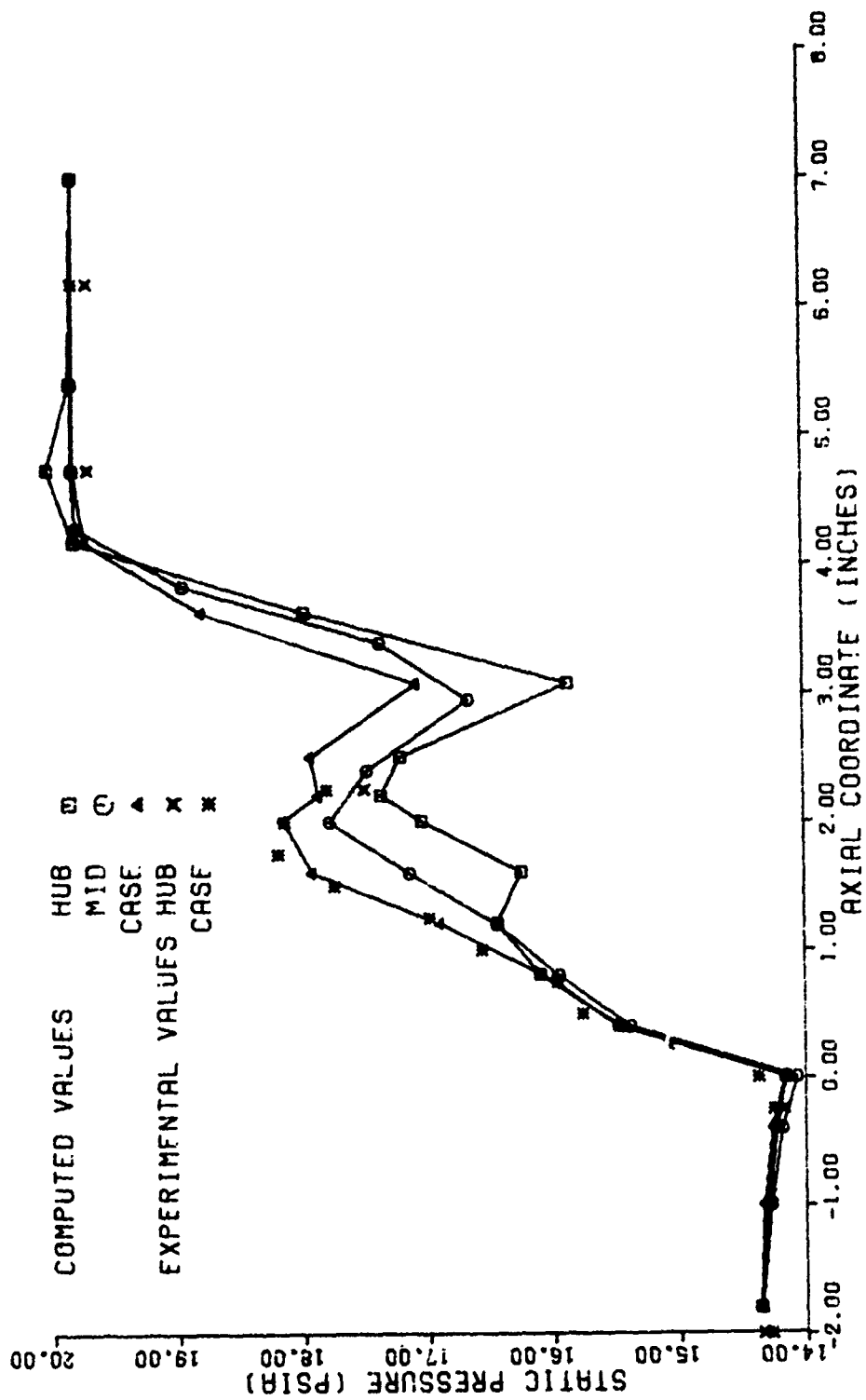


FIGURE 194. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 60% SPEED)

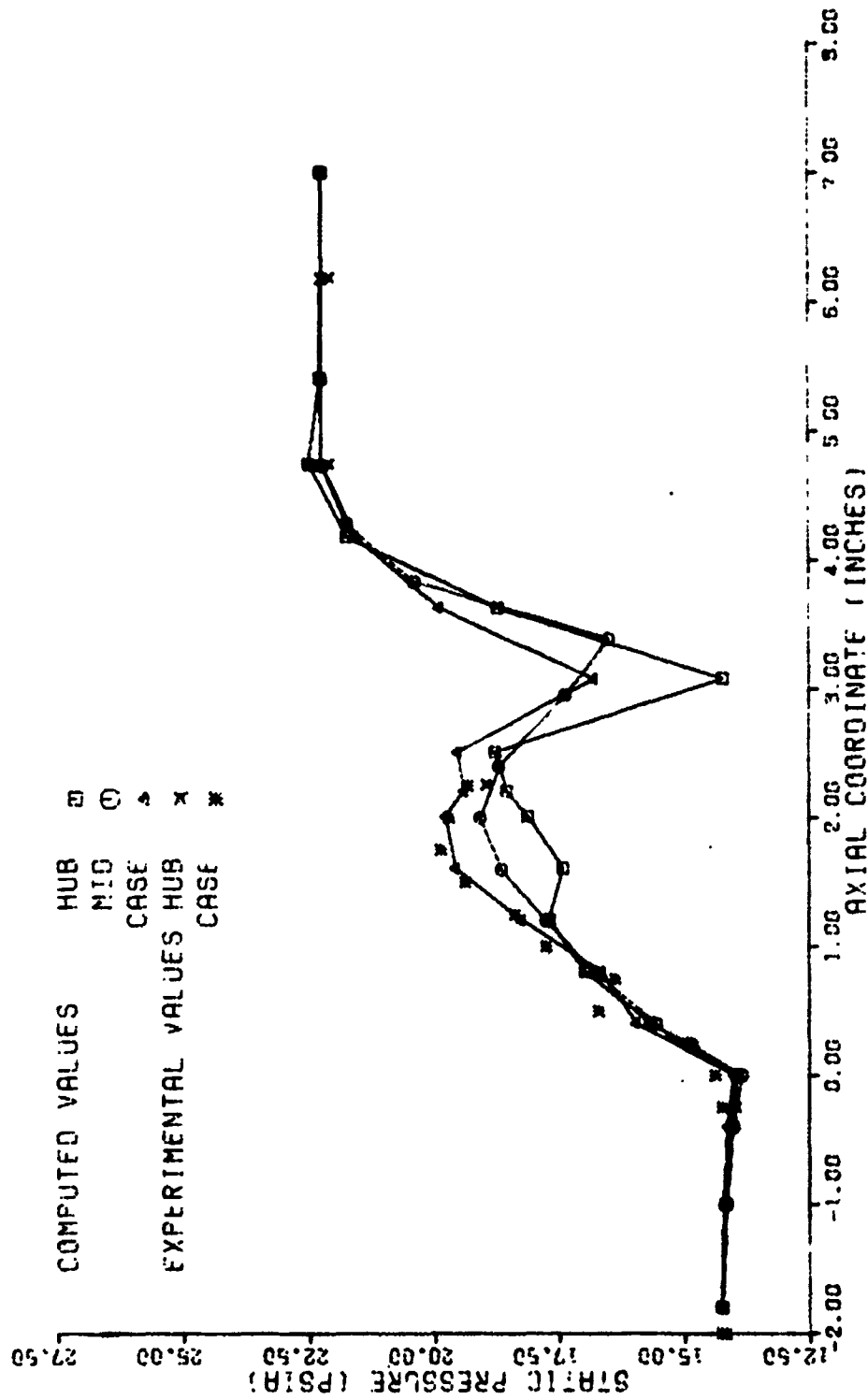


FIGURE 195. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 70% SPEED)

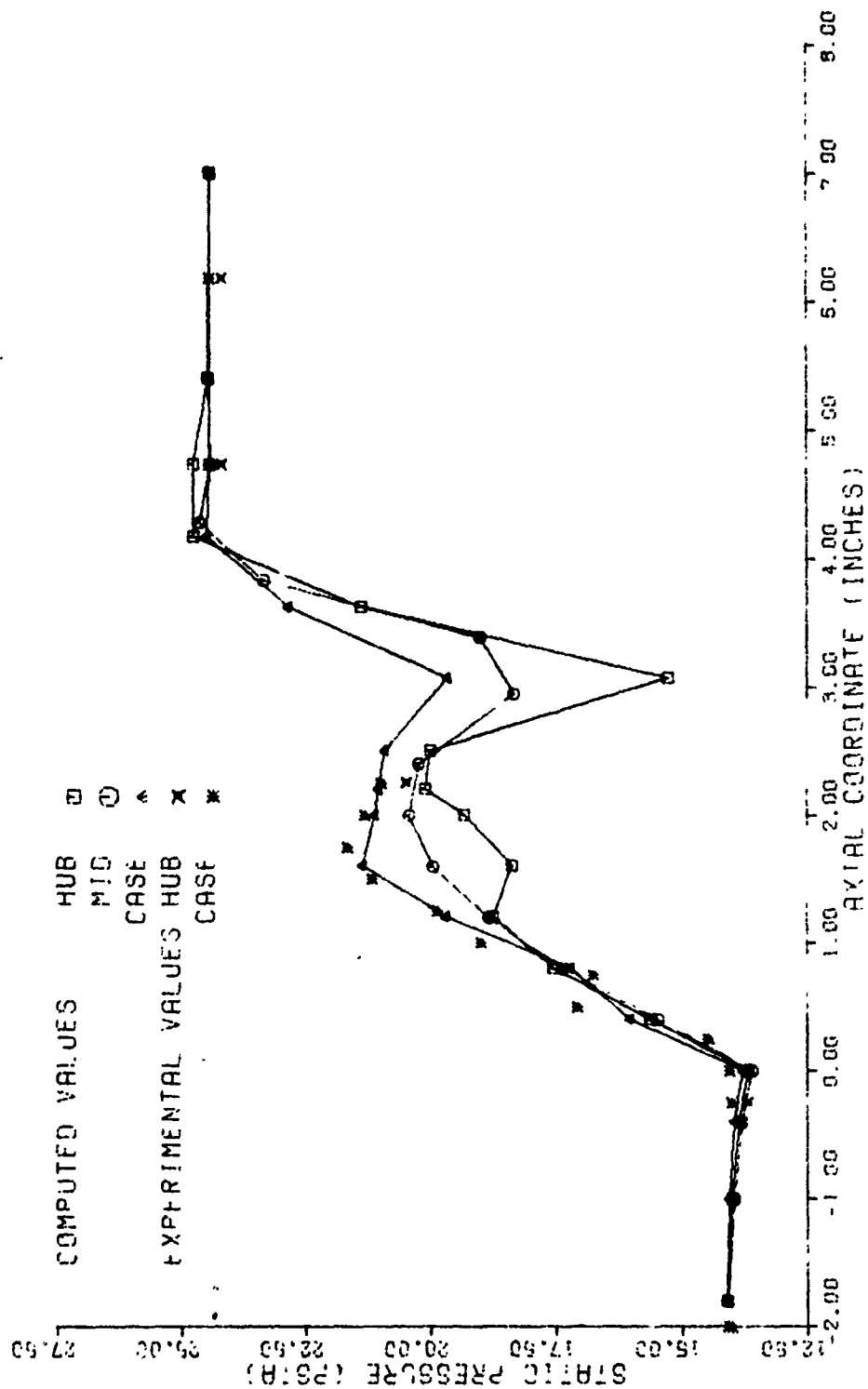


FIGURE 196. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 80% SPEED)

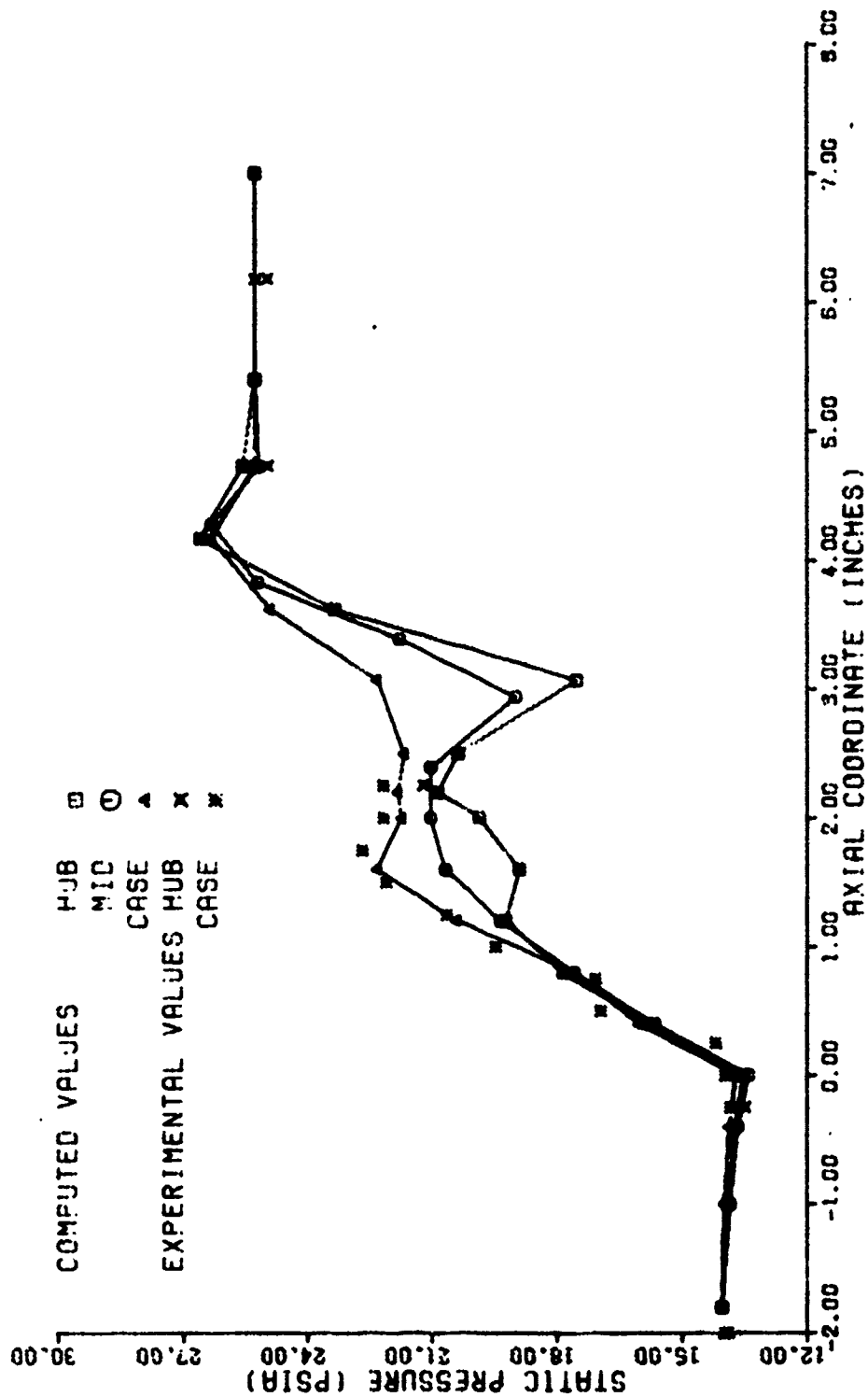


FIGURE 197. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 85% SPEED)

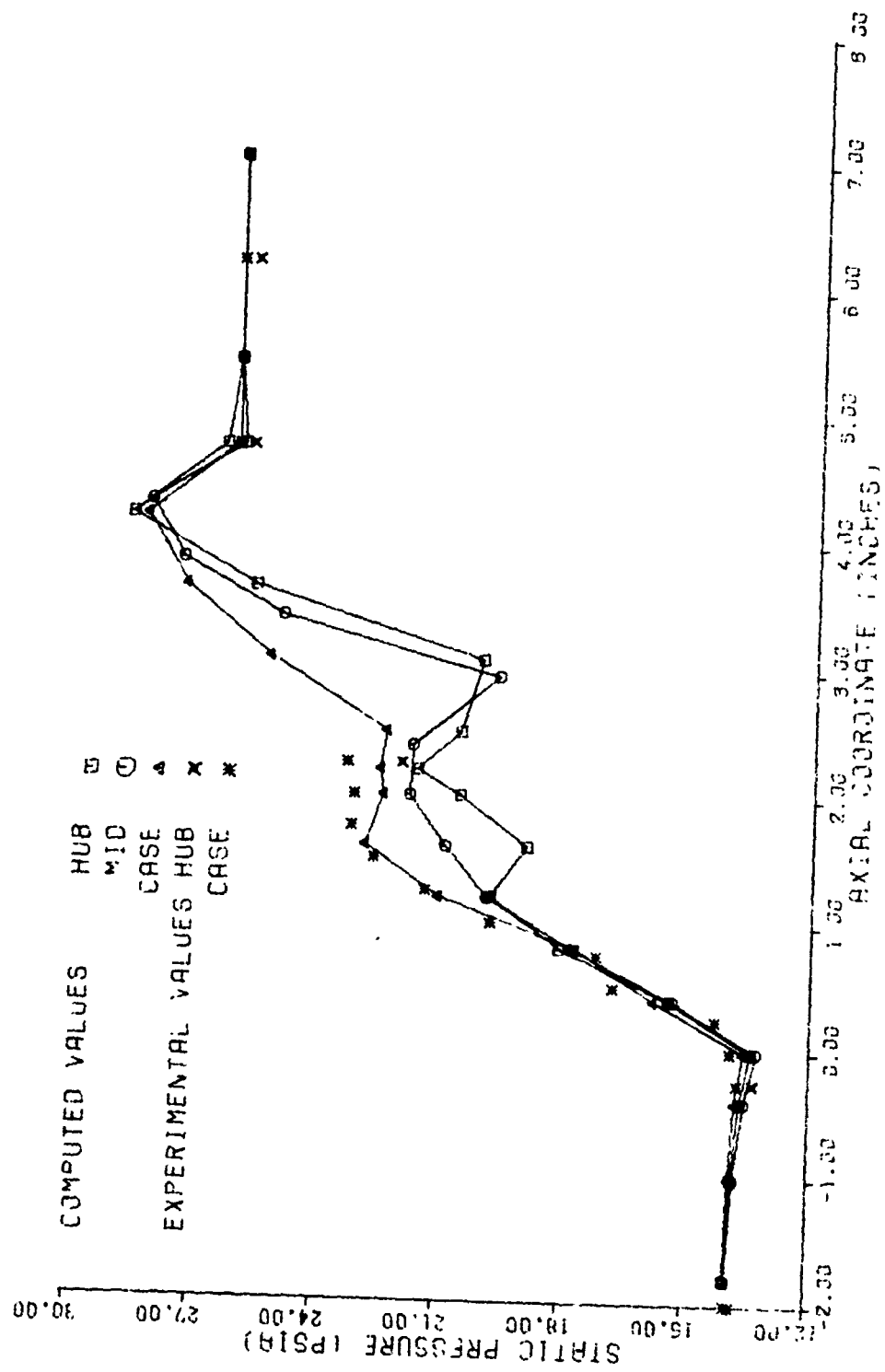


FIGURE 198. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 90% SPEED)

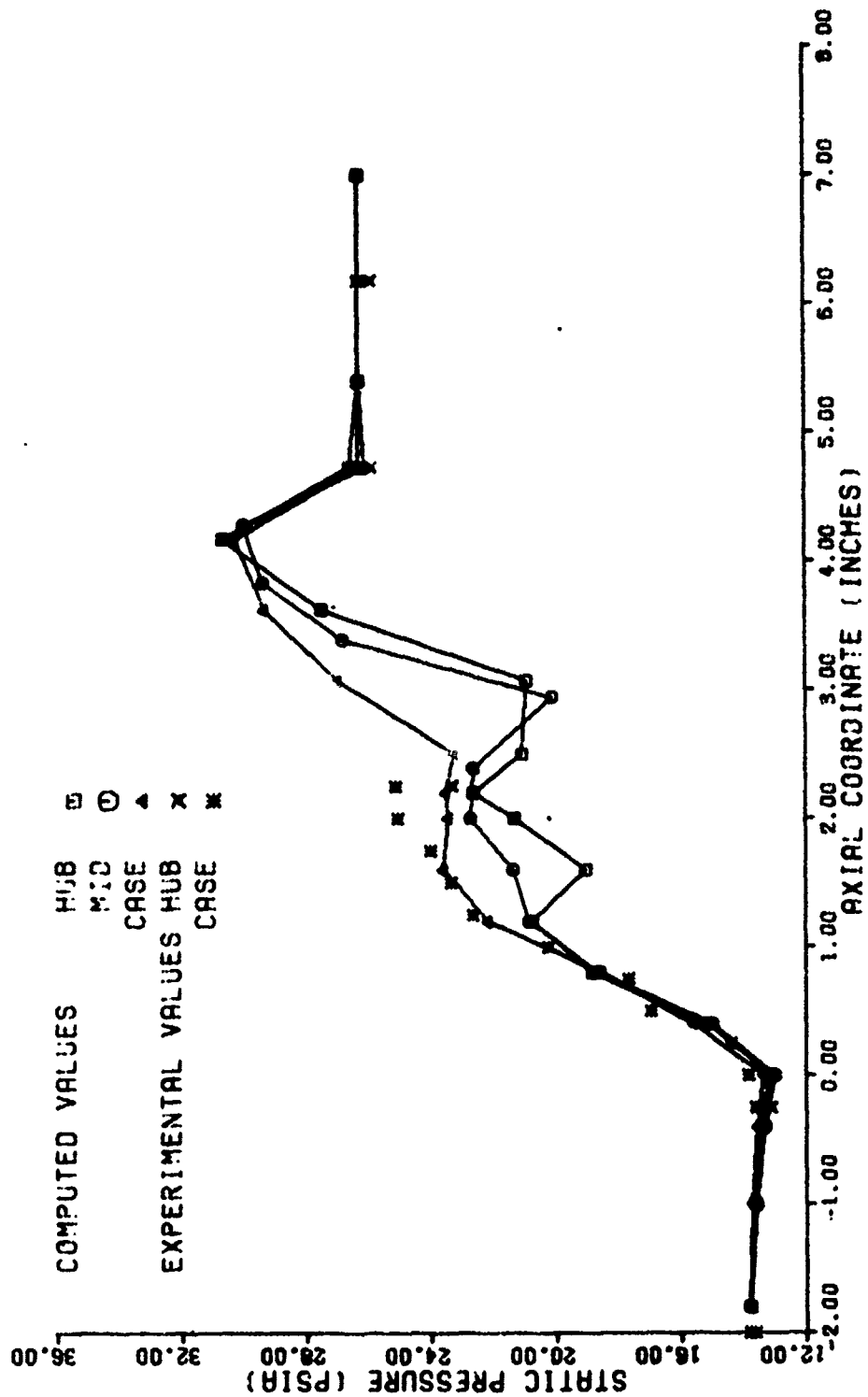


FIGURE 199. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 95% SPEED)

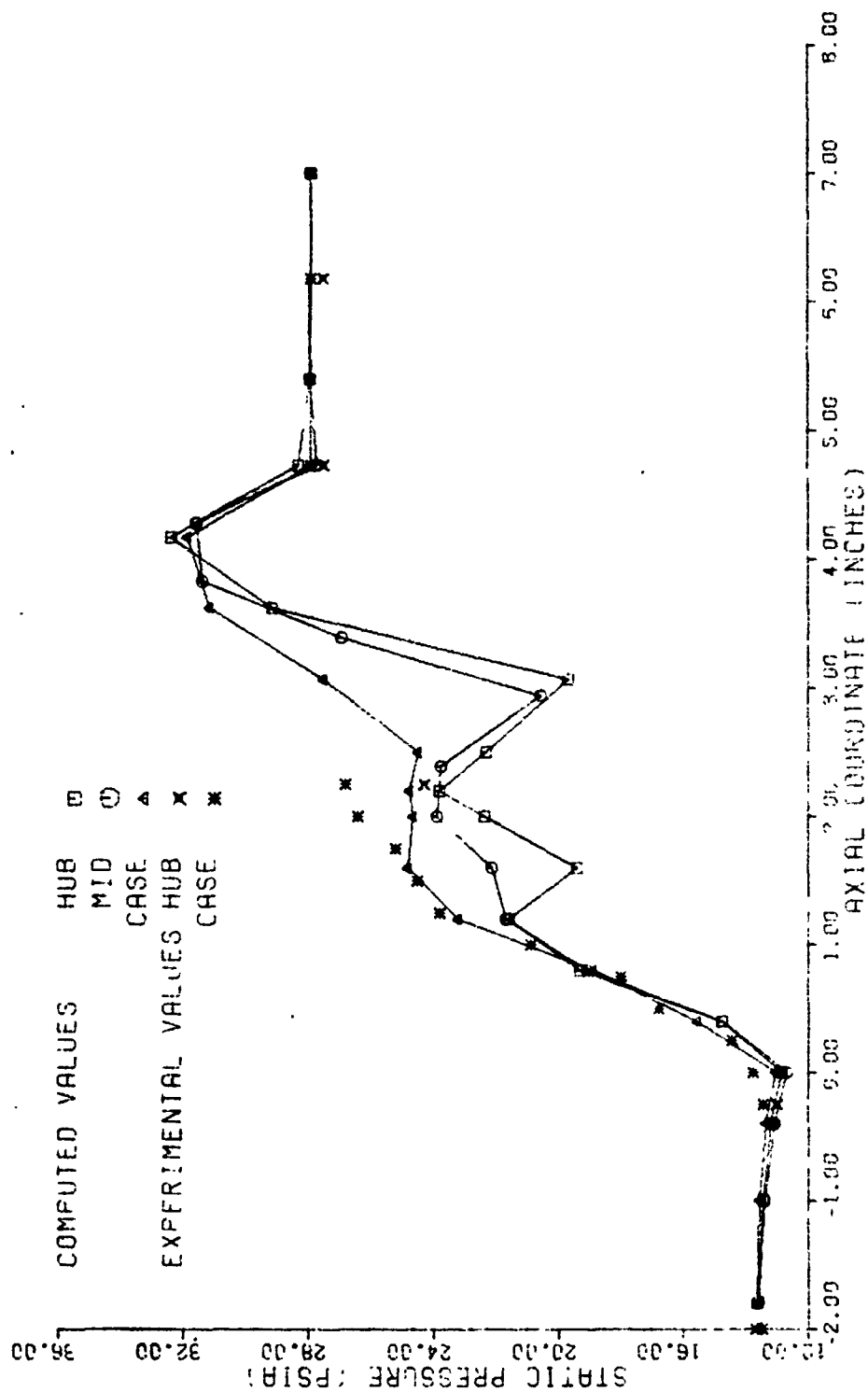


FIGURE 200. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 100% SPEED)



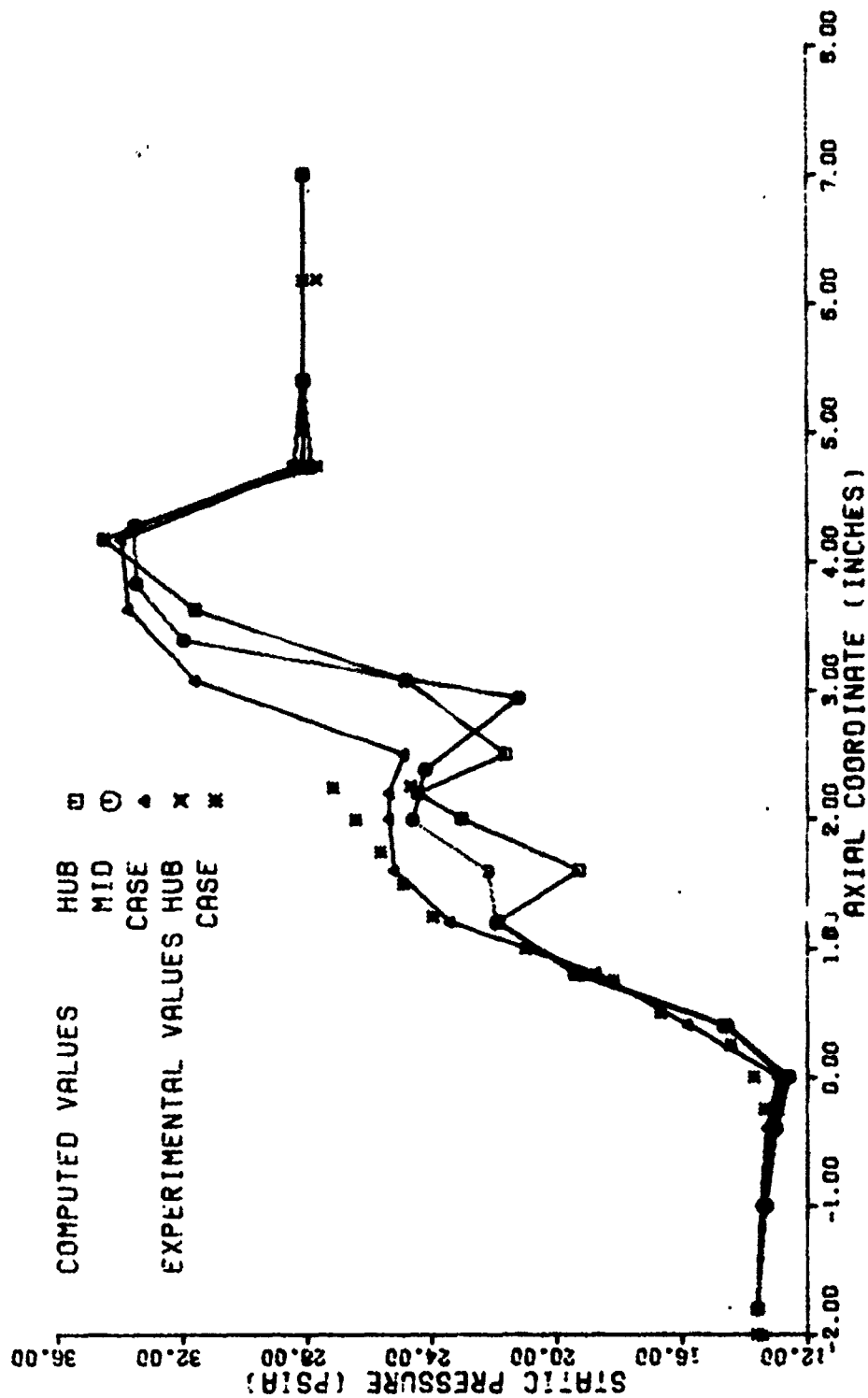


FIGURE 201. AXIAL STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 102% SPEED)

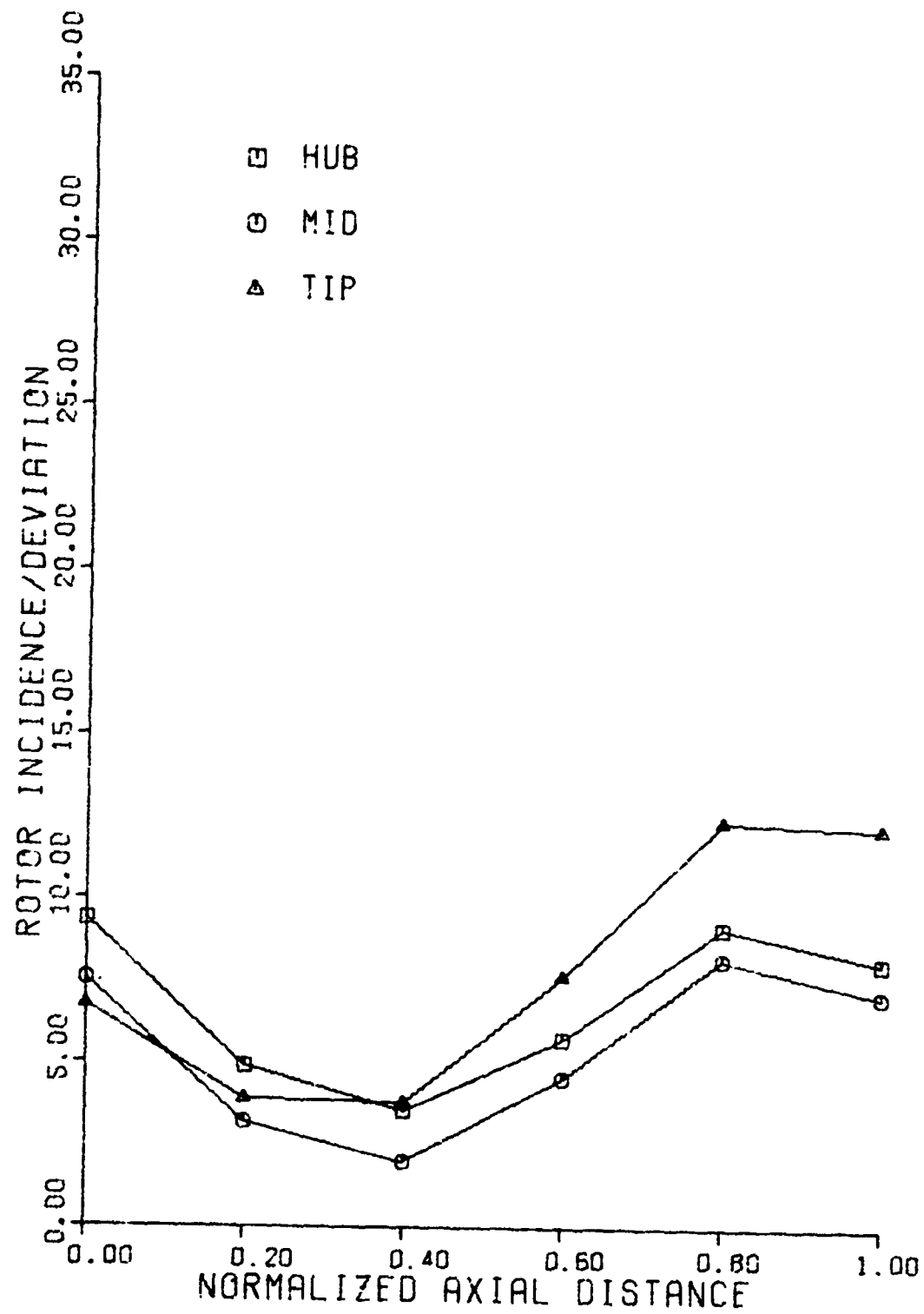


FIGURE 202. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (40% SPEED POINT)

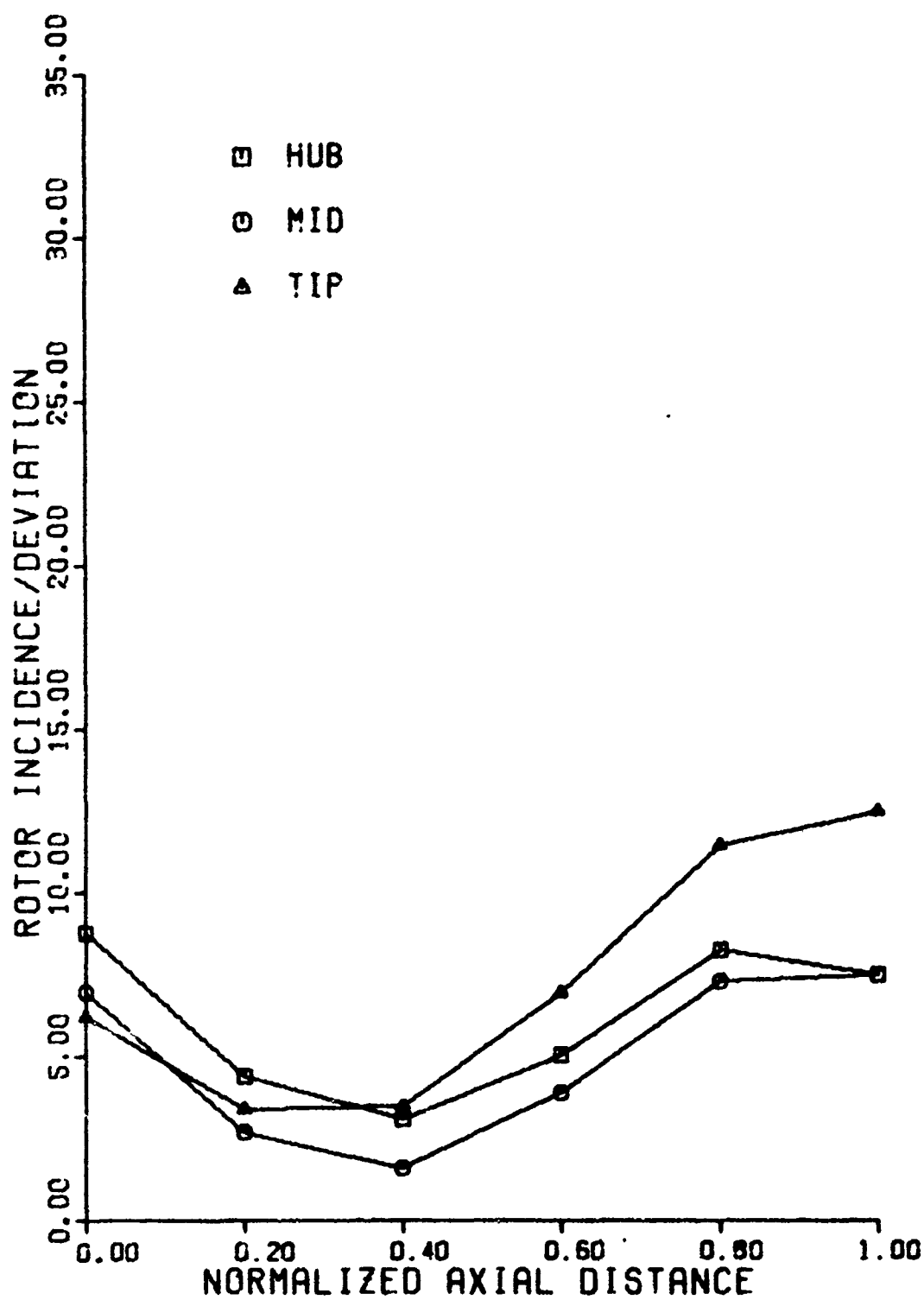


FIGURE 203. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (50% SPEED POINT)

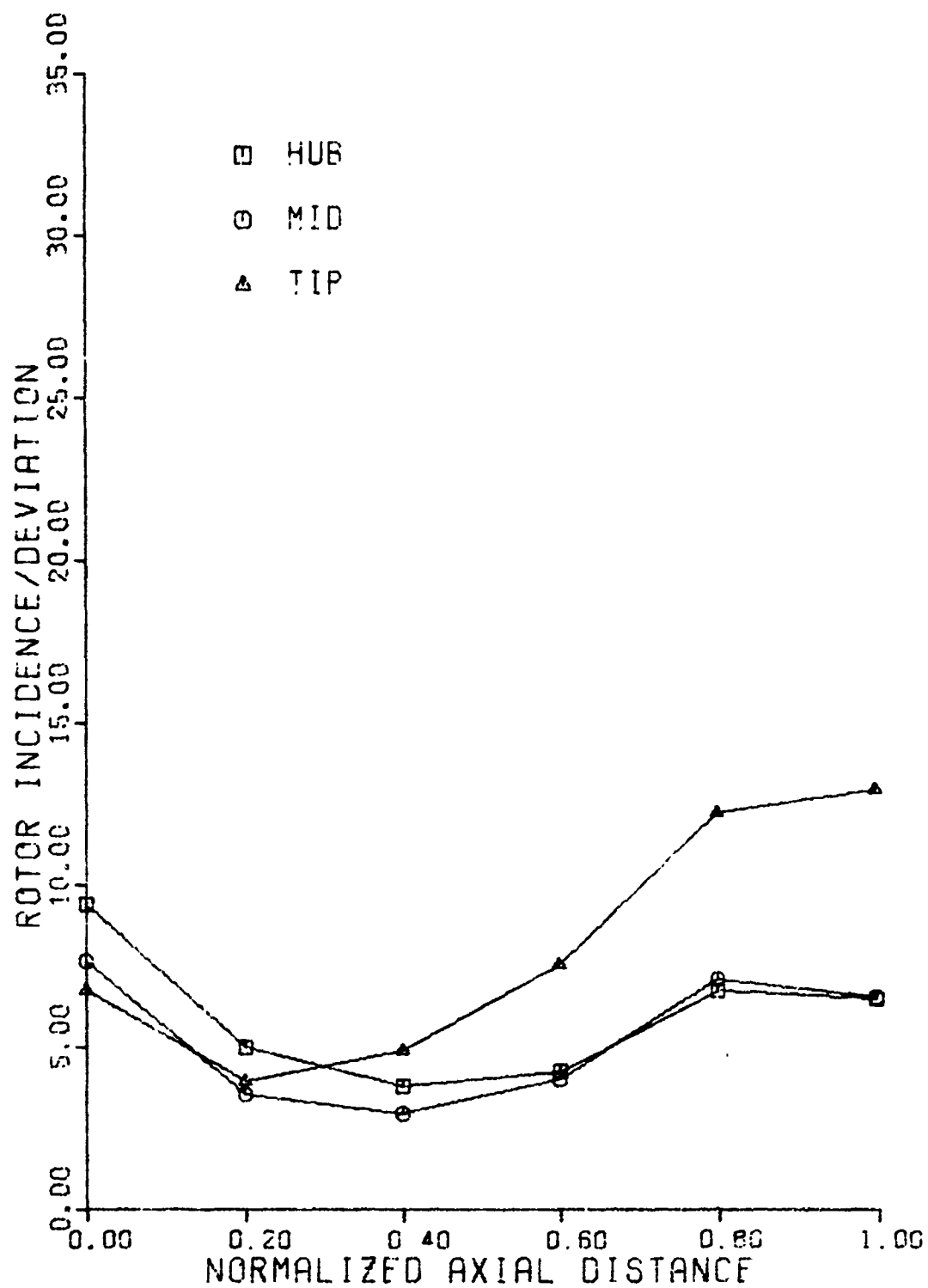


FIGURE 204. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (60% SPEED POINT)

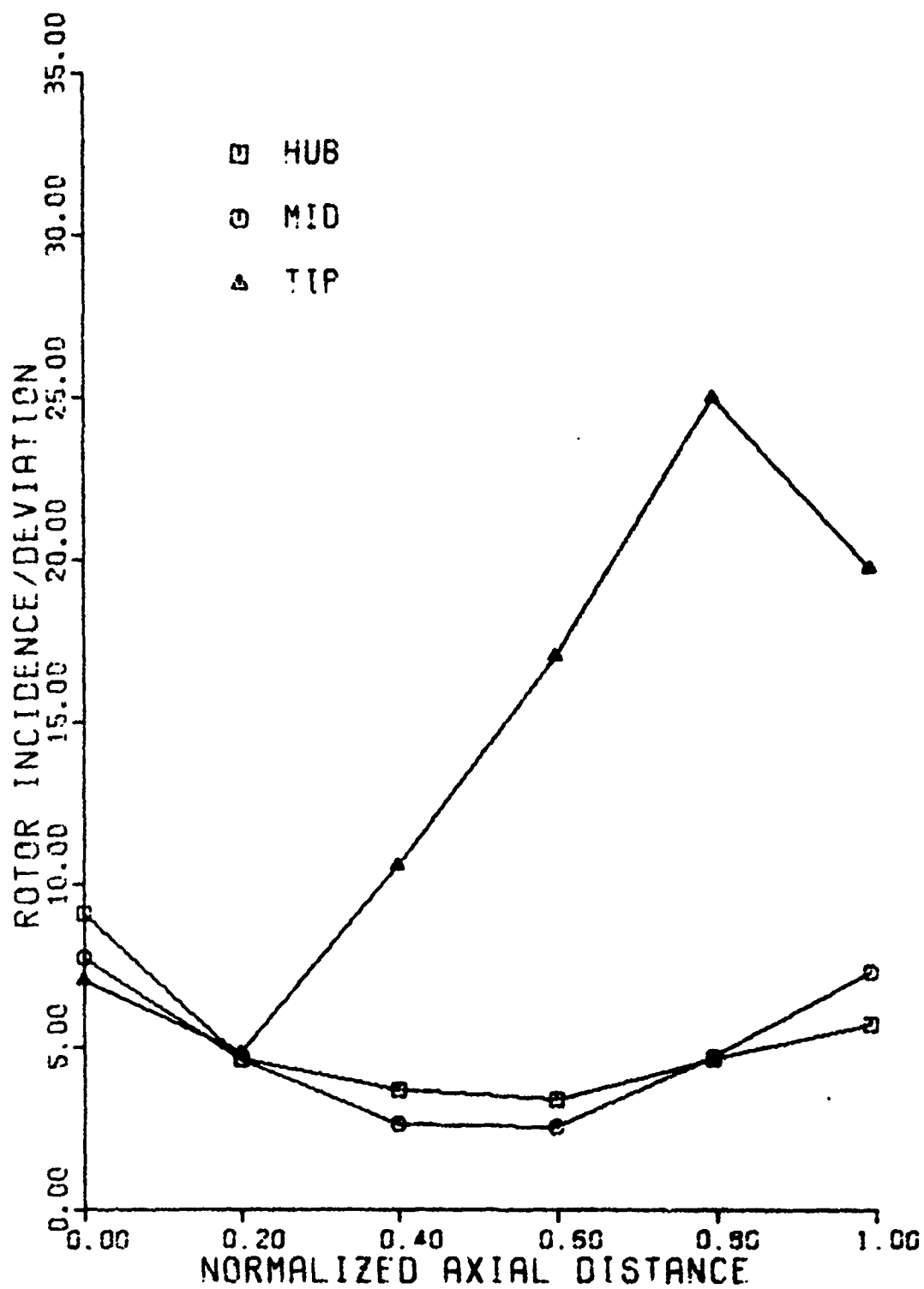


FIGURE 205. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (70% SPEED POINT)

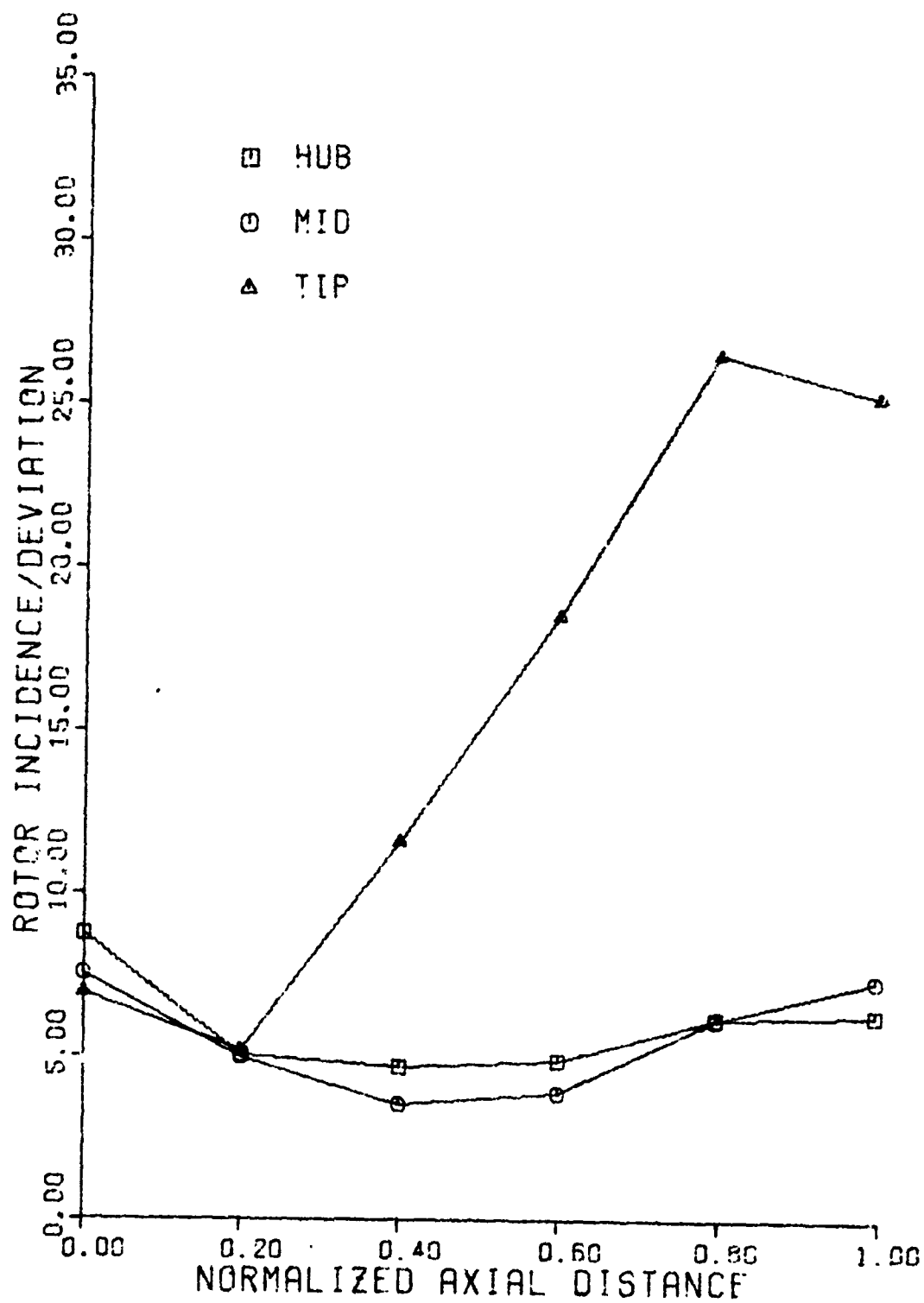


FIGURE 206. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (80% SPEED POINT)

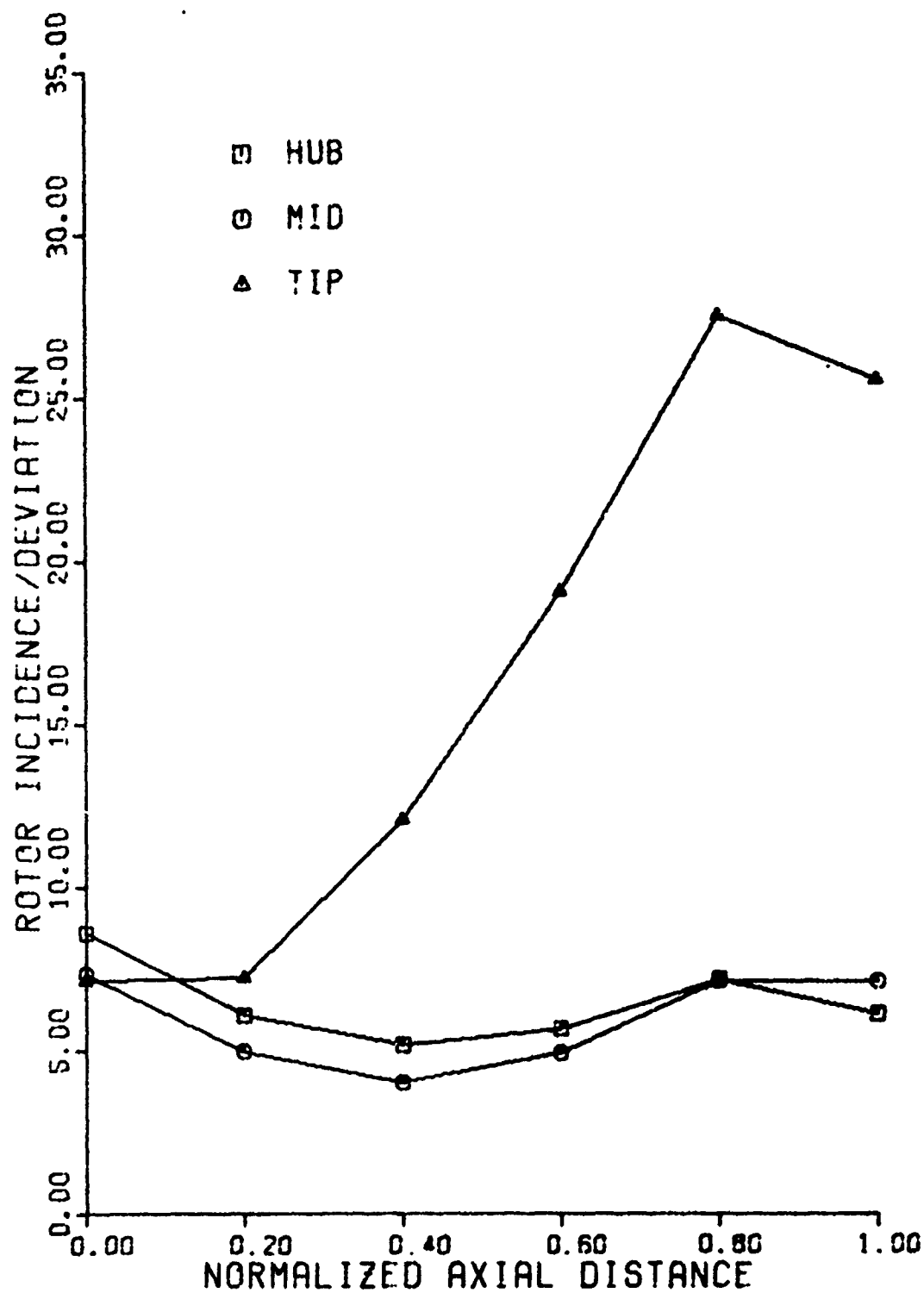


FIGURE 207. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (85% SPEED POINT)

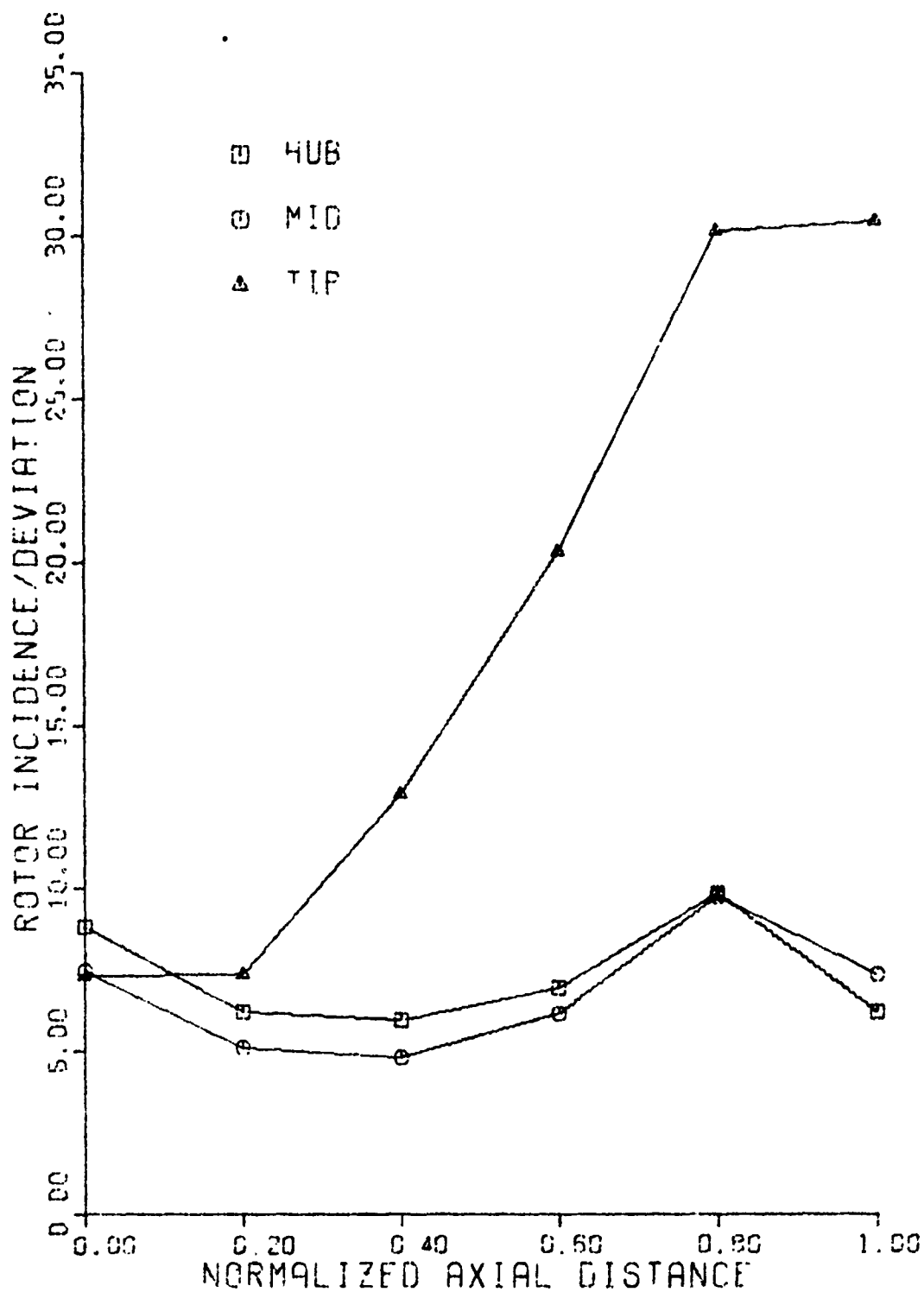


FIGURE 208. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION 90% SPEED POINT)



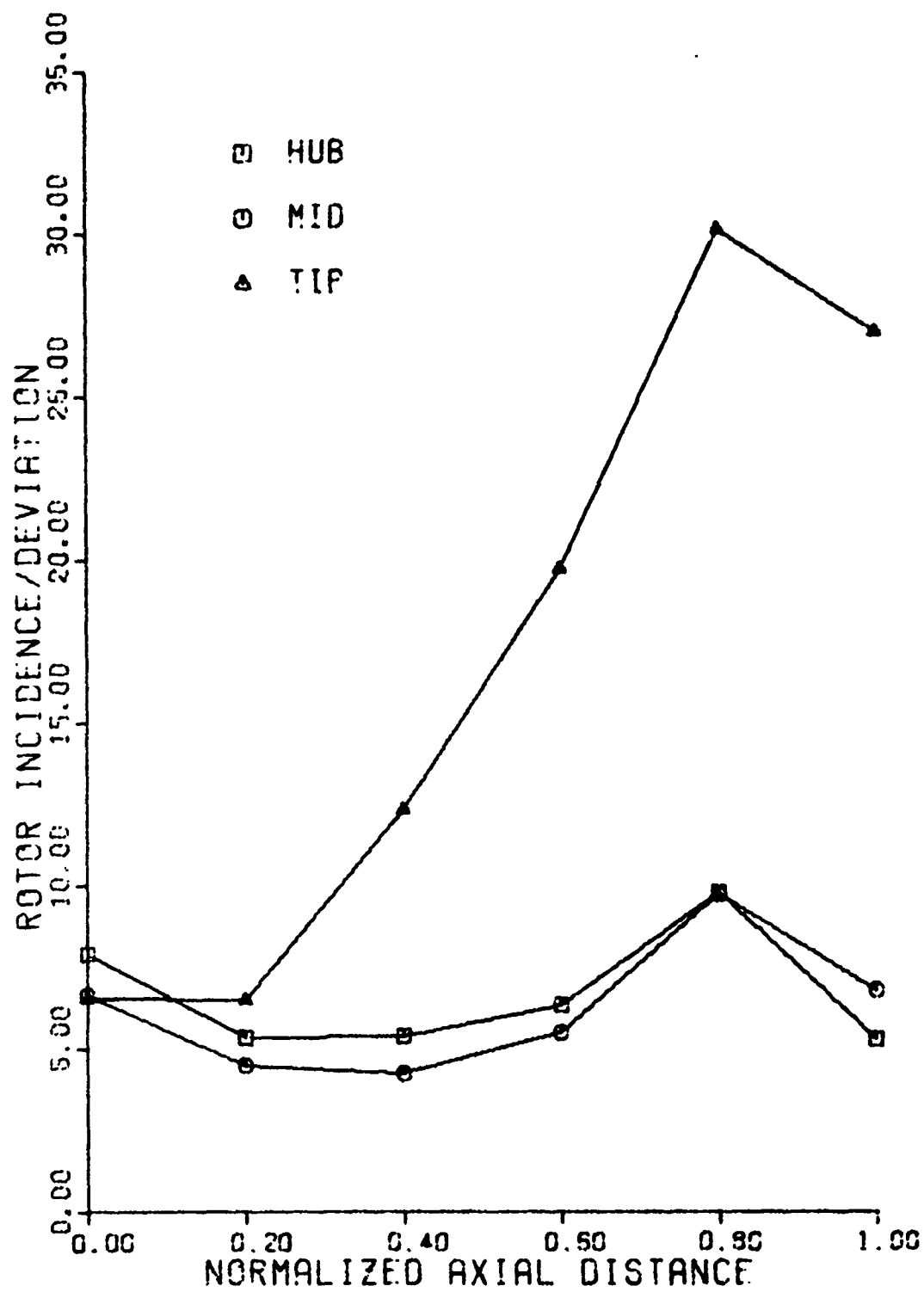


FIGURE 209. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (95% SPEED POINT)

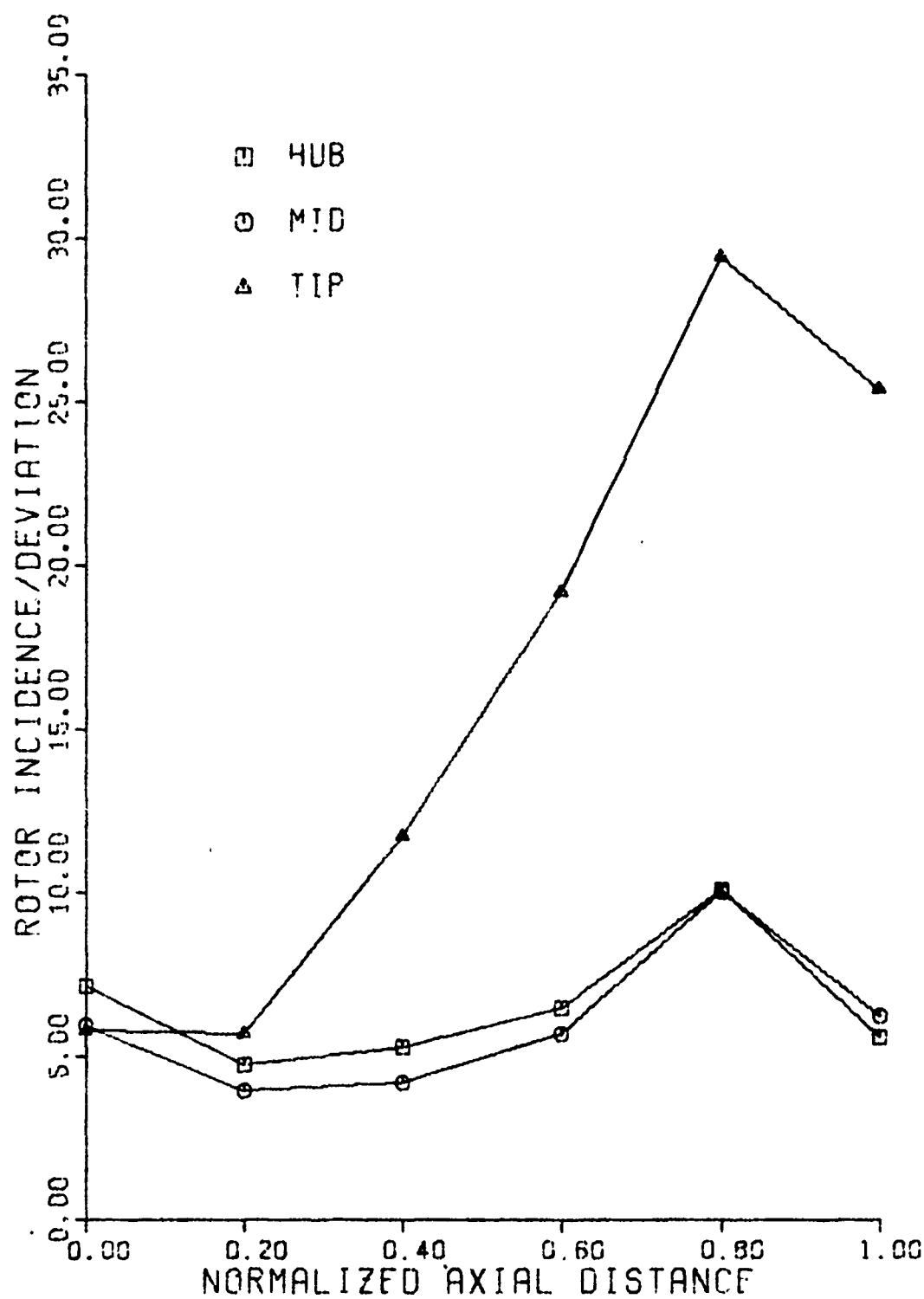


FIGURE 210. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (100% SPEED POINT)

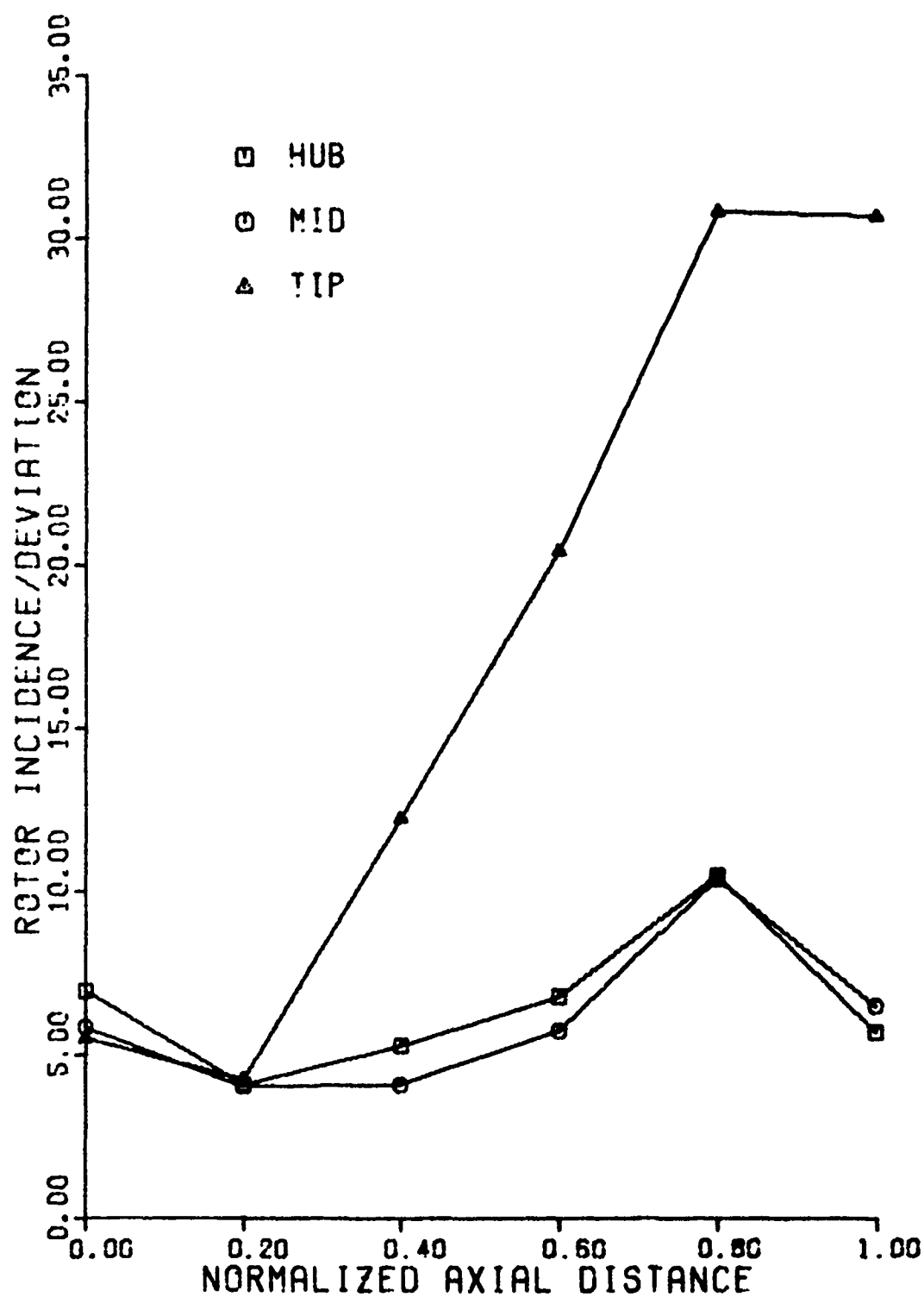


FIGURE 211. ROTOR WITHIN-BLADE DEVIATION ANGLE DISTRIBUTION (102% SPEED POINT)

212050315040

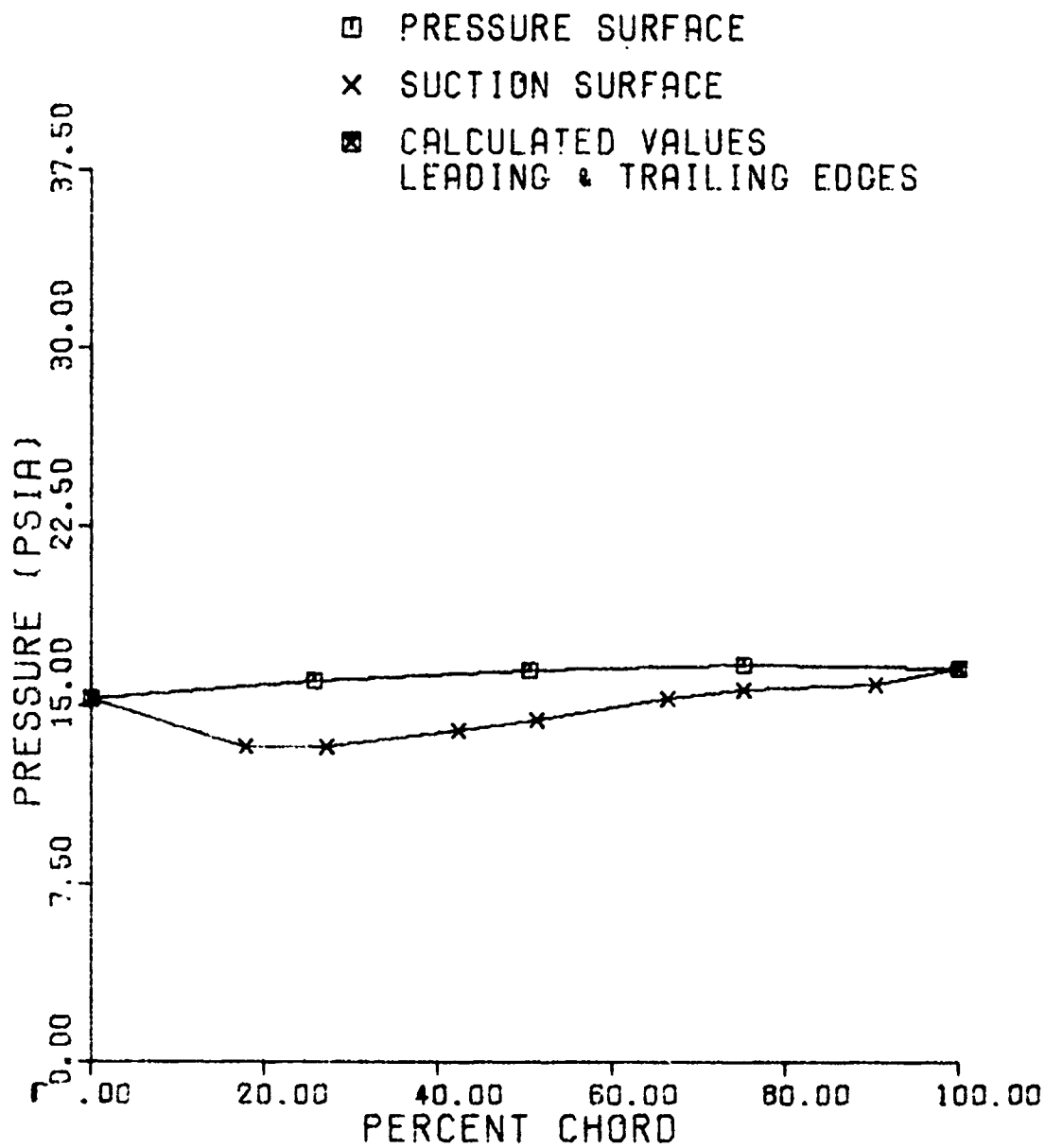


FIGURE 212. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 40% SPEED)

212050615050

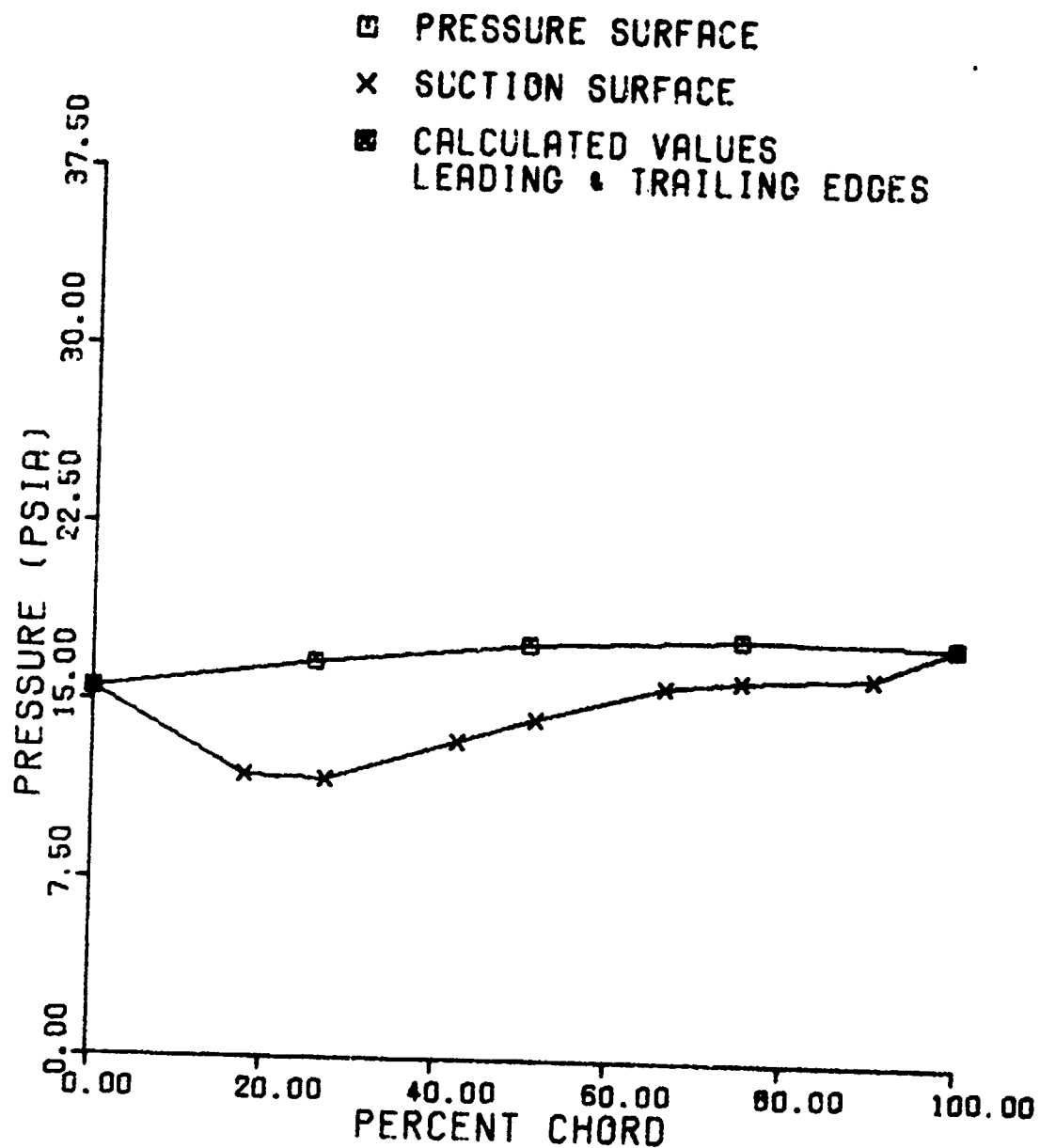


FIGURE 213. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 50% SPEED)

212051715560

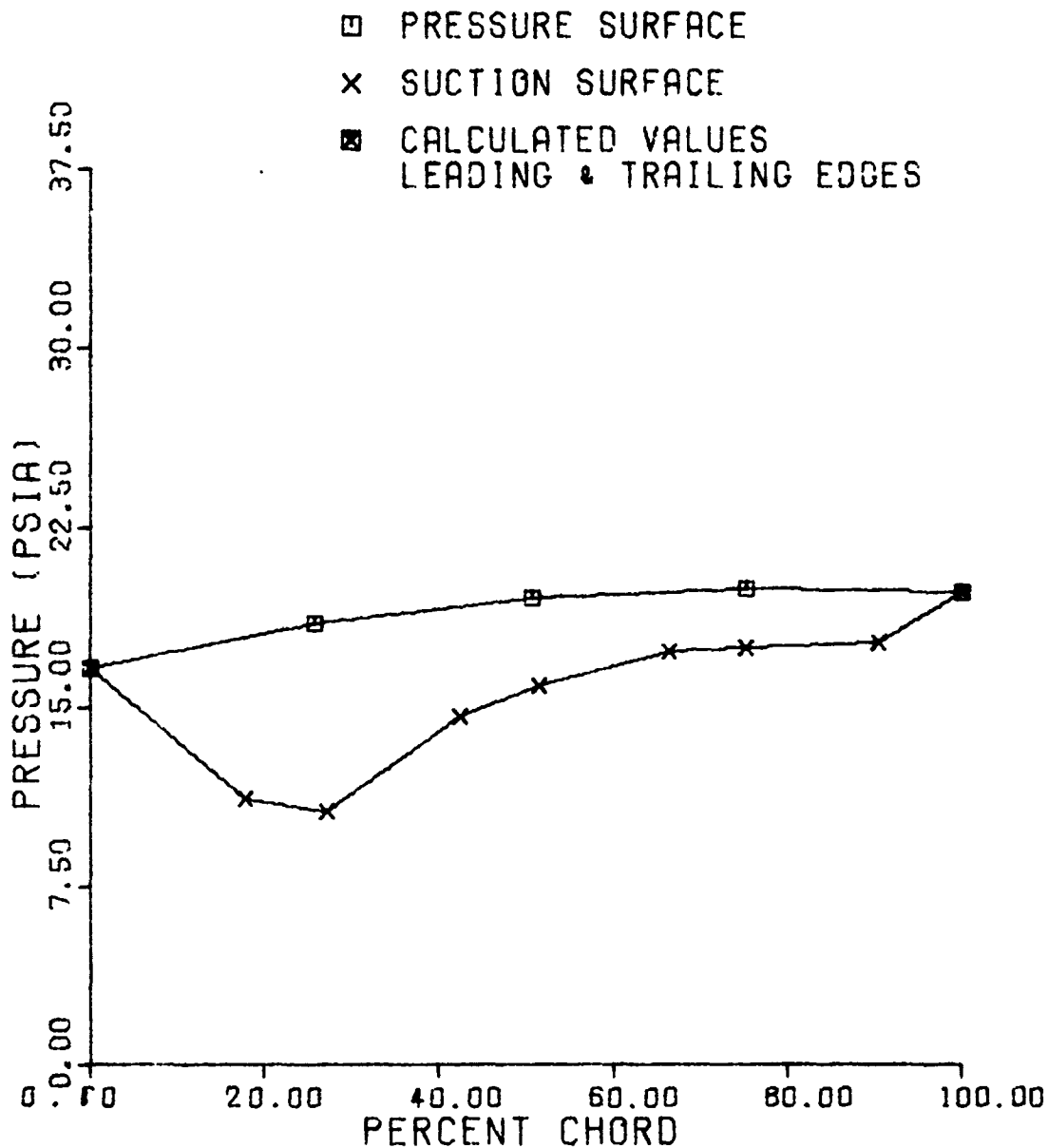


FIGURE 214. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 60% SPEED)

212070916170

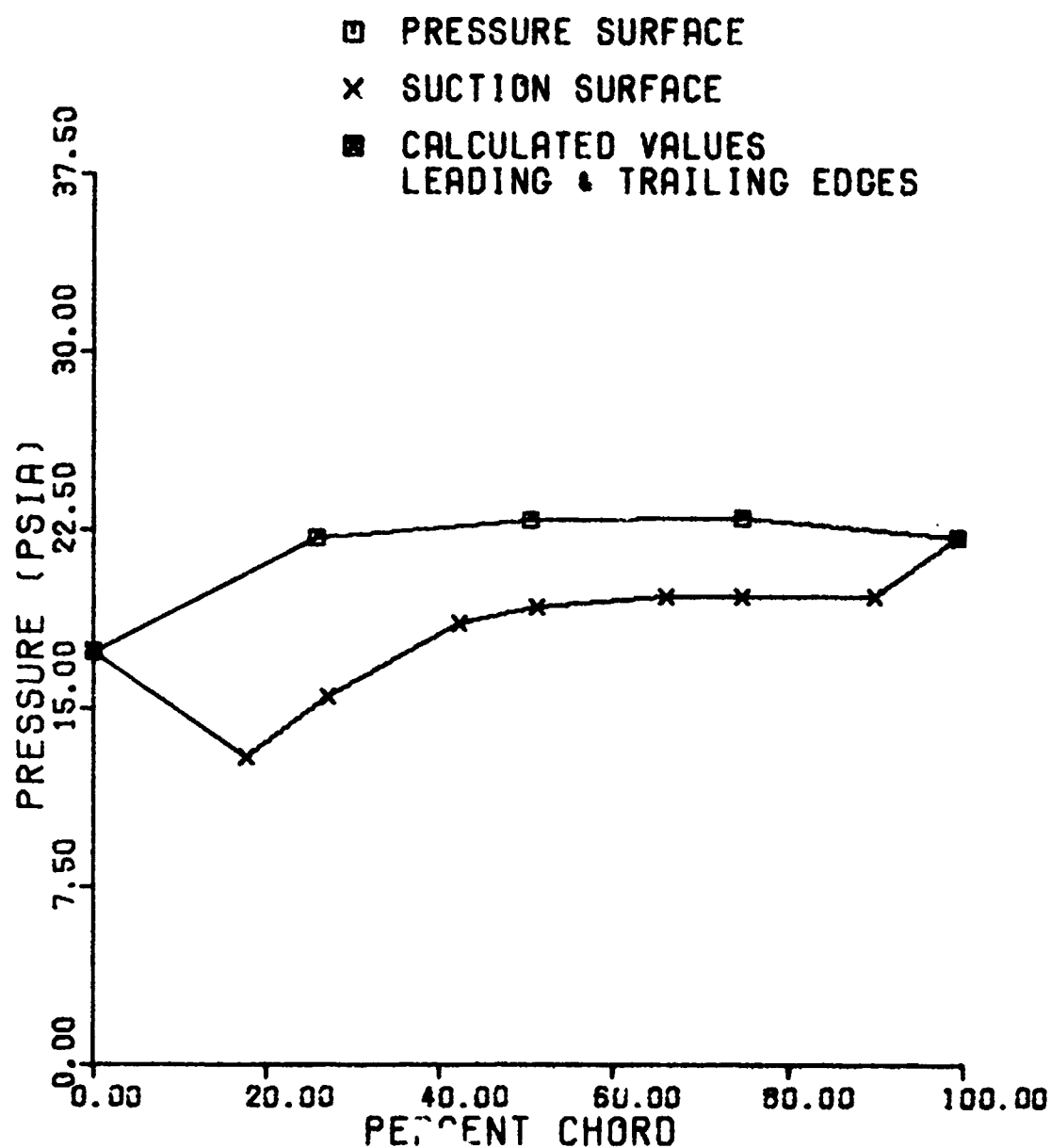


FIGURE 215. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 70% SPEED)

212071515980

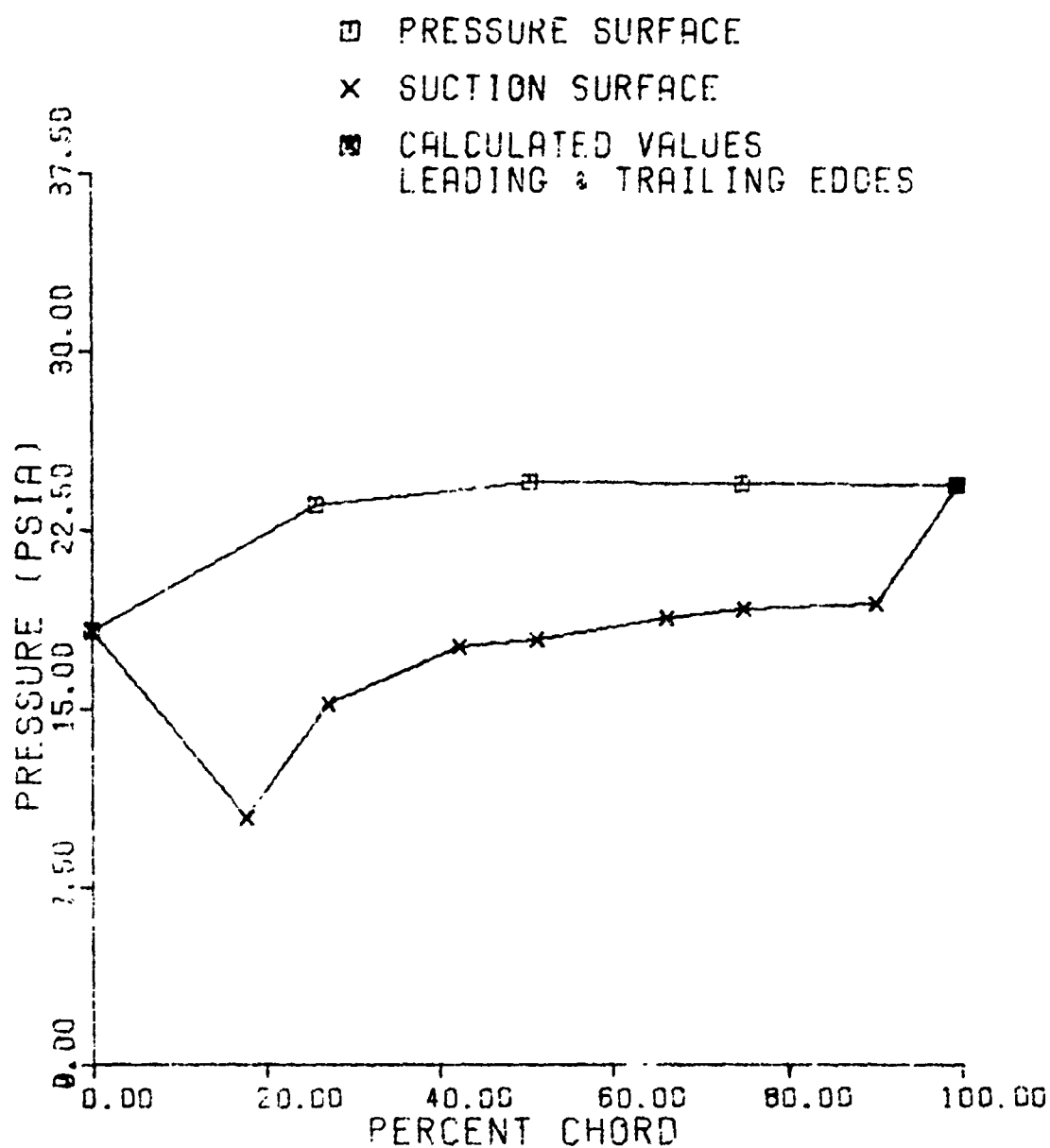


FIGURE 216. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 80% SPEED)



301181015885

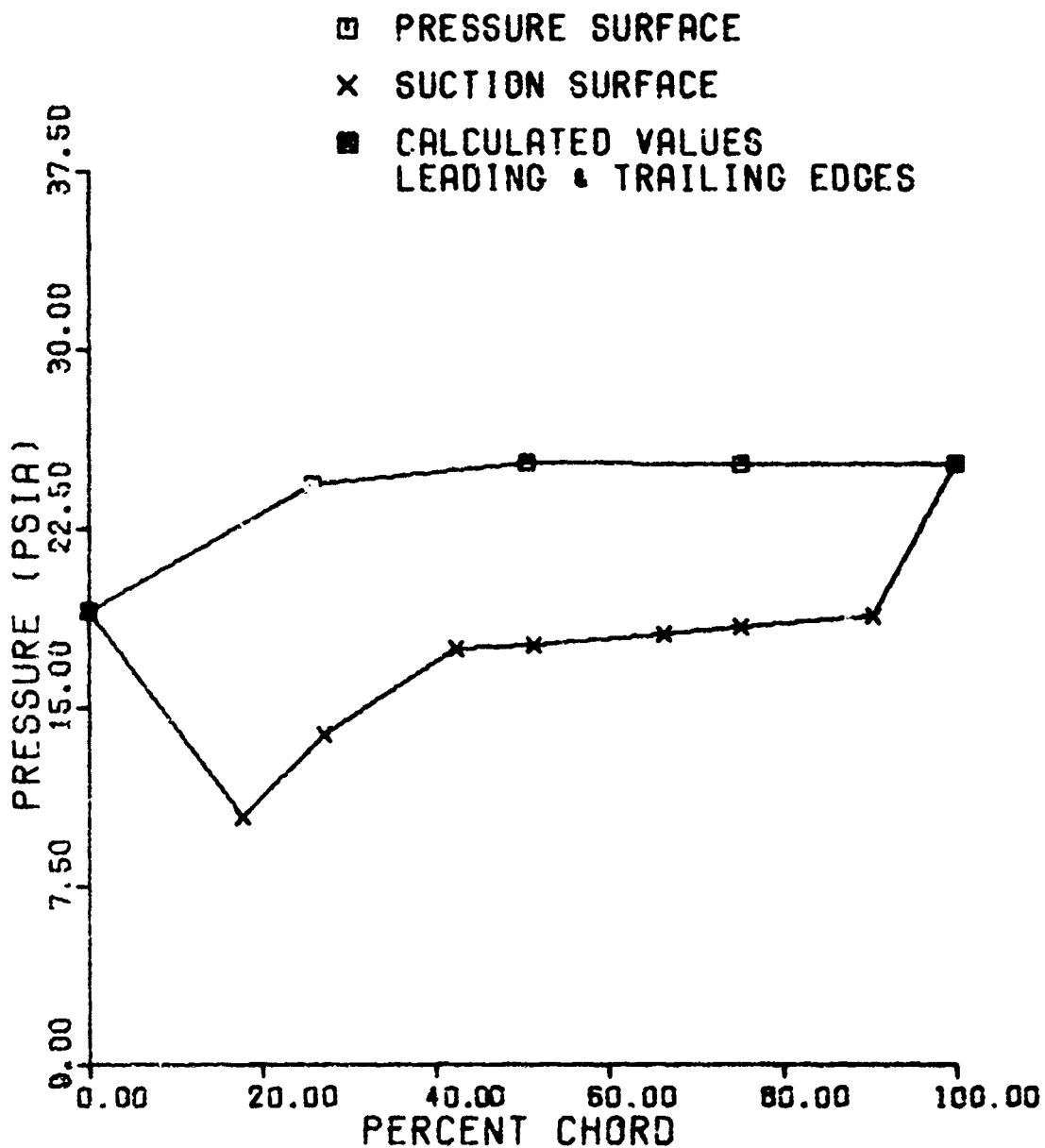


FIGURE 217. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 85% SPEED)

301181715890

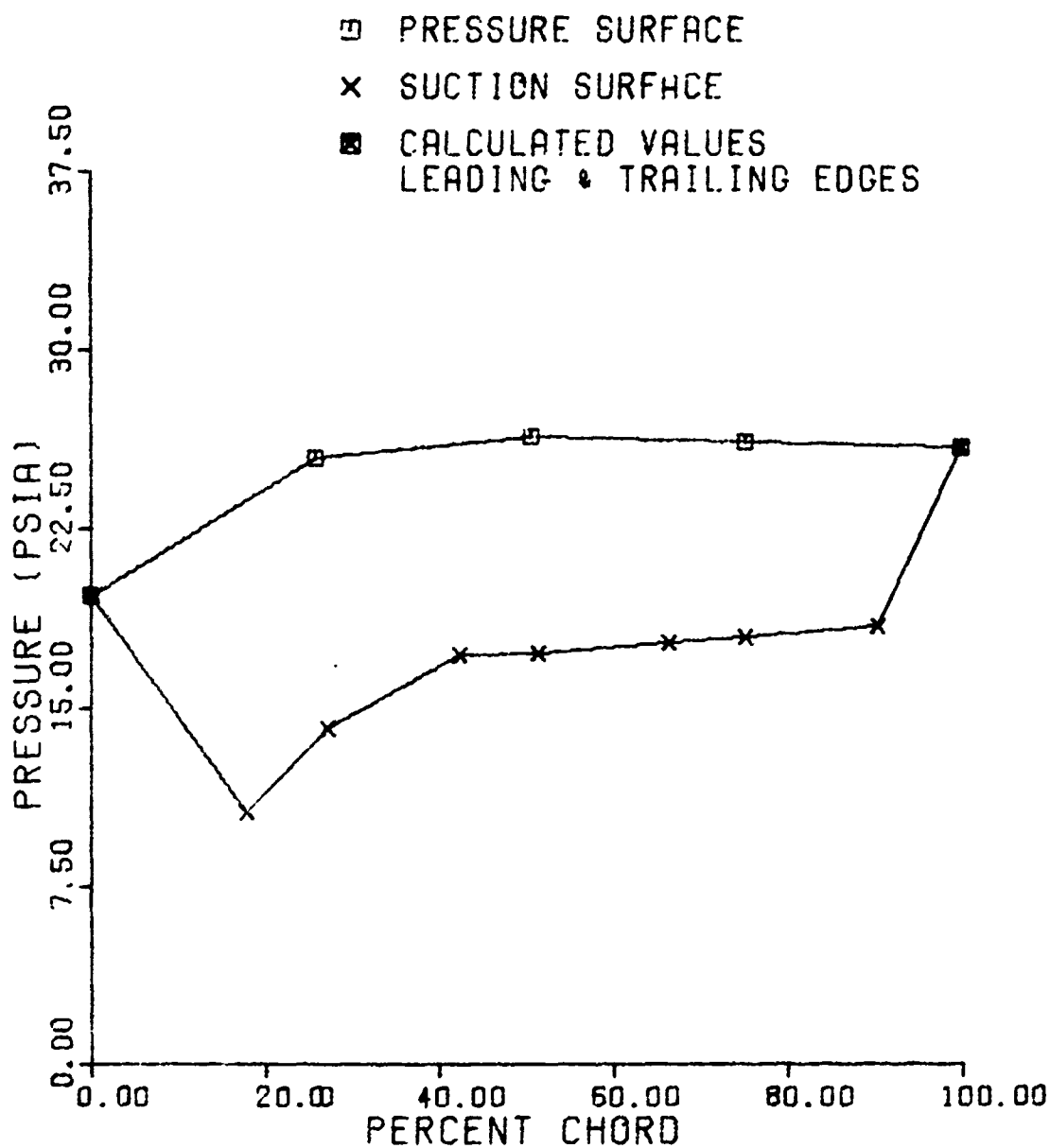


FIGURE 218. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 90% SPEED)

301230515695

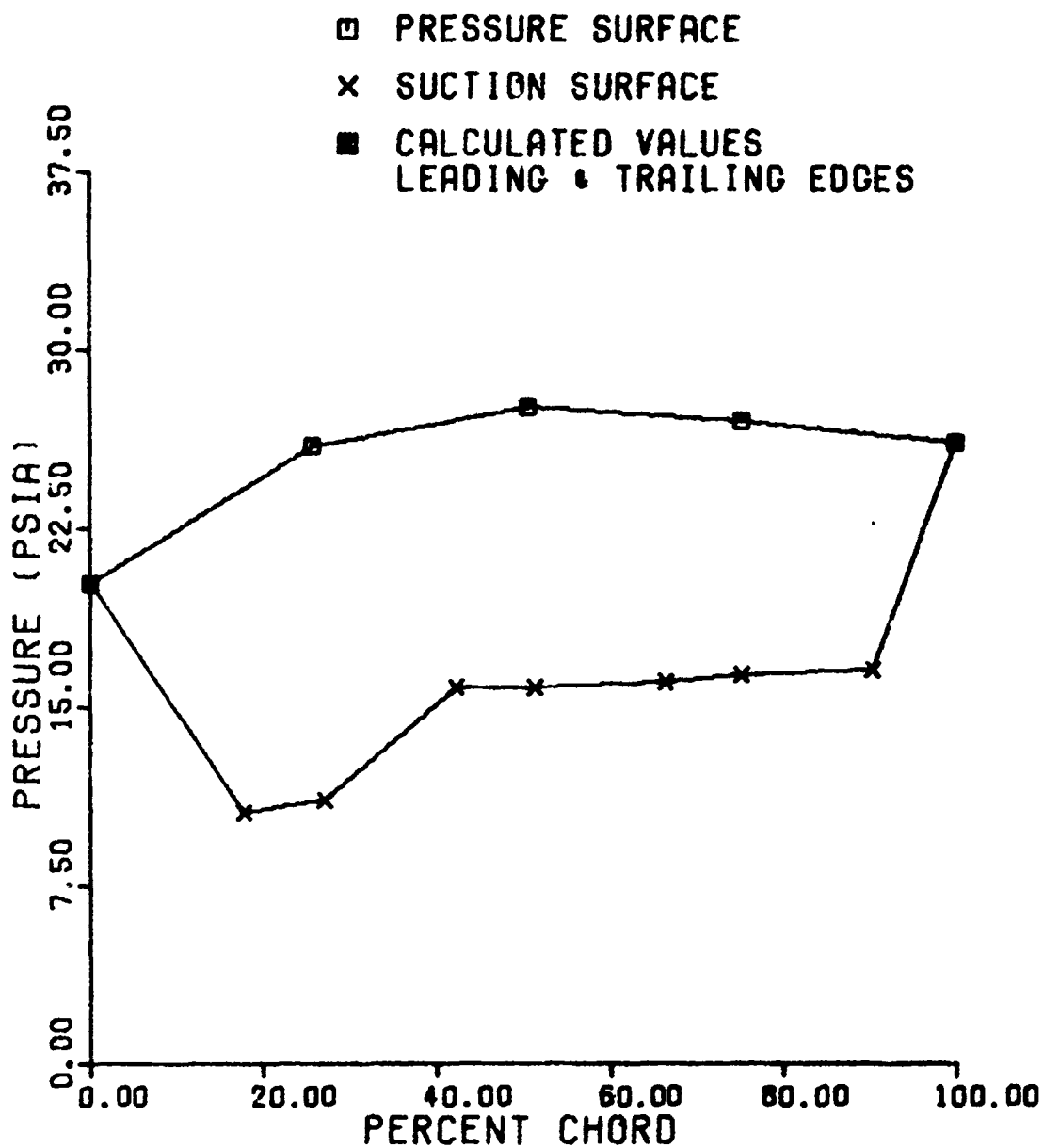


FIGURE 219. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 95% SPEED)

301231615700

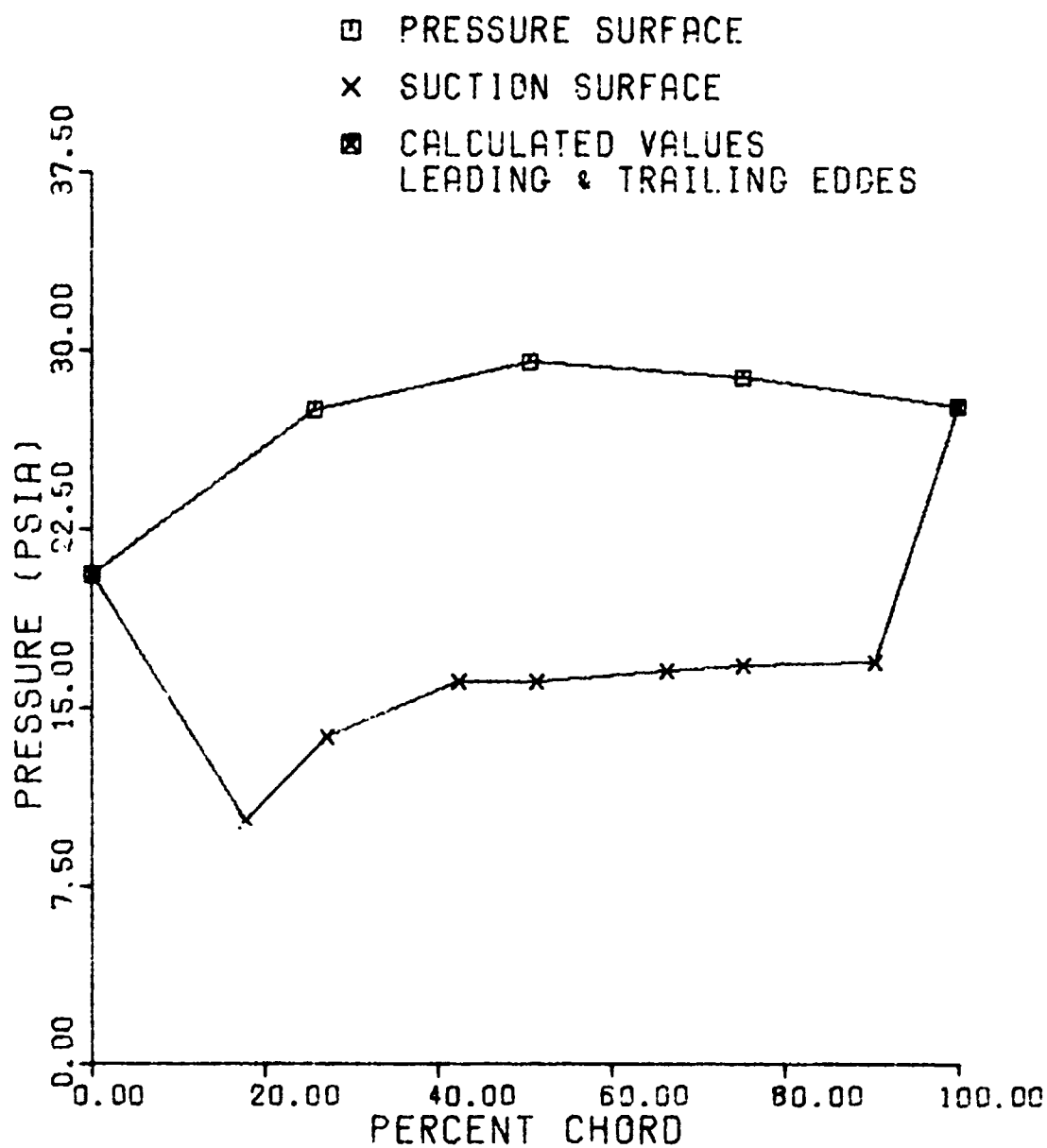


FIGURE 220. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 100% SPEED)

301240915602

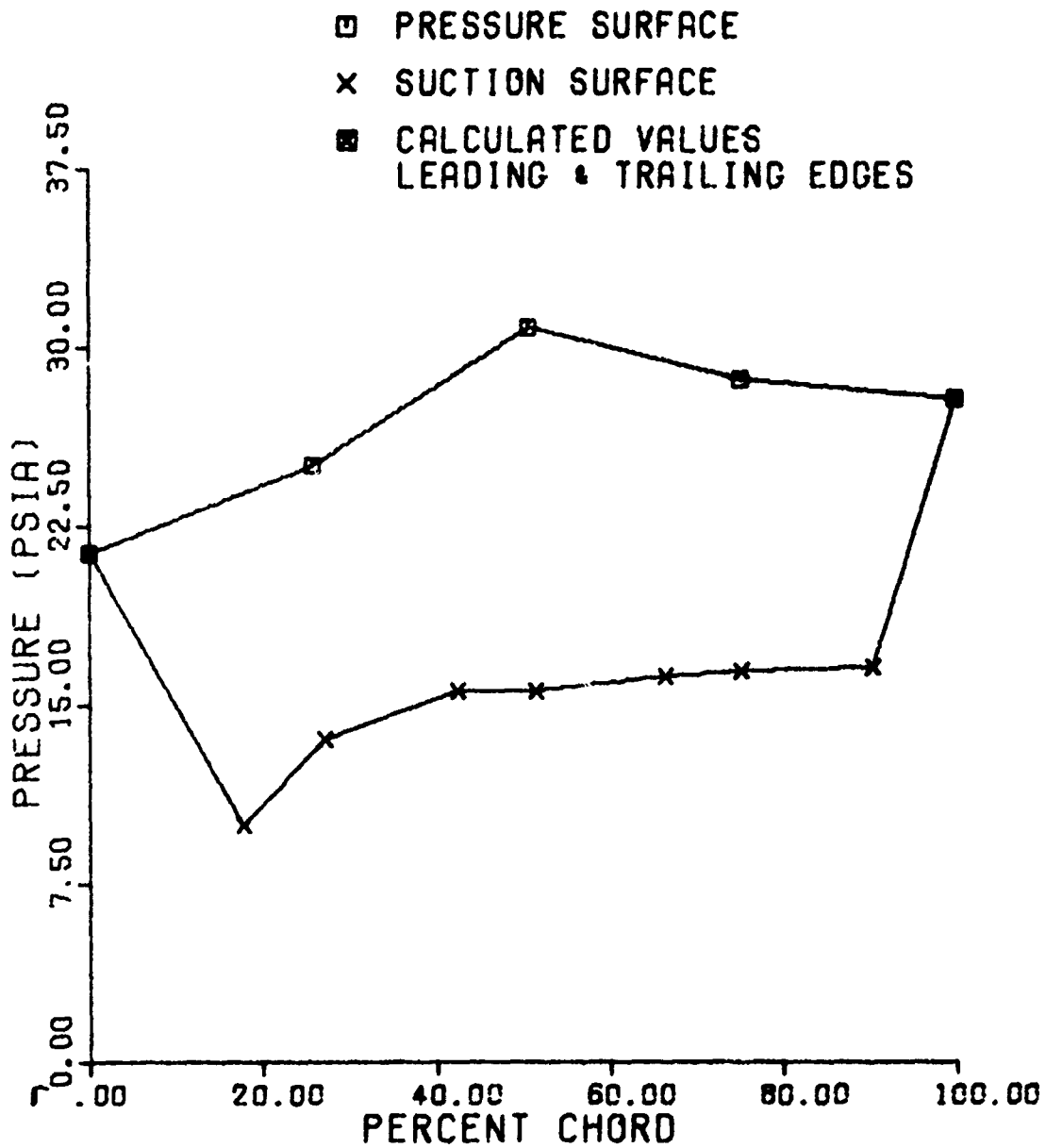


FIGURE 221. STATOR MID-SPAN SURFACE STATIC PRESSURE DISTRIBUTION (WITHIN-BLADE ANALYSIS, 102% SPEED)

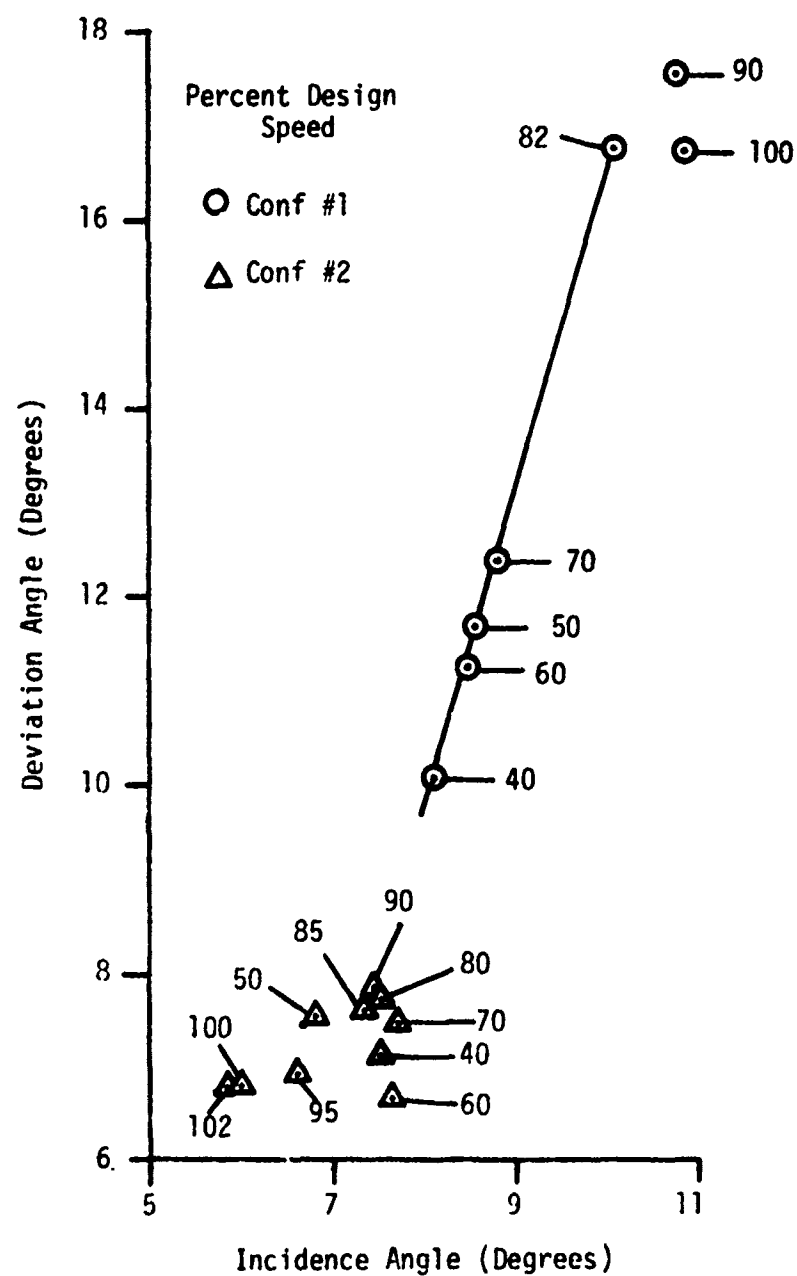


FIGURE 222. ROTOR MID-RADIUS DEVIATION VS INCIDENCE ANGLE

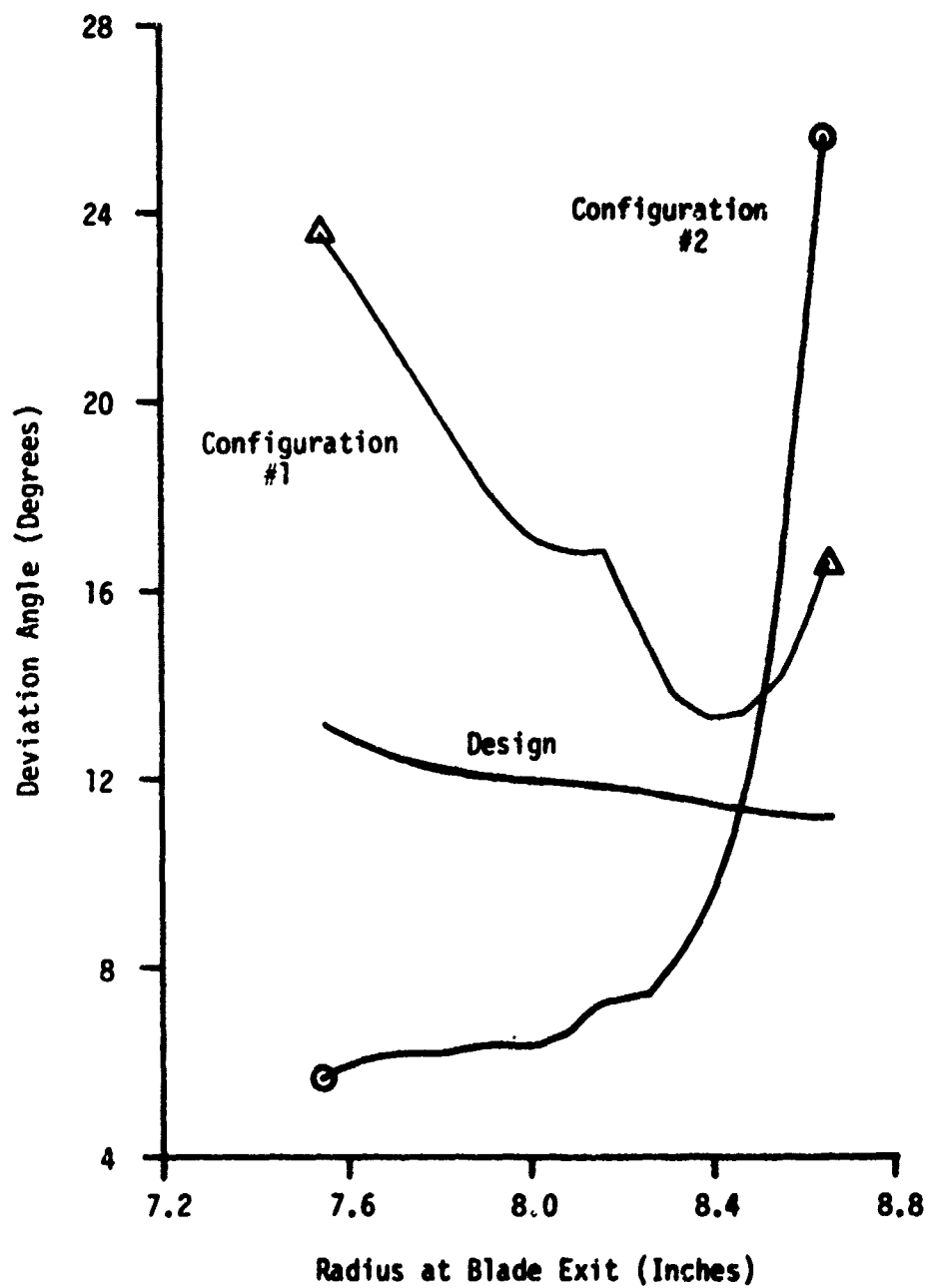


FIGURE 223. ROTOR DEVIATION ANGLE DISTRIBUTION

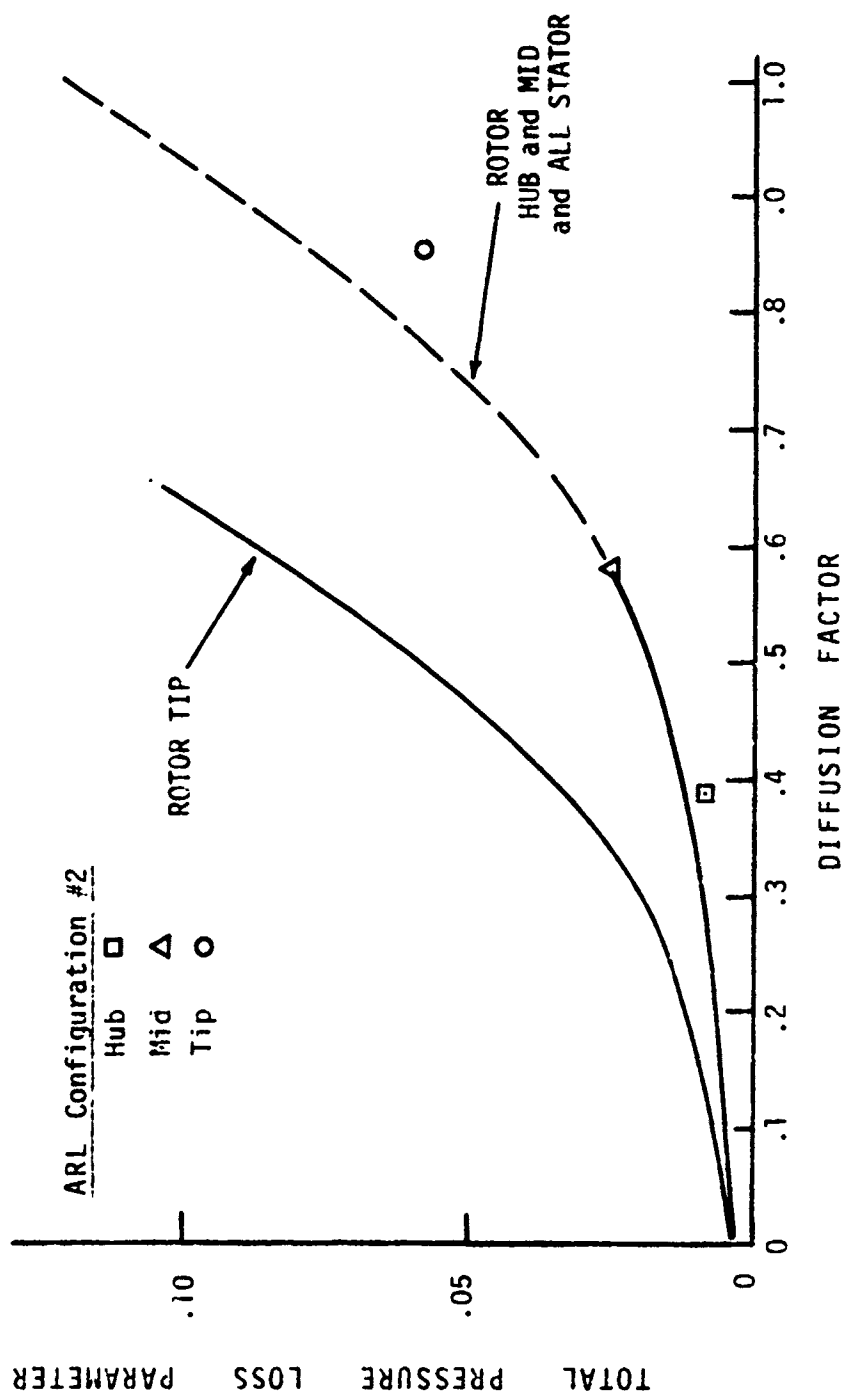


FIGURE 224. NACA COMPRESSOR LOSS CORRELATION WITH ARL CONFIGURATION #2 SUPERIMPOSED



## **APPENDIX A**

### **PHASE II WITHIN-BLADE ANALYSES (COMPUTER PRINTOUTS)**

This appendix presents the aerodynamic results (in the form of computer printouts) of the Phase II within-blade analyses for the ten test points selected for that analysis. The printout of input data which precedes the material presented herein has been removed in order to keep the number of pages to a minimum. The input data used in each of these analyses are presented in Appendix B.

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STATION 1  $\bar{r}_{L0n} = \bar{r}_{LL}$  ,  $\sigma_{L0n} = \sigma_{LL}$

2011.01.01

141





[illegible]

STATION	INTEGRATED PERFORMANCE	PRESSURE RATIO = 1.042	ISEN. EFF. = .901	POLY. EFF. = .902	DELTA T ON T = .013
1					
2					
3					
4					
5					
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91					
92					
93					
94					
95					
96					
97					
98					
99					
100					

STATION	FLOW FIELD DESCRIPTION
1	1
2	2
3	3
4	4
5	5
6	6
7	7
8	8
9	9
10	10
11	11
12	12
13	13
14	14
15	15
16	16
17	17
18	18
19	19
20	20
21	21
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87	87
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89	89
90	90
91	91
92	92
93	93
94	94
95	95
96	96
97	97
98	98
99	99
100	100

[illegible]



[illegible]

STATION 7 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.113 ISEN. EFF. = .866 POLY. EFF. = .887 DELTA T ON T = .835

STATION	8	FLOW FIELD DESCRIPTION
1	1	1
2	2	2
3	3	3
4	4	4
5	5	5
6	6	6
7	7	7
8	8	8
9	9	9
10	10	10
11	11	11
12	12	12
13	13	13
14	14	14
15	15	15
16	16	16
17	17	17
18	18	18
19	19	19
20	20	20
21	21	21
22	22	22
23	23	23
24	24	24
25	25	25
26	26	26
27	27	27
28	28	28
29	29	29
30	30	30
31	31	31
32	32	32
33	33	33
34	34	34
35	35	35
36	36	36
37	37	37
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63	63	63
64	64	64
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67	67	67
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74	74	74
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76	76	76
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82	82	82
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84	84	84
85	85	85
86	86	86
87	87	87
88	88	88
89	89	89
90	90	90
91	91	91
92	92	92
93	93	93
94	94	94
95	95	95
96	96	96
97	97	97
98	98	98
99	99	99
100	100	100

[illegible]

[illegible]

VIATION 3 FLOW FULL ESCALATION

STREAM LINE	Y-POS	V- TANG	TOTAL	TEMPERATURE T. TOTAL	TOTAL PRESSURE	YACH NO	ANGLE'S WHIRL SLOPE	RADIUS OF CURVATURE	SPECIFIC WEIGHT
1	0.000000	0.000000	0.000000	0.000000	0.000000	1	0.000000	0.000000	0.000000
2	0.000000	0.000000	0.000000	0.000000	0.000000	2	0.000000	0.000000	0.000000
3	0.000000	0.000000	0.000000	0.000000	0.000000	3	0.000000	0.000000	0.000000
4	0.000000	0.000000	0.000000	0.000000	0.000000	4	0.000000	0.000000	0.000000
5	0.000000	0.000000	0.000000	0.000000	0.000000	5	0.000000	0.000000	0.000000
6	0.000000	0.000000	0.000000	0.000000	0.000000	6	0.000000	0.000000	0.000000
7	0.000000	0.000000	0.000000	0.000000	0.000000	7	0.000000	0.000000	0.000000
8	0.000000	0.000000	0.000000	0.000000	0.000000	8	0.000000	0.000000	0.000000
9	0.000000	0.000000	0.000000	0.000000	0.000000	9	0.000000	0.000000	0.000000
10	0.000000	0.000000	0.000000	0.000000	0.000000	10	0.000000	0.000000	0.000000
11	0.000000	0.000000	0.000000	0.000000	0.000000	11	0.000000	0.000000	0.000000
12	0.000000	0.000000	0.000000	0.000000	0.000000	12	0.000000	0.000000	0.000000
13	0.000000	0.000000	0.000000	0.000000	0.000000	13	0.000000	0.000000	0.000000
14	0.000000	0.000000	0.000000	0.000000	0.000000	14	0.000000	0.000000	0.000000
15	0.000000	0.000000	0.000000	0.000000	0.000000	15	0.000000	0.000000	0.000000
16	0.000000	0.000000	0.000000	0.000000	0.000000	16	0.000000	0.000000	0.000000
17	0.000000	0.000000	0.000000	0.000000	0.000000	17	0.000000	0.000000	0.000000
18	0.000000	0.000000	0.000000	0.000000	0.000000	18	0.000000	0.000000	0.000000
19	0.000000	0.000000	0.000000	0.000000	0.000000	19	0.000000	0.000000	0.000000
20	0.000000	0.000000	0.000000	0.000000	0.000000	20	0.000000	0.000000	0.000000
21	0.000000	0.000000	0.000000	0.000000	0.000000	21	0.000000	0.000000	0.000000
22	0.000000	0.000000	0.000000	0.000000	0.000000	22	0.000000	0.000000	0.000000
23	0.000000	0.000000	0.000000	0.000000	0.000000	23	0.000000	0.000000	0.000000
24	0.000000	0.000000	0.000000	0.000000	0.000000	24	0.000000	0.000000	0.000000
25	0.000000	0.000000	0.000000	0.000000	0.000000	25	0.000000	0.000000	0.000000
26	0.000000	0.000000	0.000000	0.000000	0.000000	26	0.000000	0.000000	0.000000
27	0.000000	0.000000	0.000000	0.000000	0.000000	27	0.000000	0.000000	0.000000
28	0.000000	0.000000	0.000000	0.000000	0.000000	28	0.000000	0.000000	0.000000
29	0.000000	0.000000	0.000000	0.000000	0.000000	29	0.000000	0.000000	0.000000
30	0.000000	0.000000	0.000000	0.000000	0.000000	30	0.000000	0.000000	0.000000
31	0.000000	0.000000	0.000000	0.000000	0.000000	31	0.000000	0.000000	0.000000
32	0.000000	0.000000	0.000000	0.000000	0.000000	32	0.000000	0.000000	0.000000
33	0.000								









[illegible][illegible]

STATION 13 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.241 ISEN. EFF. = .875 POLY. EFF. = .879 DELTA T ON T = .873



[illegible][illegible]

DATA

UNIT	NO. 13	NO. 14	NO. 15	NO. 16	NO. 17	NO. 18	NO. 19	NO. 20	NO. 21	NO. 22	NO. 23	NO. 24	NO. 25	NO. 26	NO. 27	NO. 28	NO. 29	NO. 30	NO. 31	NO. 32	NO. 33	NO. 34	NO. 35	NO. 36	NO. 37	NO. 38	NO. 39	NO. 40	NO. 41	NO. 42	NO. 43	NO. 44	NO. 45	NO. 46	NO. 47	NO. 48	NO. 49	NO. 50	NO. 51	NO. 52	NO. 53	NO. 54	NO. 55	NO. 56	NO. 57	NO. 58	NO. 59	NO. 60	NO. 61	NO. 62	NO. 63	NO. 64	NO. 65	NO. 66	NO. 67	NO. 68	NO. 69	NO. 70	NO. 71	NO. 72	NO. 73	NO. 74	NO. 75	NO. 76	NO. 77	NO. 78	NO. 79	NO. 80	NO. 81	NO. 82	NO. 83	NO. 84	NO. 85	NO. 86	NO. 87	NO. 88	NO. 89	NO. 90	NO. 91	NO. 92	NO. 93	NO. 94	NO. 95	NO. 96	NO. 97	NO. 98	NO. 99	NO. 100
UNIT	NO. 13	NO. 14	NO. 15	NO. 16	NO. 17	NO. 18	NO. 19	NO. 20	NO. 21	NO. 22	NO. 23	NO. 24	NO. 25	NO. 26	NO. 27	NO. 28	NO. 29	NO. 30	NO. 31	NO. 32	NO. 33	NO. 34	NO. 35	NO. 36	NO. 37	NO. 38	NO. 39	NO. 40	NO. 41	NO. 42	NO. 43	NO. 44	NO. 45	NO. 46	NO. 47	NO. 48	NO. 49	NO. 50	NO. 51	NO. 52	NO. 53	NO. 54	NO. 55	NO. 56	NO. 57	NO. 58	NO. 59	NO. 60	NO. 61	NO. 62	NO. 63	NO. 64	NO. 65	NO. 66	NO. 67	NO. 68	NO. 69	NO. 70	NO. 71	NO. 72	NO. 73	NO. 74	NO. 75	NO. 76	NO. 77	NO. 78	NO. 79	NO. 80	NO. 81	NO. 82	NO. 83	NO. 84	NO. 85	NO. 86	NO. 87	NO. 88	NO. 89	NO. 90	NO. 91	NO. 92	NO. 93	NO. 94	NO. 95	NO. 96	NO. 97	NO. 98	NO. 99	NO. 100

STATISTICS, UNIT, REFERENCE, PRESSURE, RATIO = 1.233, ISOTOPE, EFF. = .845, POLY. EFF. = .050, DELTA T ON T = .073



ROUTED TO - FOR FAN -

[illegible]

## STATJN PLRFO24ANC.

[illegible]

WAKE 1400 30JNJA07 L4V:2 BLOCKAGES (PERCENT)

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SUMMARY POINT NO. 1 THE CALCULATION IS CONVERGED PASS 20

1-51 POINT TITLE = 212050315040

1730 POINT 1 TIME = 22.690000000000  
FLOW = 10.22 CM<sup>3</sup>/MIN APL=2 PRESSURE RATIO = 1.233 ISOTHERMATIC EFFY = .9453 POLYTROPIC EFFY = .8499 DEL T/T = .0727

### SUMMARY OF 1 TEST POINTS

POINT NO.	TEST POINT TITLE	STATUS OF CALCULATION	FLOW RATE LBS/SEC	SPEED RPM	---COLOR--- PRESSURE LBS/IN	---STAGE--- PRESSURE LBS/IN	FLOW/CHARGE (LBS/IN)
1	2100-03150+0	CONV=35.0 AFTER 20 PASSES	10.214	6154.2	1.250	1.233	.26789









[illegible]

```
STATION 3  INTGRATED PERFORMANCE  PRESSURE RATIO = 1.13,  I2/I0 = .906  P.O.Y. EFF. = .907  DELTA T ON T = .041
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[illegible]



[illegible][illegible]

STAT 13 PC93 C-12

[illegible]





[illegible][illegible]

$\Delta T = 1.00$  in.  $\Delta T = 0.95$   $\Delta T = 0.113$

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[illegible][illegible]

```
STATION 13 INTGRAL FORMATION = 0.339 DELTA TON T = 0.113
POLYMER EFF. = 0.371 ISEN. EFF. = 0.332
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[illegible]

[illegible]

STATION 3 INTEGRATED PERFORMANCE: PRESSURE RATIO = 1.115 ISEN, EFF. = .915 POLY. EFF. = .917 DELTA T ON T = .126

174

STATION : FLOW FIELD DESCRIPTION

STREAM LINE	RADIUS X	Y- COORDINATE	TEMPERATURE TOTAL	TEMPERATURE STATIC	PR-SURFACE TOTAL	Y- COORDINATE	ANGLE WHEN	RADIUS OF CURVATURE	SPEED METER
1	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
2	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
3	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
4	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
5	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
6	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
7	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
8	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
9	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
10	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
11	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
12	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
13	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
14	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
15	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
16	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
17	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
18	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
19	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
20	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
21	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
22	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
23	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
24	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
25	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
26	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
27	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
28	1.000000	0.000000	1.000000	1.000000	1.000000	0.000000	0.000000	1.000000	1.000000
29	1								

LOCAL  
BLADE-ANGLE  
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NO. 1  
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SPEED  
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PRESSURE  
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PRESSURE  
RATIO  
DELTA T  
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EFFICIENCY

[illegible]

STATION, INTEGRATED PERFORMANCE PRESSURE RATIO = 1.19; ISEN. EFF. = .897 POLY. EFF. = .899 DELTA T ON T = .060

STATION	7	FLCM	FIELD	DESCRIPTION
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[illegible]



LOCATION: 3L4J5-205L-5  
SECTION: 25A

[illegible]

STALLION #	INT:GRAT_2	P_2PERFORMANCE	P_2SSURE	RATIO = 1.472	ISEN	EFF % = .900	PC.Y.	EFF % = .905	DELTA T ON Y = .130
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## STATION , FLOW FIELD DESCRIPTION

[illegible]



179





STATION 13 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.005 ISEN. EFF. = .857 POLY. EFF. = .867 DELTA T ON T = .166



[illegible]

BLAD- JATA

[illegible]

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STATION 15  INI-GRATED P-RFORMANCE  PRESSURE RATIO = 1.564  IS-N EFF. = .814  POLY. EFF. = .025  DELTA T DM Y = .106
```





**STREAM**

## REVIEWS

-----S-----TOTAL  
4-BT C13  
-----A-----I1C13-----

TEMPERATURE

---PRESUSPENSE---

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---ANGLE SLOPE

### RADIUS OF CURVATURE

**SPENCER**

STATION	2	FLOW FIELD DESCRIPTION
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**STREAM**

**RADIUS**

-----VELOCITY:-----  
-----TOTAL-----

TEMPERATURES--

---PRESUPES---

## MACH

---ANGLE\$---  
UNIT 1, OBE

**RADIUS OF**

**SECRET**









[illegible]

STATION 6 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.29% ISEN. EFF. = .890 POLY. EFF. = .892 DELTA T ON T = .004

STATION	7	FLOW FIELD DESCRIPTION
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[illegible]

STATION 7 INLET PAV. SURFACE RATIO = 1.431 ISEN EFF. = .99 POLY. EFF. = .99 DELTA T ON T = .136

STATION	FLUM FIELD DESCRIPTION
1	FLUM FIELD DESCRIPTION

BLADE DATA  
 -----  
 LOGAT SLASH-ANGLES  
 SECTION LEAN  
 REL ANGLE  
 FLOW DEVIATION  
 LOSS  
 SPEED  
 RELATIVE MACH NO  
 RELATIVE VELOCITY  
 RELATIVE TEMPERATURE  
 PRESSURE RATIO  
 DELTA T  
 ON T  
 DELTA T ON T = .189

STATION 6 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.721 ISEN. EFF. = .888 POLY. EFF. = .897 DELTA T ON T = .189

STATION 9 FLOW FIELD DESCRIPTION

STREAM LINE  
 RADIUS  
 MERID  
 VELOCITIES  
 TOTAL  
 TEMPERATURES  
 TOTAL  
 PRESSURES  
 TOTAL  
 MACH NO  
 ANGLES  
 SLOPE  
 RADIUS OF CURVATURE  
 SPECIFIC WEIGHT

BLADE DATA									
LOCAT	SECTION	REL ANGLE	REL FLOW	DEVIATION	COEFF	BLADE	RELATIVE	RELATIVE	ISENTROPIC
ION		INCLIN	ANGLE	INC		SECT	MACH NO	VELOCITY	EFFICIENCY
1	1	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
2	2	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0
3	3	30.0	30.0	30.0	30.0	30.0	30.0	30.0	30.0
4	4	40.0	40.0	40.0	40.0	40.0	40.0	40.0	40.0
5	5	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
6	6	60.0	60.0	60.0	60.0	60.0	60.0	60.0	60.0
7	7	70.0	70.0	70.0	70.0	70.0	70.0	70.0	70.0
8	8	80.0	80.0	80.0	80.0	80.0	80.0	80.0	80.0
9	9	90.0	90.0	90.0	90.0	90.0	90.0	90.0	90.0
10	10	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0

STATION 9 INT-GRATED PERFORMANCE PRESSURE RATIO = 1.920 ISEN. EFF. = .981 POLY. EFF. = .692 DELTA T ON T = .232

STATION 10 FLOW FIELD DESCRIPTION

STREAM	RADIUS	PERIO	VEL	Q	TANGEN	IS	TOTAL	TEMPERATURES	STATIC	TOTAL	PRESSURES	STATIC	MACH	ANGLE	SLOPE	RADIUS OF	SPECIFIC	EFFICIENCY
1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0
3	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0
4	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
5	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
6	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0
7	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0
8	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0
9	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0
10	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0



STATION 12 INT. GATED PERFORMANCE PRESSURE RATIO = 1.632 ISEN EFF. = .053 POLY. EFF. = .071 DELTA T ON T = .232





















STATION 3 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.172 I<sub>EN</sub> EFF. = .664 POLY. EFF. = .666 DELTA T ON T = .083

STATION 6 FLOW FIELD DESCRIPTION



STATION 7 INJECTED PERFORMANCE PRESSURE RATIO = 1.645 ISEN EFF. = .870 POLY. EFF. = .986 DELTA T ON T = .176



BLADE DATA

LOGAT SECTION LEIN  
 REL FLOW INCIDENCE ANGLE  
 LOSS COEFF  
 BLADE SPEED  
 RELATIVE MACH NO  
 VELOCITY  
 PRESSURE  
 RELATIVE TEMPERATURE  
 PRESSURE RATIO  
 DELTA T  
 EFFICIENCY

STATION 9 INTEGRATED PERFORMANCE PRESSURE RATIO = 2.271 ISEN EFF = .985 POLY EFF = .888 DELTA T ON T = .388

STATION 10 FLOW FIELD DESCRIPTION

STREAM LINE  
 RADIUS  
 VELOCITY  
 MACH NO  
 PRESSURE  
 TEMPERATURE  
 TOTAL  
 RADIUS OF CURVATURE  
 ANGLE  
 SLOPE  
 SPECIFIC HEIGHT

STATION 11	INT:GRADED	PERFORMANCE	PRESSURE RATIO = 2.271	ISEN. EFF. = .865	POLY. EFF. = .880	DELTA T ON T = .384
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# STATION 16 FLOW FIELD DESCRIPTION

STREAM -LINE	RADIUS	HERD	VELOCITIES	TOTAL	TEMPERATURES	STATIC	TOTAL	PR:SSURES	STATIC	MACH	NO	ANGLE	SLOPE	RADIUS OF	CURVATURE	SPECIFIC	WEIGHT
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# STATION 17 FLOW FIELD DESCRIPTION

STREAM -LINE	RADIUS	HERD	VELOCITIES	TOTAL	TEMPERATURES	STATIC	TOTAL	PR:SSURES	STATIC	MACH	NO	ANGLE	SLOPE	RADIUS OF	CURVATURE	SPECIFIC	WEIGHT
.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....



6. TEST POINT 301281015885 (85%)



STATION DATA	STATION 1	STATION 2	STATION 3	STATION 4	STATION 5	STATION 6	STATION 7	STATION 8	STATION 9	STATION 10	STATION 11	STATION 12	STATION 13	STATION 14	STATION 15	STATION 16	STATION 17	STATION 18	STATION 19	STATION 20	STATION 21	STATION 22	STATION 23	STATION 24	STATION 25	STATION 26	STATION 27	STATION 28	STATION 29	STATION 30	STATION 31	STATION 32	STATION 33	STATION 34	STATION 35	STATION 36	STATION 37	STATION 38	STATION 39	STATION 40	STATION 41	STATION 42	STATION 43	STATION 44	STATION 45	STATION 46	STATION 47	STATION 48	STATION 49	STATION 50	STATION 51	STATION 52	STATION 53	STATION 54	STATION 55	STATION 56	STATION 57	STATION 58	STATION 59	STATION 60	STATION 61	STATION 62	STATION 63	STATION 64	STATION 65	STATION 66	STATION 67	STATION 68	STATION 69	STATION 70	STATION 71	STATION 72	STATION 73	STATION 74	STATION 75	STATION 76	STATION 77	STATION 78	STATION 79	STATION 80	STATION 81	STATION 82	STATION 83	STATION 84	STATION 85	STATION 86	STATION 87	STATION 88	STATION 89	STATION 90	STATION 91	STATION 92	STATION 93	STATION 94	STATION 95	STATION 96	STATION 97	STATION 98	STATION 99	STATION 100
STATION DATA	STATION 1	STATION 2	STATION 3	STATION 4	STATION 5	STATION 6	STATION 7	STATION 8	STATION 9	STATION 10	STATION 11	STATION 12	STATION 13	STATION 14	STATION 15	STATION 16	STATION 17	STATION 18	STATION 19	STATION 20	STATION 21	STATION 22	STATION 23	STATION 24	STATION 25	STATION 26	STATION 27	STATION 28	STATION 29	STATION 30	STATION 31	STATION 32	STATION 33	STATION 34	STATION 35	STATION 36	STATION 37	STATION 38	STATION 39	STATION 40	STATION 41	STATION 42	STATION 43	STATION 44	STATION 45	STATION 46	STATION 47	STATION 48	STATION 49	STATION 50	STATION 51	STATION 52	STATION 53	STATION 54	STATION 55	STATION 56	STATION 57	STATION 58	STATION 59	STATION 60	STATION 61	STATION 62	STATION 63	STATION 64	STATION 65	STATION 66	STATION 67	STATION 68	STATION 69	STATION 70	STATION 71	STATION 72	STATION 73	STATION 74	STATION 75	STATION 76	STATION 77	STATION 78	STATION 79	STATION 80	STATION 81	STATION 82	STATION 83	STATION 84	STATION 85	STATION 86	STATION 87	STATION 88	STATION 89	STATION 90	STATION 91	STATION 92	STATION 93	STATION 94	STATION 95	STATION 96	STATION 97	STATION 98	STATION 99	STATION 100





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[illegible]

STATION	INTEGRATED PERFORMANCE	PRESSURE RATIO	ISEN. EFF.	POLY. EFF.	DELTA T ON T
117		1.403	.870	.876	.117

STATION	7	FLOW FIELD	DESCRIP.
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**STREAM-  
LINE**

[illegible]

STATION	FLOW (CFS)	DESCRIPTION
1	100	...
2	200	...
3	300	...
4	400	...
5	500	...
6	600	...
7	700	...
8	800	...
9	900	...
10	1000	...







STATION 12 FLOW FIELD DESCRIPTION

STREAM -LINE-	RADIUS	PERIOD	PERCENTAGE	TOTAL	TEMPERATURE -STATIC- TOTAL	PER-SURFACE TOTAL	MACH NO	WIND ANGLE	RADIUS OF CURVATURE	SPEED OF SOUND
.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....

225

LOCAL SECTION	SECTION -LINE-	ANGLE	PERCENTAGE	TOTAL	TEMPERATURE -STATIC- TOTAL	PER-SURFACE TOTAL	MACH NO	WIND ANGLE	RADIUS OF CURVATURE	SPEED OF SOUND
.....	.....	.....	.....	.....	.....	.....	.....	.....	.....	.....

STATION 12 INITIAL PERFORMANCE PRESSURE RATIO = 2.405 ISENTROPIC EFF. = .826 POLY. EFF. = .846 DELTA T ON T = .343







[illegible][illegible]

BLADE= 3ATA

[illegible][illegible]

STATION 15	INTEGRATED PERFORMANCE	PRESSURE RATIO = 2.147	ISEN. EFF. = .726	POLY. EFF. = .754	DELTA T ON T = .343
1	1.000	2.147	.726	.754	.343
2	1.000	2.147	.726	.754	.343
3	1.000	2.147	.726	.754	.343
4	1.000	2.147	.726	.754	.343
5	1.000	2.147	.726	.754	.343
6	1.000	2.147	.726	.754	.343
7	1.000	2.147	.726	.754	.343
8	1.000	2.147	.726	.754	.343
9	1.000	2.147	.726	.754	.343
10	1.000	2.147	.726	.754	.343
11	1.000	2.147	.726	.754	.343
12	1.000	2.147	.726	.754	.343
13	1.000	2.147	.726	.754	.343
14	1.000	2.147	.726	.754	.343
15	1.000	2.147	.726	.754	.343
16	1.000	2.147	.726	.754	.343
17	1.000	2.147	.726	.754	.343
18	1.000	2.147	.726	.754	.343
19	1.000	2.147	.726	.754	.343
20	1.000	2.147	.726	.754	.343
21	1.000	2.147	.726	.754	.343
22	1.000	2.147	.726	.754	.343
23	1.000	2.147	.726	.754	.343
24	1.000	2.147	.726	.754	.343
25	1.000	2.147	.726	.754	.343
26	1.000	2.147	.726	.754	.343
27	1.000	2.147	.726	.754	.343
28	1.000	2.147	.726	.754	.343
29	1.000	2.147	.726	.754	.343
30	1.000	2.147	.726	.754	.343
31	1.000	2.147	.726	.754	.343
32	1.000	2.147	.726	.754	.343
33	1.000	2.147	.726	.754	.343
34	1.000	2.147	.726	.754	.343
35	1.000	2.147	.726	.754	.343
36	1.000	2.147	.726	.754	.343
37	1.000	2.147	.726	.754	.343
38	1.000	2.147	.726	.754	.343
39	1.000	2.147	.726	.754	.343
40	1.000	2.147	.726	.754	.343
41	1.000	2.147	.726	.754	.343
42	1.000	2.147	.726	.754	.343
43	1.000	2.147	.726	.754	.343
44	1.000	2.147	.726	.754	.343
45	1.000	2.147	.726	.754	.343
46	1.000	2.147	.726	.754	.343
47	1.000	2.147	.726	.754	.343
48	1.000	2.147	.726	.754	.343
49	1.000	2.147	.726	.754	.343
50	1.000	2.147	.726	.754	.343
51	1.000	2.147	.726	.754	.343
52	1.000	2.147	.726	.754	.343
53	1.000	2.147	.726	.754	.343
54	1.000	2.147	.726	.754	.343
55	1.000	2.147	.726	.754	.343
56	1.000	2.147	.726	.754	.343
57	1.000	2.147	.726	.754	.343
58	1.000	2.147	.726	.754	.343
59	1.000	2.147	.726	.754	.343
60	1.000	2.147	.726	.754	.343
61	1.000	2.147	.726	.754	.343
62	1.000	2.147	.726	.754	.343
63	1.000	2.14			

[illegible][illegible]

[illegible][illegible]

SUMMARY									
POINT NO.	1	2	3	4	5	6	7	8	9
STATION	100	100	100	100	100	100	100	100	100
ADJUST	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ADJUST	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
INT. CLOCK	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1 THE CALCULATION IS CONVERGED PASS 20									

FLOW = 20.00 SPEED = 17341.4 PRESSURE RATIO = 2.107 ISENTROPIC EFFY = .7264 POLYTROPIC EFFY = .7543 DEL T/° = .3634

TEST POINT TITLE	STATUS OF CALCULATION	FLOW	SPEED	---ROTOR---	---STAGE---	FLOW/ STAGE
1						
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90						

	RAT	PRESSURE RATIO	I <sub>SEN</sub> EFFY	(UNOKE FLOW)
L3S/S=C				
NCH				

	CONV-REGD AFTER 20 PASSES			
30119161868	20.001	1714.4	.057	2.107 .726 .54559

1. The first step in the process of creating a new product is to identify a market need. This involves conducting market research to understand what consumers want and what problems they are facing. Once a need is identified, the next step is to develop a concept that addresses this need. This is often done through brainstorming sessions with a team of designers and engineers. The concept is then refined through prototyping and testing, ensuring that it meets the requirements of the market. Finally, the product is launched and its performance is monitored to ensure it continues to meet the needs of the market.

1. *Introduction*

[illegible]

DATE: 1 FLOW #1 100-10101

10-15

ALL INFORMATION CONTAINED  
HEREIN IS UNCLASSIFIED

437

22

ਅਗਲੀ 9 ਜੁਲਾਈ, 1954 ਵਿਚ ਭਾ. ਕ. ਸਿੰਘ ਨੇ  
ਅਖਬਾਰ ਵਿਚ ਦਿੱਤੇ ਆਪਣੇ ਆਲੋਚਨਾਤਮਕ ਲੇਖ

[illegible]

19CH  
NO

[illegible][illegible]

**TOTAL**

**DATE**

**TIME**

**CHECK**

[illegible]

AUG 7 1960

01-05-55-2011

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000 1001 1002 1003 1004 1005 1006 1007 1008 1009 1010 1011 1012 1013 1014 1015 1016 1017 1018 1019 1020 1021 1022 1023 1024 1025 1026 1027 1028 1029 1030 1031 1032 1033 1034 1035 1036 1037 1038 1039 1040 1

[illegible]



[illegible][illegible]



[illegible]

235

[illegible]



STATION 7 INT-STATD PERFORMANCE PRESSURE 477.0 ISEN EFF. 857 POLY. EFF. 868 DELTA T ON T = .214  
 STATION 3 FLOW FIELD DESCRIPTION  
 STATION 1  
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 STATION 97  
 STATION 98  
 STATION 99  
 STATION 100



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STATION 1  INT.GATEJ PERFORMANC.  PRESSUR. RATIO = 2.042  L.D. = .FF. = .041  POLY. EFF. = .061  DELTA T ON T = .307
```

STATION	10	FLOW	FL-LD	DESCRIPTION
1	100	100	100	100
2	200	200	200	200
3	300	300	300	300
4	400	400	400	400
5	500	500	500	500
6	600	600	600	600
7	700	700	700	700
8	800	800	800	800
9	900	900	900	900
10	1000	1000	1000	1000

STATION 11 INT. RATIO = 2.09<sup>3</sup> LINEAL EFF. = .841 POLY. EFF. = .651 DELTA T 0.4 T = .367



TABLE 1. INTRINSIC VISCOSITIES,  $[\eta]$ , OF POLYMER SOLUTIONS IN CHLOROFORM AT 25°C.  $[\eta]$  VALUES WERE DETERMINED BY MEANS OF A CAPILLARY VISCOMETER OF THE UBBELOHDE TYPE.  $[\eta]$  VALUES WERE CORRECTED FOR SOLVENT VISCOSITY BY THE METHOD OF BIRD ET AL.<sup>11</sup>







[illegible][illegible]

UNIT	DATE	TIME	LOCATION	REMARKS
1	10/10/54	10:00	1000	1000
2	10/10/54	10:00	1000	1000
3	10/10/54	10:00	1000	1000
4	10/10/54	10:00	1000	1000
5	10/10/54	10:00	1000	1000
6	10/10/54	10:00	1000	1000
7	10/10/54	10:00	1000	1000
8	10/10/54	10:00	1000	1000
9	10/10/54	10:00	1000	1000
10	10/10/54	10:00	1000	1000
11	10/10/54	10:00	1000	1000
12	10/10/54	10:00	1000	1000
13	10/10/54	10:00	1000	1000
14	10/10/54	10:00	1000	1000
15	10/10/54	10:00	1000	1000
16	10/10/54	10:00	1000	1000
17	10/10/54	10:00	1000	1000
18	10/10/54	10:00	1000	1000
19	10/10/54	10:00	1000	1000
20	10/10/54	10:00	1000	1000
21	10/10/54	10:00	1000	1000
22	10/10/54	10:00	1000	1000
23	10/10/54	10:00	1000	1000
24	10/10/54	10:00	1000	1000
25	10/10/54	10:00	1000	1000
26	10/10/54	10:00	1000	1000
27	10/10/54	10:00	1000	1000
28	10/10/54	10:00	1000	1000
29	10/10/54	10:00	1000	1000
30	10/10/54	10:00	1000	1000
31	10/10/54	10:00	1000	1000
32	10/10/54	10:00	1000	1000
33	10/10/54	10:00	1000	1000
34	10/10/54	10:00	1000	1000
35	10/10/54	10:00	1000	1000
36	10/10/54	10:00	1000	1000
37	10/10/54	10:00	1000	1000
38	10/10/54	10:00	1000	1000
39	10/10/54	10:00	1000	1000
40	10/10/54	10:00	1000	1000
41	10/10/54	10:00	1000	1000
42	10/10/54	10:00	1000	1000
43	10/10/54	10:00	1000	1000
44	10/10/54	10:00	1000	1000
45	10/10/54	10:00	1000	1000
46	10/10/54	10:00	1000	1000
47	10/10/54	10:00	1000	1000
48	10/10/54	10:00	1000	1000
49	10/10/54	10:00	1000	1000
50	10/10/54	10:00	1000	1000
51	10/10/54	10:00	1000	1000
52	10/10/54	10:00	1000	1000
53	10/10/54	10:00	1000	1000
54	10/10/54	10:00	1000	1000
55	10/10/54	10:00	1000	1000
56	10/10/54	10:00	1000	1000
57	10/10/54	10:00	1000	1000
58	10/10/54	10:00	1000	1000
59	10/10/54	10:00	1000	1000
60	10/10/54	10:00	1000	1000
61	10/10/54	10:00	1000	1000
62	10/10/54	10:00	1000	1000
63	10/10/54	10:00	1000	1000
64	10/10/54	10:00	1000	1000
65	10/10/54	10:00	1000	1000
66	10/10/54	10:00	1000	1000
67	10/10/54	10:00	1000	1000
68	10/10/54			

STAT02 P\_2FO34V3.

[illegible][illegible]

TEST CONTROL FILE = 301111715090

$E_{\text{OW}} = 21.7\%$      $\rho = 1.336\text{ g/cc}$      $\text{PRESURE RATIO} = 2.32$      $\text{ISOTHERMIC EFFY} = .7011$      $\text{POLYTROPIC EFFY} = .7335$      $\text{DEL T/T} = .3868$

POINT NO.	TEST POINT TITLE	STATUS OF CALCULATION	FLOW RATE LBS/SEC	SPEED RPM	---ROTOR--- PRESSURE ISEN RATIO EFFY	---STAGE--- PRESSURE ISEN RATIO EFFY	FLOW/ (CHOKED FLOW)
1	30114171000	CONV. REQD AFTER 23 PASSES	21.7+0	19336.4	2.032	2.324	57037

	COV_RGEU	AFT-23	PASSES	
901141712010	21.7%	19336.4	2.032	.841 2.324 .701 .57037

3. TEST POINT 301230515695 (95%)

[illegible][illegible]

[illegible][illegible]

[illegible][illegible]

LOCALIZATION OF RELATIVE VELOCITY  
RELATIONSHIP BETWEEN PRESSURE RATIO AND ISENTROPIC EFFICIENCY

[illegible]

STATION 5 INT. GATE PERFORMANCE PRESSURE RATIO = 1.191 ISEN. EFF. = .340 POLY. EFF. = .652 DELTA T ON T = .060

STATION 3 FLOW FIELD DESCRIPTION

[illegible]



[illegible]



COAT  
COM  
SECTION  
REL-ANGLE  
FLW ANGLE  
INCIDENCE  
LOSS COEFF  
SPACED  
RELATIVE  
MACH NO  
RELATIVE VELOCITY  
PRESSURE  
TEMPERATURE  
PRESSURE DELTA T  
T  
ELECTRICITY  
POLYMER

STATION	FLOW	FIELD DESCRIPTION
1	100	100
2	200	200
3	300	300
4	400	400
5	500	500
6	600	600
7	700	700
8	800	800
9	900	900
10	1000	1000
11	1100	1100
12	1200	1200
13	1300	1300
14	1400	1400
15	1500	1500
16	1600	1600
17	1700	1700
18	1800	1800
19	1900	1900
20	2000	2000
21	2100	2100
22	2200	2200
23	2300	2300
24	2400	2400
25	2500	2500
26	2600	2600
27	2700	2700
28	2800	2800
29	2900	2900
30	3000	3000
31	3100	3100
32	3200	3200
33	3300	3300
34	3400	3400
35	3500	3500
36	3600	3600
37	3700	3700
38	3800	3800
39	3900	3900
40	4000	4000
41	4100	4100
42	4200	4200
43	4300	4300
44	4400	4400
45	4500	4500
46	4600	4600
47	4700	4700
48	4800	4800
49	4900	4900
50	5000	5000
51	5100	5100
52	5200	5200
53	5300	5300
54	5400	5400
55	5500	5500
56	5600	5600
57	5700	5700
58	5800	5800
59	5900	5900
60	6000	6000
61	6100	6100
62	6200	6200
63	6300	6300
64	6400	6400
65	6500	6500
66	6600	6600
67	6700	6700
68	6800	6800
69	6900	6900
70	7000	7000
71	7100	7100
72	7200	7200
73	7300	7300
74	7400	7400
75	7500	7500
76	7600	7600
77	7700	7700
78	7800	7800
79	7900	7900
80	8000	8000
81	8100	8100
82	8200	8200
83	8300	8300
84	8400	8400
85	8500	8500
86	8600	8600
87	8700	8700
88	8800	8800
89	8900	8900
90	9000	9000
91	9100	9100
92	9200	9200
93	9300	9300
94	9400	9400
95	9500	9500
96	9600	9600
97	9700	9700
98	9800	9800
99	9900	9900
100	10000	10000

[illegible][illegible]







STATION 1 - FLO. FILL - SCHEMATIC

TABLE I.  $\chi$  and  $\chi^2$  for the fit of the data to the model. The values of  $\chi$  and  $\chi^2$  are given for the fit of the data to the model. The values of  $\chi$  and  $\chi^2$  are given for the fit of the data to the model.

[illegible][illegible]

STATION 15 INT-GATED PERFORMANCE PRESSURE RATIO = 2.492 ISEN. EFF. = .682 POLY. EFF. = .720 DELTA T ON T = .435





TEST POINT TITL. = 301230515095

FLOW = 23.74 SPEED = 19378.7 PRESSURE RATIO = 2.492 ISENTROPIC EFFY = .825 POLYTROPIC EFFY = .7198 DEL T/T = .4347

POINT NO.	TEST POINT TITLE	STATUS OF CALCULATION	FLOW RATE, LBS/SEC	SPEED, RPM	---NOTOR--- PRESSURE RATIO	ISEN EFF	---STAGE--- PRESSURE RATIO	ISEN EFF	FLOW/CHORE FLOW)
1	301230515695	CONVERGED AFTER 25 PASSES	23.7-2	13378.7	2.986	.841	2.492	.682	.62207



















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STATION 11 INT-GRATED P-RFORMANC_ PRESSURE RATIO = 5.323 ISEN EFF = .433 POLY EFF = .463 D:LTATUN T = .486
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[illegible]









110. TEST POINT 301240915602 (102%)

[illegible][illegible]

[illegible][illegible]

[illegible]

[illegible]

STATION	FLOW FIELD	DESCRIPTION
1	1	1
2	2	2
3	3	3
4	4	4
5	5	5
6	6	6
7	7	7
8	8	8
9	9	9
10	10	10
11	11	11
12	12	12
13	13	13
14	14	14
15	15	15
16	16	16
17	17	17
18	18	18
19	19	19
20	20	20
21	21	21
22	22	22
23	23	23
24	24	24
25	25	25
26	26	26
27	27	27
28	28	28
29	29	29
30	30	30
31	31	31
32	32	32
33	33	33
34	34	34
35	35	35
36	36	36
37	37	37
38	38	38
39	39	39
40	40	40
41	41	41
42	42	42
43	43	43
44	44	44
45	45	45
46	46	46
47	47	47
48	48	48
49	49	49
50	50	50
51	51	51
52	52	52
53	53	53
54	54	54
55	55	55
56	56	56
57	57	57
58	58	58
59	59	59
60	60	60
61	61	61
62	62	62
63	63	63
64	64	64
65	65	65
66	66	66
67	67	67
68	68	68
69	69	69
70	70	70
71	71	71
72	72	72
73	73	73
74	74	74
75	75	75
76	76	76
77	77	77
78	78	78
79	79	79
80	80	80
81	81	81
82	82	82
83	83	83
84	84	84
85	85	85
86	86	86
87	87	87
88	88	88
89	89	89
90	90	90
91	91	91
92	92	92
93	93	93
94	94	94
95	95	95
96	96	96
97	97	97
98	98	98
99	99	99
100	100	100

[illegible]

[illegible]

STATION 6 INTEGRATED PERFORMANCE PRESSURE RATIO = 1.620 ISEN. EFF. = .866 POLY. EFF. = .875 DELTA T ON T = .178

STATION	7	FLOW FIELD DESCRIPTION
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97		
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99		
100		

[illegible]

[illegible][illegible]

STATION	FROM FIELD	DESCRIPTION
1	100	100
2	200	200
3	300	300
4	400	400
5	500	500
6	600	600
7	700	700
8	800	800
9	900	900
10	1000	1000
11	1100	1100
12	1200	1200
13	1300	1300
14	1400	1400
15	1500	1500
16	1600	1600
17	1700	1700
18	1800	1800
19	1900	1900
20	2000	2000
21	2100	2100
22	2200	2200
23	2300	2300
24	2400	2400
25	2500	2500
26	2600	2600
27	2700	2700
28	2800	2800
29	2900	2900
30	3000	3000
31	3100	3100
32	3200	3200
33	3300	3300
34	3400	3400
35	3500	3500
36	3600	3600
37	3700	3700
38	3800	3800
39	3900	3900
40	4000	4000
41	4100	4100
42	4200	4200
43	4300	4300
44	4400	4400
45	4500	4500
46	4600	4600
47	4700	4700
48	4800	4800
49	4900	4900
50	5000	5000
51	5100	5100
52	5200	5200
53	5300	5300
54	5400	5400
55	5500	5500
56	5600	5600
57	5700	5700
58	5800	5800
59	5900	5900
60	6000	6000
61	6100	6100
62	6200	6200
63	6300	6300
64	6400	6400
65	6500	6500
66	6600	6600
67	6700	6700
68	6800	6800
69	6900	6900
70	7000	7000
71	7100	7100
72	7200	7200
73	7300	7300
74	7400	7400
75	7500	7500
76	7600	7600
77	7700	7700
78	7800	7800
79	7900	7900
80	8000	8000
81	8100	8100
82	8200	8200
83	8300	8300
84	8400	8400
85	8500	8500
86	8600	8600
87	8700	8700
88	8800	8800
89	8900	8900
90	9000	9000
91	9100	9100
92	9200	9200
93	9300	9300
94	9400	9400
95	9500	9500
96	9600	9600
97	9700	9700
98	9800	9800
99	9900	9900
100	10000	10000

[illegible]

NOT-  
LOCAL 13047

[illegible]

STATION 5 INTEGRATED PERFORMANCE PRESSURE RATIO = 2.543 ISN, EFF. = .342 PO.Y. EFF. = .061 DELTA T ON T = .362

STATION	3	FLOW FIELD DESCRIPTION
---------	---	------------------------

[illegible]

[illegible]

283

[illegible]



STATION 11 INTEGRATED PERFORMANCE PRESSURE RATIO = 3.462 ISEN. EFF. = .039 POLY. EFF. = .064 DELTA T ON T = .505

[illegible]

285

[illegible]

STATION 12 INT. GATED PERFORMANCE PRESSURE RATIO = 3.233 LIGN. EFF. = .743 P.O.V. EFF. = .929 O.F.F.I.A. T.O.V. I = .905





[illegible]

**BLADE DATA**

LOCAL BLADE ANGLE  
REL FLOW DEVIATION  
LOSS BLADE CHORD  
BLADE CHORD  
RELATIVE VELOCITY  
RELATIVE PRESSURE  
RELATIVE TEMPERATURE  
PRESSURE DELTA T  
TEMPERATURE DIFFERENCE

[illegible]

STATION 15 INTEGRATED PERFORMANCE PRESSURE RATIO = 2.773 ISEN, EFF. = .666 POLY. EFF. = .709 DELTA T ON T = .585

[illegible][illegible]

[illegible][illegible]

### WAKE AND BOUNDARY LAYER BLOCKAGES (PERCENT)

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
STAKE	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
STAKE FLGTR	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
INT BLOCKAGE	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
SUMMARY	POINT NO. 1 THE CALCULATION IS CONVERGED PASS 26																

TEST POINT TITLE = 301240915602  
FLOW = 26.21 SPEED = 20788.1 PRESSURE RATIO = 2.773 ISENTROPIC EFFY = .6663 POLYTROPIC EFFY = .7095 DEL T/T = .5850

## SUMMARY

POINT NO.	TEST POINT TITLE	STATUS OF CALCULATION	FLOW RATE LBS/SEC	SPEED RPM	---ROTOR PRESSURE RATIO	---ISEN EFFY	---STAGE PRESSURE RATIO	---ISEN EFFY	---FLOW/CHOK (FLOW)
1	3012+9915602	CONVERGED AFTER 26 PASSES	25.208	20781.1	3.462	.639	2.773	.666	.66667

**APPENDIX B**  
**COMPUTER INPUT DATA FOR DATA REDUCTION**

KEY

- SECTION 1. Common Phase I Data
- SECTION 2. Common Phase II Fixed Data  
(Log 1) Across Blade
- SECTION 3. Common Phase II Input and Test Point Data  
(Log 3, Log 4) Across Blade
- SECTION 4. Common Phase II Fixed Data  
(Log 1) Within Blade
- SECTION 5. Common Phase II Input and Test Point Data  
(Log 3, Log 4) Within Blade
- SECTION 6. Individual Test Input Data
  - a. Exceptions to Section 1 Data  
(indicated by (1) )
  - b. Exceptions to Section 2 Data  
(indicated by (2) )
  - c. Exceptions to Section 3 Data  
(indicated by (3) )
  - d. Exceptions to Section 4, Data  
(indicated by (4) )
  - e. Exceptions to Section 5 Data  
(indicated by (5) )



# SECTION 1. COMMON PHASE I DATA

## BASIC DATA DECK

```

39 1
460.0000 470.0000 480.0000 490.0000 492.0000 494.0000 496.0000 498.0000
500.0000 502.0000 504.0000 506.0000 508.0000 510.0000 512.0000 514.0000
516.0000 518.0000 520.0000 522.0000 524.0000 526.0000 528.0000 530.0000
532.0000 534.0000 536.0000 538.0000 540.0000 542.0000 544.0000 546.0000
548.0000 550.0000 552.0000 554.0000 556.0000 558.0000 560.0000
.0105 .0309 .0505 .0600 .0805 .0961 .1041 .1126
.1217 .1315 .1420 .1532 .1652 .1780 .1916 .2063
.2219 .2306 .2561 .2749 .2949 .3162 .3386 .3623
.3883 .4153 .4446 .4744 .5067 .5409 .5772 .6153
.6555 .6980 .7425 .7902 .8403 .8930 .9467
-2.0000 -.2500 2.2500 6.1010
12.6070 29.5155
.7217 .0997 .3701 .0109 1.0000 1.0000
10 1
470.0000 480.0000 490.0000 500.0000 510.0000 520.0000 530.0000 540.0000
550.0000 560.0000
9050.0000 9650.0000 3609.0000 2445.1000 1704.9000 1200.1000 060.9000 633.7000
460.0000 350.0000
3
494.0000 546.0000 561.0000
.9990 1.0000 1.0010
4 1
.2000 .4000 .6000 .8000 1.2000 1.4000 1.6000 1.8000
.9990 .9970 .9960 .9944 .9919 .9907 .9900 .9895
14.6960
8 1
1.0000 1.2000 1.4000 1.6000 1.8000 2.0000 2.2000 2.4000
0.0000 -.1700 -.2600 -.3400 -.3000 -.4050 -.4200 -.4350
16 1
423.5000 447.5000 462.5000 477.5000 492.5000 507.5000 522.5000 537.5000
552.5000 565.0000 579.3000 593.0000 600.5000 623.3000 639.3000 656.0000
410.0000 420.0000 430.0000 440.0000 450.0000 460.0000 470.0000 480.0000
490.0000 500.0000 510.0000 520.0000 530.0000 540.0000 550.0000 560.0000

6
.25037964E+00 -.00012020E-04 .23122066E-06 -.34160919E-09
.27497120E-12 -.05540936E-16

6
.43403206E+00 .10900440E-03 -.52292623E-06 .10102121E-08
-.79236916E-12 .22724403E-15

4
1 24
301 103 105 107 109 111 113 115 117 119 121 123 125 127 129 131 133 135 137 139
341 143 145 147
2 24
201 203 205 207 209 211 213 215 217 219 221 223 225 227 229 231 233 235 237 239
241 243 245 247
3 24
301 303 305 307 309 311 313 315 317 319 321 323 325 327 329 331 333 335 337 339
341 343 345 347
4 24
401 403 405 407 409 411 413 415 417 419 421 423 425 427 429 431 433 435 437 439
441 443 445 447
1
1 40
50 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78
79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20
21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40
40 1
-.0007 -.0005 -.0003 -.0000 .0002 .0004 .0006 .0008
.0011 .0013 .0015 .0016 .0020 .0022 .0024 .0027
.0029 .0031 .0034 .0036 .0038 .0041 .0043 .0045
.0046 .0050 .0052 .0054 .0057 .0059 .0061 .0063
.0065 .0066 .0070 .0072 .0074 .0076 .0079 .0081
460.0000 470.0000 480.0000 490.0000 500.0000 510.0000 520.0000 530.0000
540.0000 550.0000 560.0000 570.0000 580.0000 590.0000 600.0000 610.0000
620.0000 630.0000 640.0000 650.0000 660.0000 670.0000 680.0000 690.0000
700.0000 710.0000 720.0000 730.0000 740.0000 750.0000 760.0000 770.0000
780.0000 790.0000 800.0000 810.0000 820.0000 830.0000 840.0000 850.0000

```

# INSTRUMENTATION DATA DECK

```

1 5 0 5 5 139
20371.400 7.6272 7.6400 8.6000
1.4666 2.9228 4.4122 5.8684 7.3412
7.8718 8.8810 8.1210 8.2518 8.3718
7.8888 7.5688 8.1280 9.2888 8.4488
14.6960 318.6888 53.3420 85.7750 778.1288
1 2
107 207
2 4
2 3 4 5
3 18
327 323 319 315 311 329 325 321 317 313
4 10
14 12 18 8 6 15 13 11 9 7
5 25
335 405 415 425 435 331 401 411 421 431 337 407 417 427 437 333 403 413 423 433
339 409 419 429 439
6 25
36 31 26 21 16 39 34 29 24 19 37 32 27 22 17 40 35 38 25 20
38 33 28 23 18
7 8
233 235 237 239 225 227 229 231
8 4
105 103 205 203
9 4
213 215 217 219
10 9
0.0000 .2500 .5000 .7500 1.0000 1.2500 1.5000 1.7500
2.0000
113 115 117 119 121 123 125 127 129
11 7
131 133 135 137 139 209 211
12 3
305 307 309
13 3
1
143 145 147
1
243 245 247

1
343 345 347
1
443 445 447
14 2
223 221
15 2
109 111
16 2
101 201
99 58
1

```

## OTHER DATA

(1) 0 1 1  
14.2200 15.0000 38.8880  
.5000 .5000 .5000

## EDITING DATA DECK

0

## SECTION 2. COMMON PHASE II FIXED DATA (LOG 1) ACROSS BLADE

### FIXED DATA PRINTOUT

#### OVERALL RUN TITLE

NUMBER OF STATIONS	=	10
NUMBER OF ST. LINES	=	21
MAXIMUM NUMBER OF ITERATIONS	=	40
MAXIMUM NUMBER OF ARBITRARY ITERATIONS	=	15
TOTAL PRESSURE SOURCE INDICATOR	=	1
TOTAL TEMPERATURE SOURCE INDICATOR	=	0
STATION NUMBER FOR ROTOR EXIT DATA	=	7
STATION NUMBER FOR STAGE EXIT DATA	=	5
NUMBER OF ROTOR BLADES	=	30
NUMBER OF STATOR BLADES	=	49
MAXIMUM NUMBER OF LINES PER PAGE	=	60
NPLOT	=	3

#### ANNULUS SPECIFICATION

##### STATION 1 SPECIFIED BY 2 POINTS

RSTN	XSTN
6.0036	-1.0000
9.9900	-1.3000

##### STATION 2 SPECIFIED BY 2 POINTS

RSTN	XSTN
6.3700	-1.3000
9.9900	-1.0000

##### STATION 3 SPECIFIED BY 2 POINTS

RSTN	XSTN
6.6010	-0.4000
9.9900	-0.4000

##### STATION 4 SPECIFIED BY 2 POINTS

RSTN	XSTN
6.7000	0.0000
9.9900	0.0000

##### STATION 5 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.2439	-2.0000
8.3049	-2.0000

##### STATION 6 SPECIFIED BY 6 POINTS

RSTN	XSTN
7.2740	2.2000
7.3000	2.3350
8.3030	2.3350
8.2000	2.4030
8.4000	2.3350
8.3333	2.2000

##### STATION 7 SPECIFIED BY 8 POINTS

RSTN	XSTN
7.3193	2.5000
7.7720	2.5593
7.4730	2.8402
8.0049	2.9232
8.1427	2.8431
8.2373	2.3990
8.2401	2.7620
8.5193	2.5000

STATION 8 SPECIFIED BY 2 FCINTS

RSTN	XSTN
7.3400	4.7250
8.3000	4.7250

STATION 9 SPECIFIED BY 2 FCINTS

RSTN	XSTN
7.3400	5.4000
8.3000	5.4000

STATION 10 SPECIFIED BY 2 FCINTS

RSTN	XSTN
7.3400	7.0000
8.3000	7.0000

STATION CALCULATION SPECIFICATION AND BLADING DATA

STATION 2 NCALC = 0 NDATA = -0 NPL = -0

STATION 3 NCALC = 0 NDATA = -0 NCL = -0

(2) STATION 4 NCALC = 1 NDATA = 15 NEL = 0

RADIUS	BETA	EPSILON	BLCKAGE	THETA
5.7280	-02.0011	6.0825	.01450	.2192
6.9386	-02.2938	6.2938	.01420	.2168
7.0504	-02.5801	6.5195	.01410	.2144
7.2131	-02.8379	6.2846	.01390	.2120
7.3560	-03.0939	5.7618	.01370	.2097
7.5210	-03.3790	4.6336	.01350	.2078
7.6770	-03.7062	4.6317	.01330	.2062
7.8340	-04.0815	3.6453	.01320	.2052
7.9927	-04.5112	2.2586	.01320	.2048
8.1529	-05.0037	-1.7858	.01330	.2051
8.3143	-05.5623	-4.0672	.01340	.2061
8.4791	-06.1881	-5.0474	.01360	.2078
8.6482	-06.8700	-7.1213	.01380	.2101
8.8166	-07.5768	-8.1121	.01420	.2127
8.9300	-08.2847	-9.5200	.01450	.2157

(2) STATION 5 NCALC = 4 NDATA = 15 NBL = 0

RADIUS	BETA	EPSILON	BLCKAGE	THETA
7.5585	-11.0761	10.5221	.04437	-.1061
7.6197	-12.5921	10.3557	.04309	-.1076
7.6839	-14.1312	9.3776	.04185	-.1091
7.7508	-15.6950	8.1114	.04100	-.1104
7.8204	-17.1350	7.1593	.04024	-.1116
7.8926	-18.3596	6.6712	.03956	-.1127
7.9573	-19.3791	6.2211	.03882	-.1138
8.0442	-20.2566	7.6047	.03806	-.1151
8.1233	-21.0488	8.6547	.03752	-.1165
8.2047	-21.7990	10.6021	.03690	-.1182
8.2982	-22.4822	12.2000	.03633	-.1202
8.3739	-23.0488	13.4357	.03584	-.1226
8.4623	-23.4032	14.6543	.03545	-.1252
8.5549	-23.4990	13.7640	.03496	-.1279
8.6550	-23.4258	13.2395	.03437	-.1307

(2) STATION 6 NCALC = 0 NDATA = 0 NEL = 0

(2) STATION 7 NCALC = 1 NDATA = 10 NBL = 0

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5440	55.1561	-41.7532	.01614	-.1043
7.6595	53.5860	-37.7735	.01723	-.0952
7.7778	49.8380	-30.1445	.01536	-.0847
7.8365	47.1487	-24.8681	.01445	-.0773
8.0211	45.3735	-11.8297	.01392	-.0727
8.1454	44.4932	-.6196	.01358	-.0710
8.2714	44.6432	9.6085	.01338	-.0722
8.3997	45.8152	26.7782	.01333	-.0770
8.5310	49.5428	41.5535	.01370	-.0882
8.6721	54.4829	48.7546	.01130	-.1047

STATION 8 NCALC = 3 NDATA = 10 NBL = 0

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5000	-6.7608	.0181	.00694	.0001
7.6250	-7.1856	.0202	.00579	.0001
7.7500	-7.6868	.0180	.00964	.0001
7.8750	-8.1755	.0121	.00950	.0001
8.0000	-8.5885	.0076	.00936	0.0000
8.1250	-8.9062	.0030	.00923	0.0000
8.2500	-9.0563	-.0025	.00910	0.0000
8.3750	-9.0583	-.0113	.00896	0.0000
8.5000	-9.1339	-.0255	.00884	.0001
8.6250	-9.2331	-.0416	.00873	.0001

(2) STATION 9 NCALC = 0 NDATA = 0 NBL = 1

STATION 10 NCALC = 0 NDATA = 0 NBL = 1

ACTOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 2 POINTS

1-COORD LOSS COEFF/TOTAL LOSS COEFF

0.0000 0.0000  
1.0000 1.0000

OUTLET RADIUS = 0.0000

M-COORD DEVIATION ANGLE (DEGREES)

0.0000 0.0000  
1.0000 1.0000

STATION GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 2 POINTS

M-COORD LOSS COEFF/TOTAL LOSS COEFF

0.0000 0.0000  
1.0000 1.0000

OUTLET RADIUS = 0.0000

1-COORD DEVIATION ANGLE (DEGREES)

0.0000 0.0000  
1.0000 1.0000

NUMBER OF TEST POINTS TO BE ANALYSED = 4

(3) PSCL= 4.00 PLOW= 12.00 CAMF= 4.000 NSAVE= 1 NNPA= 0 PFCRC= 0 NEX= 2

# SECTION 3. COMMON PHASE II INPUT AND TEST POINT DATA (LOG 3, LOG 4) WITHIN BLADE

## TEST DATA PRINTOUT FOR POINT NO. 1

### TEST POINT TITLE

GAS CONSTANT	53.4631
AIR MASS FRACTION	0.2167
FLOWRATE	20.4101
ROTOR SPEED	14.6830
INLET TOTAL PRESSURE	51.6000
INLET TOTAL TEMPERATURE	753.233
T IN/1 IN(1ST)	753.233
P IN/1 IN(1ST)	51.6000

### ROTOR OUTLET TOTAL PRESSURE ( 5 POINTS)

RADIUS	PRESSURE
--------	----------

7.8710	50.6306
8.0010	50.9374
8.1210	48.7050
8.2510	47.1334
8.3710	45.1251

### ROTOR OUTLET TOTAL TEMPERATURE ( 5 POINTS)

RADIUS	TEMPERATURE
--------	-------------

7.8710	749.170
8.0010	750.274
8.1210	725.174
8.2510	705.757
8.3710	793.234

### STAGE OUTLET TOTAL PRESSURES ( 5 POINTS)

RADIUS	MEAN PRES	PEAK PRES
--------	-----------	-----------

7.8900	41.2973	45.6670
7.9500	39.2335	42.8378
8.1200	36.2137	42.1651
8.2400	36.1250	42.1721
8.4400	39.7045	44.1210

### STAGE OUTLET TOTAL TEMPERATURES ( 5 POINTS)

RADIUS	TEMPERATURE
--------	-------------

7.8900	753.615
7.9500	761.333
8.1200	763.585
8.2400	773.233
8.4400	774.937

### STAGE OUTLET FLOW ANGLES ( 1 POINTS)

RADIUS	ANGLE
--------	-------

0.0000	0.000
--------	-------

### CASING STATIC PRESSURES (14 POINTS)

X-COORD	PRESSURE
---------	----------

-2.0000	13.4804
-1.2500	13.4510
0.0000	13.7632
0.2500	14.4438
0.5000	15.7940
0.7500	16.0131
1.0000	20.3045
1.2500	23.8027
1.5000	24.5302
1.7500	25.2124
2.0000	26.1941
2.2500	26.7330
4.7250	27.0493
6.1510	27.1953

# HUB STATIC PRESSURES ( 5 POINTS)

X-CORD	PRESSURE
-2.0000	13.6635
-0.2500	13.0121
2.2500	24.2955
4.7250	27.4607
6.1310	27.4607

## DISTRIBUTED BLOCKAGE SPECIFICATION

(3) STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ACC.F=VA.	DISTRIBUTION FACTOR	FRACTION TO BLOCKAGE
1	0.00000	1.0000	-0.000	-0.0000	-0.0000
2	0.00000	1.0000	-0.000	-0.0000	-0.0000
3	0.00000	1.0000	-0.000	-0.0000	-0.0000
4	0.00000	1.0000	-0.000	-0.0000	-0.0000
5	.05000	0.0000	-0.000	-0.0000	-0.0000
6	.05000	0.0000	-0.000	-0.0000	-0.0000
7	.10000	1.0000	-0.000	-0.0000	-0.0000
8	.26000	1.0000	-0.000	-0.0000	-0.0000
9	.05400	1.0000	-0.000	-0.0000	-0.0000
10	.05400	1.0000	-0.000	-0.0000	-0.0000

## SOLUTION TYPE INDICATORS

(3) STATION	1	2	3	4	5	6	7	8	9	10
NRACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0
NJUMP	0									

# SECTION 4. COMMON PHASE II FIXED DATA (LOG 1) WITHIN BLADE

## ----- FIXED DATA PRINTOUT -----

### OVERALL RUN TITLE

NUMBER OF STATIONS  
NUMBER OF STREAMLINES  
MAXIMUM NUMBER OF ITERATIONS  
MAXIMUM NUMBER OF ARBITRARY ITERATIONS  
TOTAL PRESSURE SOURCE INDICATOR  
TOTAL TEMPERATURE SOURCE INDICATOR  
STATION NUMBER FOR ROTOR EXIT DATA  
STATION NUMBER FOR STAGE EXIT DATA  
NUMBER OF ROTOR BLADES  
NUMBER OF STATOR BLADES  
MAXIMUM NUMBER OF LINES PER PAGE  
NPLOT

\* 17  
\* 21  
\* 66  
\* 20  
\* 0  
\* 0  
\* 11  
\* 16  
\* 30  
\* 49  
\* 80  
\* 2

### ANNULUS SPECIFICATION

#### STATION 1 SPECIFIED BY 2 POINTS

RSTN	XSTN
6.0095	-1.0000
9.1900	-1.3033

#### STATION 2 SPECIFIED BY 2 POINTS

RSTN	XSTN
9.3746	-1.0000
9.0900	-1.3033

#### STATION 3 SPECIFIED BY 2 POINTS

RSTN	XSTN
9.3010	-0.4000
9.0500	-0.4000

#### STATION 4 SPECIFIED BY 2 POINTS

RSTN	XSTN
6.7500	0.0030
9.0000	0.0030

#### STATION 5 SPECIFIED BY 2 POINTS

RSTN	XSTN
6.3373	0.4330
8.9340	0.4000

#### STATION 6 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.0784	0.8000
8.1573	0.8000

#### STATION 7 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.2620	1.2000
8.3019	1.2000

#### STATION 8 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.4492	1.6030
8.7353	1.6000



STATION 3 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.5439	2.0000
8.6639	2.0000

STATION 10 SPECIFIED BY 6 POINTS

RSTN	XSTN
7.5748	2.2000
7.8000	2.3350
8.0000	2.3950
8.2000	2.4030
8.4000	2.3500
8.6339	2.2000

STATION 11 SPECIFIED BY 8 POINTS

RSTN	XSTN
7.5139	2.5000
7.7472	2.6938
7.8730	2.8482
8.0049	2.7262
8.1427	2.7491
8.2873	2.8996
8.4401	2.7656
8.6139	2.5000

STATION 12 SPECIFIED BY 8 POINTS

RSTN	XSTN
7.7150	3.0659
7.8336	3.2061
7.9410	3.3114
8.0550	3.3759
8.1746	3.3931
8.2934	3.3560
8.4257	3.2554
8.5730	3.0678

STATION 13 SPECIFIED BY 8 POINTS

RSTN	XSTN
7.7230	3.6189
7.8456	3.7124
7.9538	3.7826
8.0686	3.8256
8.1885	3.8370
8.3126	3.8123
8.4337	3.7453
8.5735	3.6202

STATION 14 SPECIFIED BY 3 POINTS

RSTN	XSTN
7.6720	4.1720
8.1900	4.2810
8.5900	4.1726

STATION 15 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.5490	4.7250
8.6090	4.7250

STATION 16 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.5400	5.4000
8.5300	5.4000

STATION 17 SPECIFIED BY 2 POINTS

RSTN	XSTN
7.6400	7.0900
8.6000	7.0000

STATION CALCULATION SPECIFICATION AND BLADING DATA

STATION 2	NCALC = 0	NDA = -0	NBL = -0
STATION 3	NCALC = 0	NDA = -0	NBL = -0
STATION 4	NCALC = 1	NDA = 15	NBL = 0

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
6.7586	-62.8811	6.0825	.01450	.2192
6.9086	-62.2938	6.2938	.01420	.2168
7.0604	-62.5801	6.4195	.01410	.2144
7.2131	-62.8379	6.2846	.01390	.2120
7.3668	-63.0939	5.7818	.01370	.2097
7.5216	-63.3790	4.8992	.01350	.2078
7.6775	-63.7062	3.6317	.01330	.2062
7.8345	-64.0816	2.0493	.01320	.2052
7.9927	-64.5112	.2588	.01320	.2048
8.1529	-65.0037	-1.7858	.01330	.2051
8.3148	-65.5623	-4.0672	.01340	.2061
8.4791	-66.1881	-6.0474	.01360	.2078
8.6462	-66.8700	-7.1213	.01380	.2101
8.8166	-67.5768	-8.1121	.01420	.2127
8.9900	-68.2887	-9.5200	.01450	.2157

(4) STATION 5 NCALC = 2 NDA = 15 NBL = 3

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
6.9066	-60.4843	4.2528	.11660	.1895
7.0443	-60.8164	4.1868	.11320	.1881
7.1829	-61.1343	3.7778	.10980	.1867
7.3217	-61.4067	3.1230	.10630	.1856
7.4607	-61.6313	2.6462	.10280	.1846
7.5999	-61.8603	2.2043	.09960	.1838
7.7397	-62.1272	1.6392	.09670	.1832
7.8799	-62.4467	1.0024	.09450	.1828
8.0211	-62.8331	.3683	.09280	.1826
8.1640	-63.3022	-.3192	.09160	.1826
8.3088	-63.9650	-1.0951	.09100	.1828
8.4564	-64.5226	-1.7009	.09140	.1832
8.6074	-65.2580	-1.8276	.09230	.1838
8.7629	-66.0375	-2.1796	.09340	.1844
8.9231	-66.8334	-3.0445	.09450	.1852

(4) STATION 6 NCALC = 2 NDA = 15 NBL = 3

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.0871	-54.7236	2.4431	.15180	.0157
7.2111	-52.0830	2.1140	.14700	.0150
7.3352	-55.4640	1.2241	.14230	.0145
7.4588	-55.8124	.1247	.13780	.0143
7.5820	-56.0634	-.2912	.13350	.0143
7.7051	-56.3007	-.3032	.12940	.0144
7.8282	-56.5794	-.2037	.12580	.0145
7.9512	-56.9187	.0605	.12290	.0145
8.0748	-57.3364	.5445	.12060	.0145
8.1994	-57.8545	1.1927	.11880	.0142
8.3253	-58.4881	1.9451	.11770	.0138
8.4530	-59.2396	2.8362	.11760	.0132
8.5835	-60.1111	3.9074	.11820	.0123
8.7176	-60.9981	4.6308	.11890	.0111
8.8562	-61.9604	4.9033	.11960	.0098

(4) STATION 7 NCALC = 2 NDATA = 15 NBL = 3

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.2700	-42.4530	1.4890	.20936	-.0504
7.3758	-43.2304	1.0422	.19685	-.0507
7.4400	-43.3701	1.0200	.18715	-.0509
7.5346	-44.4573	-1.1013	.17888	-.0507
7.6385	-44.9031	-1.2430	.17166	-.0504
7.7425	-45.3233	-1.7671	.16513	-.0502
7.8472	-45.7857	-1.0043	.15950	-.0501
8.0023	-46.3129	1.0785	.15419	-.0502
8.1083	-46.9235	2.3041	.15016	-.0506
8.2157	-47.6576	4.1911	.14656	-.0514
8.3246	-48.4394	6.0132	.14416	-.0526
8.4355	-49.4333	7.7420	.14275	-.0542
8.5492	-50.4285	9.3300	.14233	-.0562
8.6667	-51.3333	10.3001	.14225	-.0586
8.7834	-52.3237	10.8437	.14220	-.0612

(4) STATION 8 NCALC = 2 NDATA = 15 NBL = 3

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.4300	-24.3339	2.8700	.16500	-.0586
7.5291	-25.5733	2.8220	.15501	-.0631
7.6333	-26.8033	2.1498	.14656	-.0696
7.7307	-28.0303	1.2496	.13967	-.0899
7.7733	-29.1233	1.1645	.13377	-.0901
7.8587	-30.7233	1.6595	.12653	-.09304
7.9455	-32.3540	2.5576	.12361	-.09307
8.0340	-34.3333	3.3882	.11927	-.09314
8.1243	-36.4730	5.6393	.11547	-.09323
8.2157	-38.3235	7.6543	.11220	-.09335
8.3110	-40.2257	9.7467	.10980	-.09354
8.4175	-42.1513	11.5906	.10801	-.09375
8.5071	-44.3558	12.8628	.10684	-.1001
8.6110	-46.7200	13.3143	.10601	-.1029
8.7225	-49.3403	13.2525	.10507	-.1050

(4) STATION 9 NCALC = 4 NDATA = 15 NBL = 3

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5585	-11.0751	10.9221	.04437	-.1051
7.6137	-12.5921	10.3557	.04309	-.1076
7.6339	-14.1312	9.3773	.04165	-.1091
7.7203	-15.5953	3.1113	.04100	-.1104
7.8204	-17.1350	7.1593	.04024	-.1116
7.8426	-18.3596	6.6712	.03996	-.1127
7.9573	-19.3731	6.3211	.03882	-.1138
8.0442	-20.2535	7.5847	.03800	-.1151
8.1233	-21.0443	8.9547	.03752	-.1165
8.2047	-21.7930	10.6021	.03690	-.1182
8.2382	-22.4822	12.2000	.03635	-.1202
8.3739	-23.7450	13.4357	.03584	-.1226
8.4523	-24.4032	13.3543	.03545	-.1252
8.5344	-25.4330	13.7549	.03495	-.1279
8.6550	-26.4253	13.2395	.03437	-.1307

STATION 10 NCALC = 0 NDATA = -0 NBL = 1

STATION 11 NCALC = 1 NDATA = 10 NBL = -0

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5440	33.1531	-43.7533	.01614	-.1083
7.6595	33.5850	-37.7735	.01723	-.0952
7.7775	43.3380	-30.1445	.01336	-.0847
7.8355	47.1407	-21.2031	.01445	-.0773
8.0211	45.3735	-11.4237	.01392	-.0727
8.1454	44.4392	-3.3193	.01358	-.0710
8.2714	44.3432	3.8093	.01338	-.0722
8.3397	45.3152	26.7782	.01333	-.0770
8.5330	49.5323	41.5535	.01370	-.0832
8.6721	54.4529	48.7540	.01130	-.1047

STATION 12 NCALC = 2 NDATA = 10 N3L = 0

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5113	34.7293	-25.7556	.11858	-.0549
7.6334	33.9362	-26.3943	.18511	-.0470
7.7560	32.8982	-23.2637	.09202	-.0394
7.8795	31.3971	-16.2152	.08062	-.0337
8.0036	30.4237	-9.4954	.07350	-.0301
8.1283	29.8951	-2.9737	.06992	-.0284
8.2534	29.8235	3.3793	.06961	-.0285
8.3789	30.3733	12.2206	.07270	-.0305
8.5053	32.4775	23.1254	.08078	-.0353
8.6330	33.6328	32.3432	.09245	-.0432

STATION 13 NCALC = 2 NDATA = 10 N3L = 0

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5009	16.6561	-9.9376	.12611	-.0156
7.6256	16.3973	-10.2334	.11167	-.0127
7.7504	15.0640	-9.0207	.09770	-.0098
7.8752	13.9233	-6.7565	.08599	-.0076
8.0001	15.7355	-3.7730	.07831	-.0061
8.1251	15.3033	-1.1768	.07436	-.0055
8.2501	15.9516	2.493	.07368	-.0054
8.3751	16.0597	2.9553	.07641	-.0059
8.5002	16.7301	6.0343	.08323	-.0070
8.6254	17.3003	10.0593	.09466	-.0091

STATION 14 NCALC = 2 NDATA = 10 N3L = 0

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5000	4.4731	-1.0973	.08357	.0024
7.6250	4.1107	-1.1011	.07496	.0027
7.7500	3.3830	-.3188	.06672	.0030
7.8750	3.8057	-.6227	.06023	.0032
8.0000	2.9953	-.4587	.05577	.0034
8.1250	2.9012	-.3036	.05325	.0035
8.2501	2.7537	-.1369	.05270	.0035
8.3751	2.4770	-.3981	.05419	.0036
8.5001	3.1370	-.3345	.05797	.0037
8.6251	3.6112	-1.0923	.06461	.0040

STATION 15 NCALC = 3 NDATA = 10 N3L = 1

RADIUS	BETA	EPSILON	BLOCKAGE	THETA
7.5000	-6.7608	.0181	.00994	.0001
7.6250	-7.1856	.0202	.00979	.0001
7.7500	-7.6858	.0180	.00964	.0001
7.8750	-8.1753	.0121	.00950	.0001
8.0000	-8.6005	.0076	.00936	.0000
8.1250	-8.9062	.0030	.00923	.0000
8.2500	-9.0553	-.0026	.00910	.0000
8.3750	-9.0533	-.0113	.00896	.0000
8.5000	-9.1338	-.0255	.00884	.0001
8.6250	-9.2331	-.0418	.00873	.0001

STATION 16 NCALC = -0 NDATA = -0 N3L = 1

STATION 17 NCALC = -0 NDATA = -0 N3L = 1

ROTOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 3 POINTS

4-COORD LOSS COEFF/TOTAL LOSS COEFF

0.0000 0.0000  
1.0000 1.0010

(4) OUTLET RADIUS = 7.5499

4-COORD DEVIATION ANGLE (DEGREES)

.2000 -5.1750  
.4000 -5.4200  
.6000 -4.7700

(4) OUTLET RADIUS = 7.7343

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.0750
.4000	-4.5420
.8000	-4.7060

(4) OUTLET RADIUS = 7.9385

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1000
.4000	-4.2030
.8000	-4.6500

(4) OUTLET RADIUS = 8.1919

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3750
.4000	-5.7420
.8000	-5.5890

(4) OUTLET RADIUS = 8.6599

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3250
.4000	-12.3300
.8000	-25.0850

STATOR GENERALISED PERFORMANCE LOSS 2 POINTS DEVIATION 6 POINTS

M-COORD LOSS COEFF/TOTAL LOSS COEFF

0.0000	0.0000
1.0000	1.0000

OUTLET RADIUS = 0.0000

M-COORD DEVIATION ANGLE (DEGREES)

0.0000	.1000
.2000	.1100
.4000	.1500
.6000	.2200
.8000	.3800
1.0000	1.0000

NUMBER OF TEST POINTS TO BE ANALYSED = 1

(5) PSCALE= 1.00 PLOWER= 14.00 DAMPF= 5.000 NSAVE= 1 NNMAX= -0 MFORCE= -0 NEX= 2

# SECTION 5. COMMON PHASE II INPUT AND TEST POINT DATA (LOG 3, LOG 4) WITHIN BLADE

TEST DATA PRINTOUT FOR POINT NO. 1

## TEST POINT TITLE

GAS CONSTANT	= 53.5218
AIR MASS FRACTION	= .09446
FLOWRATE	= 13.8351
ROTOR SPEED	= 10195.8
INLET TOTAL PRESSURE	= 14.6960
INLET TOTAL TEMPERATURE	= 518.688
T IN/T IN(STO)	= .96970
P IN/P IN(STO)	= .98610

## ROTOR OUTLET TOTAL PRESSURE ( 5 POINTS)

RADIUS	PRESSURE
7.8710	20.5335
8.0010	20.5238
8.1210	20.5564
8.2510	20.5779
8.3710	20.5773

## ROTOR OUTLET TOTAL TEMPERATURE ( 5 POINTS)

RADIUS	TEMPERATURE
7.8710	572.227
8.0010	572.272
8.1210	573.975
8.2510	574.431
8.3710	573.030

## STAGE OUTLET TOTAL PRESSURES ( 5 POINTS)

RADIUS	MEAN PRES	PEAK PRES
7.8000	20.1102	20.6143
7.9500	20.0819	20.5803
8.1200	20.1487	20.7571
8.2800	20.2026	20.8303
8.4500	20.1297	20.4392

## STAGE OUTLET TOTAL TEMPERATURES ( 5 POINTS)

RADIUS	TEMPERATURE
7.8000	573.687
7.9500	573.153
8.1200	575.339
8.2800	577.637
8.4500	573.322

## STAGE OUTLET FLOW ANGLES ( 1 POINTS)

RADIUS	ANGLE
0.0000	0.000

## CASING STATIC PRESSURES (14 POINTS)

X-COORD	PRESSURE
-2.0000	14.4017
-1.2500	14.3557
0.0000	14.3173
0.2500	14.7776
0.5000	15.1334
0.7500	15.6123
1.0000	15.8897
1.2500	15.9153
1.5000	16.5372
1.7500	16.8434
2.0000	16.3633
2.2500	15.5537
4.7250	17.7205
5.1310	17.7205

# HUB STATIC PRESSURES ( 5 POINTS)

X-COORD	PRESSURE
-2.0000	14.4513
-2.2500	14.3257
-2.5000	14.3502
-2.7250	17.6348
-6.1810	17.6348

## (5) DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD.DEVN.	DISTRIBUTION FACTOR	FRACTION TE BLOCKAGE
1	0.00000	1.0000	-0.000	-0.0000	-0.0000
2	0.00000	1.0000	-0.000	-0.0000	-0.0000
3	0.00000	1.0000	-0.000	-0.0000	-0.0000
4	0.00000	1.0000	-0.000	-0.0000	-0.0000
5	0.00000	.8000	.010	1.0000	.2000
6	0.01000	.6000	.010	1.0000	.4000
7	0.03000	.4000	.010	1.0000	.6000
8	0.01000	.2000	.010	1.0000	.8000
9	0.03000	0.0000	.010	1.0000	1.0000
10	0.02000	0.0000	-0.000	-0.0000	-0.0000
11	0.03000	1.0000	-0.000	-0.0000	-0.0000
12	0.11000	1.0000	-0.000	-0.0000	-0.0000
13	0.13000	1.0000	-0.000	-0.0000	-0.0000
14	0.14000	1.0000	-0.000	-0.0000	-0.0000
15	0.10000	1.0000	-0.000	-0.0000	-0.0000
16	0.10000	1.0000	-0.000	-0.0000	-0.0000
17	0.10000	1.0000	-0.000	-0.0000	-0.0000

## (5) SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
NMACH	0	0	-0	-0	0	0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

NJUMP= 0

## SECTION 6. INDIVIDUAL TEST INPUT DATA

### a. EXCEPTIONS TO SECTION 1 DATA (Indicated by (1) )

Test Point Number	Exception (1)
212050109840	14.1590
212050213440	"
212050315040	"
212050415940	"
212050516240	"
212050616440	"
212050615050	14.1590
212050815750	"
212050916250	"
212051015050	"
212051114250	"
212051212250	"
212051415060	"
212051514360	"
212051612960	"
212051715560	"
212051815960	"
212051916360	"
212070215070	14.5035
212070314770	"
212070615070	"
212070715670	"
212070815970	"
212070916170	"
212071015080	14.5035
212071315080	"
212071415580	"
212071515980	"
301180915685	14.2208
301181015885	"
301180615085	"
301180815385	"
301181515590	14.2208
301181615790	"
301181715890	"
301181415290	"



301230615095	5.0097	15.0097	15.00	30.00
301230415395	""	""	""	""
301230515695	""	""	""	""
301231515600	5.0097	15.0097	15.00	30.00
301231615700	""	""	""	""
301231315200	""	""	""	""
301231415400	""	""	""	""
301240815302	""	""	""	""
301240915602	""	""	""	""

b. EXCEPTIONS TO SECTION 2 DATA  
(Indicated by (2) )

Test Point 212050109840

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212050213440

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212050315040

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212050415940

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 21205016240

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212050616440

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212050615050

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212050815750

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212050916250

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051015050

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051114250

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051212250

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051415060

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051514360

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051612960

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051715560

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051815960

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212051916360

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212070215070

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212070314770

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212070615070

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212070715670

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212070815970

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212070916170

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212071015080

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212071315080

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212071415580

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 212071515980

Station	NCALC	NDATA	NBL
4	1	15	1
5	4	15	1
6	0	0	1
7	1	10	1
8	3	10	1

Test Point 301180915685

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	1
6	0	0	1
7	1	10	2
8	3	10	1

Test Point 301181015885

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	1
6	0	0	1
7	1	10	2
8	3	10	1

Test Point 301180615085

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	1
6	0	0	1
7	1	10	2
8	3	10	1

Test Point 301180815385

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	1
6	0	0	1
7	1	10	2
8	3	10	1

Test Point 301181515590

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301181615790

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301181715890

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0



Test Point 301181415290

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301230615095

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301230415395

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301230515695

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301231515600

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301231615700

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301231315200

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301231415400

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301240815702

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

Test Point 301240915602

Station	NCALC	NDATA	NBL
4	1	15	0
5	4	15	0
6	0	0	0
7	1	10	0
8	3	10	0

c. EXCEPTIONS TO SECTION 3 DATA  
(indicated by (3) )

Test Point 212050109840

PSCALE = .50

FLOWER = 14.0

DAMP F = 6.00

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	1.0000
6	.05666	1.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050213440

PSCALE = .50

FLOWER = 14.0

DAMP F = 6.00

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	1.0000
6	.09000	1.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050315040

PSCALE = .50

FLOWER = 14.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	1.0000
6	.09000	1.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050415940

PSCALE = .50

FLOWER = 14.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.02000	1.0000
6	.09000	1.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
MMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050516240

PSCALE = .50

FLOWER = 14.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	1.0000
6	.09000	1.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
MMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050616440

PSCALE = .50

FLOWER = 14.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	1.0000
6	.05000	1.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050615050

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	.5000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050815750

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	1.00000	1.0000
4	0.00000	1.0000
5	.08000	.5000
6	.00000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212050916250

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	.5000
6	.00000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212051015050

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.00000	0.5000
6	0.00000	0.5000
7	0.00000	1.0000
8	0.05400	1.0000
9	0.05400	1.0000
10	0.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
MPACH	0	0	0	0	0	0	0	0	0	0

Test Point 212051114250

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.00000	0.0000
6	0.00000	0.0000
7	0.00000	1.0000
8	0.05400	1.0000
9	0.05400	1.0000
10	0.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
MPACH	0	0	0	0	0	0	0	0	0	0



Test Point 212051212250

PSCALE = 1.0

PLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.0000	1.0000
2	0.0000	1.0000
3	0.0000	1.0000
4	0.0000	1.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	1.0000
8	0.0000	1.0000
9	0.0000	1.0000
10	0.0000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMALH	1	0	0	0	0	0	0	0	0	0

Test Point 212051415060

PSCALE = 1.0

PLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.0000	1.0000
2	0.0000	1.0000
3	0.0000	1.0000
4	0.0000	1.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	1.0000
8	0.0000	1.0000
9	0.0000	1.0000
10	0.0000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMALH	1	0	0	0	0	0	0	0	0	0

Test Point 212051514360

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

~~DISTRIBUTED BLOCKAGE SPECIFICATION~~

~~STATION BLOCKAGE DISTRIBUTION FACTOR~~

<del>1</del>	<del>0.00000</del>	<del>1.0000</del>
<del>2</del>	<del>0.00000</del>	<del>1.0000</del>
<del>3</del>	<del>0.00000</del>	<del>1.0000</del>
<del>4</del>	<del>0.00000</del>	<del>1.0000</del>
<del>5</del>	<del>0.0000</del>	<del>0.0000</del>
<del>6</del>	<del>0.0000</del>	<del>0.0000</del>
<del>7</del>	<del>0.0000</del>	<del>1.0000</del>
<del>8</del>	<del>0.05400</del>	<del>1.0000</del>
<del>9</del>	<del>0.05400</del>	<del>1.0000</del>
<del>10</del>	<del>0.05400</del>	<del>1.0000</del>

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
MMACH	0	0	0	0	0	0	0	0	0	0

Test Point 212051612960

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

~~DISTRIBUTED BLOCKAGE SPECIFICATION~~

~~STATION BLOCKAGE DISTRIBUTION FACTOR~~

<del>1</del>	<del>0.65000</del>	<del>1.0000</del>
<del>2</del>	<del>0.00000</del>	<del>1.0000</del>
<del>3</del>	<del>0.00000</del>	<del>1.0000</del>
<del>4</del>	<del>0.00000</del>	<del>1.0000</del>
<del>5</del>	<del>0.00000</del>	<del>0.0000</del>
<del>6</del>	<del>0.00000</del>	<del>0.0000</del>
<del>7</del>	<del>0.00000</del>	<del>1.0000</del>
<del>8</del>	<del>0.05400</del>	<del>1.0000</del>
<del>9</del>	<del>0.05400</del>	<del>1.0000</del>
<del>10</del>	<del>0.05400</del>	<del>1.0000</del>

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
MMACH	0	0	0	0	0	0	0	0	0	0

Test Point 212051715560

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

~~DISTRIBUTED BLOCKAGE SPECIFICATION~~

~~STATION BLOCKAGE DISTRIBUTION FACTOR~~

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.00000	0.0000
6	0.00000	0.0000
7	0.00000	1.0000
8	0.05400	1.0000
9	0.05400	1.0000
10	0.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
RMACH	0	0	0	0	0	0	0	0	0	0

Test Point 212051815960

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

~~DISTRIBUTED BLOCKAGE SPECIFICATION~~

~~STATION BLOCKAGE DISTRIBUTION FACTOR~~

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.00000	0.0000
6	0.00000	0.0000
7	0.00000	1.0000
8	0.05400	1.0000
9	0.05400	1.0000
10	0.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
RMACH	0	0	0	0	0	0	0	0	0	0

Test Point 212051916360

PSCALE = 1.0

FLOWER = 13.0

DAMP F = 6.0

~~DISTRIBUTED BLOCKAGE SPECIFICATION~~

~~STATION BLOCKAGE DISTRIBUTION FACTOR~~

<del>1</del>	<del>0.00000</del>	<del>1.0000</del>
<del>2</del>	<del>0.00000</del>	<del>1.0000</del>
<del>3</del>	<del>0.00000</del>	<del>1.0000</del>
<del>4</del>	<del>0.00000</del>	<del>1.0000</del>
<del>5</del>	<del>.00000</del>	<del>0.0000</del>
<del>6</del>	<del>.08000</del>	<del>0.0000</del>
<del>7</del>	<del>.08000</del>	<del>1.0000</del>
<del>8</del>	<del>.05400</del>	<del>1.0000</del>
<del>9</del>	<del>.05400</del>	<del>1.0000</del>
<del>10</del>	<del>.05400</del>	<del>1.0000</del>

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	0	0	0	0	0	0	0	0

Test Point 212070215070

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	0.0000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	0	0	0	0	0	0	0	0

Test Point 212070314770

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	0.0000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212070615070

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	0.0000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212070715670

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.08000	0.0000
6	0.08000	0.0000
7	0.08000	1.0000
8	0.05400	1.0000
9	0.05400	1.0000
10	0.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212070815970

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.08000	1.0000
6	0.08000	1.0000
7	0.08000	1.0000
8	0.05400	1.0000
9	0.05400	1.0000
10	0.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212070916170

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	0.0000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	J	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212071015080

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	0.0000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	J	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212071315080

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	0.0000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 212071415580

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.08000	0.0000
6	.08000	0.0000
7	.08000	1.0000
8	.05400	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0



Test Point 212071515980

PSCALE = 2.0

PLOWER = 13.0

DAMP F = 6.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	0.0000	1.0000
3	0.0000	1.0000
4	0.0000	1.0000
5	0.0000	1.0000
6	0.0000	1.0000
7	0.0000	1.0000
8	0.0540	1.0000
9	0.0540	1.0000
10	0.0540	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 30180615085

PSCALE = 4.0

PLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.05000	1.0000
6	0.05000	1.0000
7	0.05000	1.0000
8	0.07000	1.0000
9	0.07000	1.0000
10	0.07000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
AMACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 30180815385

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.05000	0.0000
6	.05000	0.0000
7	.05000	1.0000
8	.07000	1.0000
9	.07000	1.0000
10	.07000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NPACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301180915685

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.05000	0.0000
6	.05000	0.0000
7	.05000	1.0000
8	.07000	1.0000
9	.07000	1.0000
10	.07000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NPACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 30118105885

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.05000	0.0000
6	0.05000	0.0000
7	0.05000	1.0000
8	0.07000	1.0000
9	0.07000	1.0000
10	0.07000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NRACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301181415290

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	0.03750	0.0000
6	0.03750	0.0000
7	0.07500	1.0000
8	0.27000	1.0000
9	0.05400	1.0000
10	0.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NRACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301181515590

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.03750	0.0000
6	.03750	0.0000
7	.07500	1.0000
8	.26000	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
APACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301181615790

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.03750	0.0000
6	.03750	0.0000
7	.07500	1.0000
8	.25000	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
APACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301181715890

PSCALE = 2.0

FLOWER = 13.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.03750	0.0000
6	.03750	0.0000
7	.07500	1.0000
8	.24000	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
RMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301230415395

PSCALE = 2.5

FLOWER = 13.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.03750	0.0000
6	.03750	0.0000
7	.07500	1.0000
8	.26000	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
RMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301230515695

PSCALE = 2.5

FLOWER = 13.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.05000	0.0000
6	.05000	0.0000
7	.10000	1.0000
8	.25000	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301230615095

PSCALE = 2.5

FLOWER = 13.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.03750	0.0000
6	.03750	0.0000
7	.07500	1.0000
8	.26500	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NMACH	0	0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301231315200

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

# DISTRIBUTED FLOWAGE SPECIFICATION

## STATION FLOWAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	0.0000	1.0000
3	0.0000	1.0000
4	0.0000	1.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	1.0000
8	0.0000	1.0000
9	0.0000	1.0000
10	0.0000	1.0000

## SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
SMALL	0	0	0	0	0	0	0	0	0	0

Test Point 301231415400

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

# DISTRIBUTED FLOWAGE SPECIFICATION

## STATION FLOWAGE DISTRIBUTION FACTOR

1	0.0000	1.0000
2	0.0000	1.0000
3	0.0000	1.0000
4	0.0000	1.0000
5	0.0000	0.0000
6	0.0000	0.0000
7	0.0000	1.0000
8	0.0000	1.0000
9	0.0000	1.0000
10	0.0000	1.0000

## SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
SMALL	0	0	0	0	0	0	0	0	0	0

Test Point 301231515600

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION		
STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.05000	0.0000
6	.05000	0.0000
7	.10000	1.0000
8	.25000	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS										
STATION	1	2	3	4	5	6	7	8	9	10
NRACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301231615700

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION		
STATION	BLOCKAGE	DISTRIBUTION FACTOR
1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.05000	0.0000
6	.05000	0.0000
7	.10000	1.0000
8	.25000	1.0000
9	.05400	1.0000
10	.05400	1.0000

SOLUTION TYPE INDICATORS										
STATION	1	2	3	4	5	6	7	8	9	10
NRACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0



Test Point 301240815302

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.05000	0.0000
6	.05000	0.0000
7	.07500	1.0000
8	.26000	1.0000
9	.05000	1.0000
10	.05000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NRACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0

Test Point 301240915602

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 4.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION BLOCKAGE DISTRIBUTION FACTOR

1	0.00000	1.0000
2	0.00000	1.0000
3	0.00000	1.0000
4	0.00000	1.0000
5	.03750	0.0000
6	.03750	0.0000
7	.07500	1.0000
8	.20000	1.0000
9	.05000	1.0000
10	.05000	1.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10
NRACH	0	-0	-0	-0	-0	-0	-0	-0	-0	-0

d. EXCEPTIONS TO SECTION 4 DATA  
(Indicated by (4) )

Test Point 212050315040

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	2	15	3

OUTLET RADIUS = 7.5433

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-3.0000
.4000	-6.7200
.5000	-8.3000
.8000	-8.0000

OUTLET RADIUS = 3.0331

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-7.3000
.4000	-7.2000
.5000	-7.1000
.8000	-7.0000

OUTLET RADIUS = 1.5533

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-8.0000
.4000	-9.0000
.5000	-10.2000
.8000	-11.2000

Test Point 212050615050

Station	NCALC	NDATA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	2	15	3

OUTLET RADIUS = 7.5499

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-9.0000
.4000	-8.7000
.6000	-8.3000
.8000	-8.0000

OUTLET RADIUS = 3.0331

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-7.3000
.4000	-7.2000
.6000	-7.1000
.8000	-7.0000

OUTLET RADIUS = 3.0599

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-8.0000
.4000	-9.1000
.6000	-10.2000
.8000	-11.2000

Test Point 212051715560

Station	NCALC	NDA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	2	15	3

OUTLET RADIUS = 7.5499

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-8.8000
.4000	-7.9200
.6000	-7.1000
.8000	-6.2000

OUTLET RADIUS = 3.0235

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-7.4000
.4000	-7.1000
.6000	-6.8000
.8000	-5.4000

OUTLET RADIUS = 8.6599

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-7.7500
.4000	-9.0500
.6000	-10.3500
.8000	-11.6500

Test Point 212070815970

Station	NCALC	NDA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	4	15	3

OUTLET RADIUS = 7.5499

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1750
.4000	-5.4200
.8000	-4.7700

OUTLET RADIUS = 7.7343

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.0750
.4000	-4.5420
.8000	-4.7060

OUTLET RADIUS = 7.9385

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1000
.4000	-4.2030
.8000	-4.6500

OUTLET RADIUS = 8.1919

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3750
.4000	-5.7420
.8000	-6.5890

OUTLET RADIUS = 8.5599

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-7.3250
.4000	-12.3300
.8000	-25.0850

Test Point 212071515980

Station	NCALC	NDAITA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	4	15	3

OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1750
.4000	-5.4200
.8000	-4.7700

OUTLET RADIUS = 7.7343

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.0750
.4000	-4.5420
.8000	-4.7060

OUTLET RADIUS = 7.9335

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1000
.4000	-4.2030
.8000	-4.6500

OUTLET RADIUS = 8.1919

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3750
.4000	-5.7420
.8000	-6.5890

OUTLET RADIUS = 8.6399

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3250
.4000	-12.3300
.8000	-25.0850

Test Point 301181015885

Station	NCALC	NDA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	4	15	0

OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-6.1750
.4000	-5.4200
.8000	-4.7700

OUTLET RADIUS = 7.7343

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.4750
.4000	-4.5420
.8000	-4.7060

OUTLET RADIUS = 7.9395

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1000
.4000	-4.2030
.8000	-4.6500

OUTLET RADIUS = 8.1919

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3750
.4000	-5.7420
.8000	-6.5890

OUTLET RADIUS = 8.6699

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-7.3250
.4000	-12.3300
.8000	-25.0850

Test Point 301181715890

Station	NCALC	NDATA	NBL
5	2	15	0
6	2	15	3
7	2	15	3
8	2	15	3
9	4	15	0

OUTLET RADIUS = 7.5499

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-6.1750
.4000	-5.4200
.8000	-4.7700

OUTLET RADIUS = 7.7343

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.4750
.4000	-4.5420
.8000	-4.7060

OUTLET RADIUS = 7.9385

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1000
.4000	-4.2030
.8000	-4.6500

OUTLET RADIUS = 8.1319

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3750
.4000	-5.7420
.8000	-6.5890

OUTLET RADIUS = 8.6699

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-7.3250
.4000	-12.3300
.8000	-25.0850

Test Point 301230515695

Station	NCALC	NDATA	NBL
5	2	15	0
6	2	15	0
7	2	15	3
8	2	15	3
9	4	15	0

OUTLET RADIUS = 7.5499

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3750
.4000	-5.4200
.8000	-4.7700

OUTLET RADIUS = 7.7343

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-4.6750
.4000	-4.5420
.8000	-4.7060

OUTLET RADIUS = 7.9385

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-4.5000
.4000	-4.2030
.8000	-4.6500

OUTLET RADIUS = 8.1919

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-4.5750
.4000	-5.7420
.8000	-6.5890

OUTLET RADIUS = 8.6599

1-COORD DEVIATION ANGLE (DEGREES)

.2000	-6.5250
.4000	-12.3300
.8000	-25.0850



Test Point 301231615700

Station	NCAIC	NDAITA	NBL
5	2	15	0
6	2	15	0
7	2	15	3
8	2	15	3
9	4	15	0

OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-4.7640
.4000	-5.2750
.8000	-4.7700

OUTLET RADIUS = 7.7343

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-4.0730
.4000	-4.3750
.8000	-4.7060

OUTLET RADIUS = 7.9385

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-3.9700
.4000	-4.1500
.8000	-4.6500

OUTLET RADIUS = 8.1919

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-3.9600
.4000	-5.3750
.8000	-6.5890

OUTLET RADIUS = 8.6699

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.7160
.4000	-11.7500
.8000	-24.0850

Test Point 301240915602

Station	NCALC	NDA	NBL
5	2	15	3
6	2	15	3
7	2	15	3
8	2	15	3
9	4	15	0

OUTLET RADIUS = 7.5499

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1750
.4000	-5.4200
.8000	-4.7700

OUTLET RADIUS = 7.7343

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.0750
.4000	-4.5420
.8000	-4.7060

OUTLET RADIUS = 7.9395

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.1000
.4000	-4.2030
.8000	-4.6500

OUTLET RADIUS = 8.1919

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3750
.4000	-5.7420
.8000	-6.5890

OUTLET RADIUS = 8.6599

M-COORD DEVIATION ANGLE (DEGREES)

.2000	-5.3250
.4000	-12.3300
.8000	-25.0850

e. EXCEPTIONS TO SECTION 5 DATA  
(indicated by (5) )

Test Point 212050315040

PSCALE = 1.0

FLOWER = 14.0

DAMP F = 5.0

# DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD.DEVN.
1	0.00000	1.00000	-0.0000
2	0.00000	1.00000	-0.0000
3	0.00000	1.00000	-0.0000
4	0.00000	1.00000	-0.0000
5	.00300	.80000	.0100
6	.00700	.50000	.0100
7	.01000	.40000	.0100
8	.01400	.20000	.0100
9	.01800	0.00000	.0100
10	.03000	0.00000	-0.0000
11	.03000	1.00000	-0.0000
12	.05000	1.00000	-0.0000
13	.07000	1.00000	-0.0000
14	.08000	1.00000	-0.0000
15	.10000	1.00000	-0.0000
16	.10000	1.00000	-0.0000
17	.10000	1.00000	-0.0000

# SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
WACH	0	0	-0	-0	0	0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 212050615050

PSCALE = 1.0

FLOWER = 14.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD.DEVN.
1	0.00000	1.0000	-0.000
2	0.00000	1.0000	-0.000
3	0.00000	1.0000	-0.000
4	0.00000	1.0000	-0.000
5	.00400	.8000	.010
6	.00800	.6000	.010
7	.01200	.4000	.010
8	.01600	.2000	.010
9	.02100	0.0000	.010
10	.03000	0.0000	-0.000
11	.03000	1.0000	-0.000
12	.05000	1.0000	-0.000
13	.07000	1.0000	-0.000
14	.03000	1.0000	-0.000
15	.10000	1.0000	-0.000
16	.10000	1.0000	-0.000
17	.10000	1.0000	-0.000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
NMACH	0	0	-0	-0	0	0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 212051715560

PSCALE = 1.0

FLOWER = 14.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD.DEVN.
1	0.00000	1.0000	-0.000
2	0.00000	1.0000	-0.000
3	0.00000	1.0000	-0.000
4	0.00000	1.0000	-0.000
5	.01000	.8000	.010
6	.02000	.6000	.010
7	.03000	.4000	.010
8	.04000	.2000	.010
9	.05000	0.0000	.010
10	.03000	0.0000	-0.000
11	.03000	1.0000	-0.000
12	.05000	1.0000	-0.000
13	.07000	1.0000	-0.000
14	.08000	1.0000	-0.000
15	.10000	1.0000	-0.000
16	.10000	1.0000	-0.000
17	.10000	1.0000	-0.000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
NMACH	0	0	-0	-0	0	0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 2120/0811 17.

PSCALE = 2.5

POWER = 12.5

DAMP F = 5.0

## DISTRIBUTED BLOCKAGE SPECIFICATION

STAFFING BLOCKAGE DISTRIBUTION FACTOR

MID ALD. DEVN.

1	0.10000	1.00000	-0.0000
2	0.00000	1.00000	-0.0000
3	0.00000	1.00000	-0.0000
4	0.00000	1.00000	-0.0000
5	0.00000	1.00000	-0.0000
6	0.00000	1.00000	-0.0000
7	0.00000	1.00000	-0.0000
8	0.00000	1.00000	-0.0000
9	0.00000	1.00000	-0.0000
10	0.00000	1.00000	-0.0000
11	0.00000	1.00000	-0.0000
12	0.00000	1.00000	-0.0000
13	0.00000	1.00000	-0.0000
14	0.00000	1.00000	-0.0000
15	0.00000	1.00000	-0.0000
16	0.00000	1.00000	-0.0000
17	0.00000	1.00000	-0.0000

SOLUTION TYPE: TROUBLE-1023

STAFF	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
NMASC	0	0	-0	-0	0	0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 21 9/11-15/50

1994 = 100

LOWEY = 12.5

LAMP F = 5.0

# DISPATCHED RELEASE SPECIFICATION

STATION BLOCKS DISTRIBUTION FACTOR

MTD ADD. DIVN.

1	0.00000	1.00000	-0.00000
2	0.00000	1.00000	-0.00000
3	0.00000	1.00000	-0.00000
4	0.00000	1.00000	-0.00000
5	0.00000	1.00000	-0.00000
6	0.00000	1.00000	-0.00000
7	0.00000	1.00000	-0.00000
8	0.00000	1.00000	-0.00000
9	0.00000	1.00000	-0.00000
10	0.00000	1.00000	-0.00000
11	0.00000	1.00000	-0.00000
12	0.00000	1.00000	-0.00000
13	0.00000	1.00000	-0.00000
14	0.00000	1.00000	-0.00000
15	0.00000	1.00000	-0.00000
16	0.00000	1.00000	-0.00000
17	0.00000	1.00000	-0.00000

## SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
MAJOR	0	0	-0	-0	0	-0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 301181015885

PSCALE = 3.0

FLOWER = 12.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD.DEVN.
1	0.00000	1.00000	-0.0000
2	0.00000	1.00000	-0.0000
3	0.00000	1.00000	-0.0000
4	0.00000	1.00000	-0.0000
5	0.00000	.30000	.0010
6	.00100	.50000	.0010
7	.00300	.40000	.0010
8	.01000	.20000	.0010
9	.05000	0.00000	.0010
10	.02000	0.00000	-0.0000
11	.03000	1.00000	-0.0000
12	.11000	1.00000	-0.0000
13	.13000	1.00000	-0.0000
14	.14000	1.00000	-0.0000
15	.10000	1.00000	-0.0000
16	.10000	1.00000	-0.0000
17	.10000	1.00000	-0.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
MAC4	0	0	-0	-0	1	-0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 301181715890

PSCALE = 3.0

FLOWER = 12.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD.DEVN.
1	0.00000	1.00000	-0.0000
2	0.00000	1.00000	-0.0000
3	0.00000	1.00000	-0.0000
4	0.00000	1.00000	-0.0000
5	0.00000	.80000	.0010
6	.00100	.50000	.0010
7	.00300	.40000	.0010
8	.01000	.20000	.0010
9	.05000	0.00000	.0010
10	.02000	0.00000	-0.0000
11	.03000	1.00000	-0.0000
12	.11000	1.00000	-0.0000
13	.13000	1.00000	-0.0000
14	.14000	1.00000	-0.0000
15	.10000	1.00000	-0.0000
16	.10000	1.00000	-0.0000
17	.10000	1.00000	-0.0000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
MAC4	0	0	-0	-0	1	-0	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 301230515695

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 5.0

# DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD. DEVN.
1	0.00000	1.00000	-0.000
2	0.00000	1.00000	-0.000
3	0.00000	1.00000	-0.000
4	0.00000	1.00000	-0.000
5	0.00000	.50000	.010
6	.00100	.50000	.010
7	.00300	.40000	.010
8	.01000	.20000	.010
9	.05000	0.00000	.010
10	.02000	0.00000	-0.000
11	.03000	1.00000	-0.000
12	.11000	1.00000	-0.000
13	.15000	1.00000	-0.000
14	.14000	1.00000	-0.000
15	.13000	1.00000	-0.000
16	.10000	1.00000	-0.000
17	.10000	1.00000	-0.000

## SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
N-ACH	0	0	-1	-1	1	-1	-0	-0	-0	-1	-0	-0	0	0	-0	-0	-0

Test Point 301231615700

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 5.0

# DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD. DEVN.
1	0.00000	1.00000	-0.000
2	0.00000	1.00000	-0.000
3	0.00000	1.00000	-0.000
4	0.00000	1.00000	-0.000
5	0.00000	.50000	.010
6	.00100	.50000	.010
7	.00300	.40000	.010
8	.01000	.20000	.010
9	.05000	0.00000	.010
10	.02000	0.00000	-0.000
11	.03000	1.00000	-0.000
12	.13000	1.00000	-0.000
13	.15000	1.00000	-0.000
14	.17000	1.00000	-0.000
15	.10000	1.00000	-0.000
16	.10000	1.00000	-0.000
17	.10000	1.00000	-0.000

## SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
N-ACH	0	0	-0	-1	1	1	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0

Test Point 301240915602

PSCALE = 4.0

FLOWER = 12.0

DAMP F = 5.0

DISTRIBUTED BLOCKAGE SPECIFICATION

STATION	BLOCKAGE	DISTRIBUTION FACTOR	MID ADD.DEVN.
1	0.00000	1.0000	-0.000
2	0.00000	1.0000	-0.000
3	0.00000	1.0000	-0.000
4	0.00000	1.0000	-0.000
5	0.00000	.8000	.010
6	.00100	.6000	.010
7	.00300	.4000	.010
8	.01000	.2000	.010
9	.03500	0.0000	.010
10	.02000	0.0000	-0.000
11	.03000	1.0000	-0.000
12	.11000	1.0000	-0.000
13	.13000	1.0000	-0.000
14	.14000	1.0000	-0.000
15	.10000	1.0000	-0.000
16	.10000	1.0000	-0.000
17	.10000	1.0000	-0.000

SOLUTION TYPE INDICATORS

STATION	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
NMACH	0	0	-0	-0	1	1	-0	-0	-0	-0	-0	-0	0	0	-0	-0	-0



**APPENDIX C**  
**ADDITIONAL CALCOMP PLOTTING ROUTINE**  
**LISTINGS**

This appendix contains the program listings for the DEVILLOT and STAPLOT plotting routines. Section C1 contains the input format and program listing for DEVILLOT. Section C2 contains the input format and program listing for STAPLOT.

## SECTION C1. DEVPLOT PROGRAM

### 1. DEVPLOT INPUT DATA FORMAT

In the following chart, the line corresponds to the card except where noted. Values in parentheses indicate the input format for the corresponding variable.

NOCASE	(1)	NPLOT	(16)	
NHASE	(1)	NHASE	(16)	
NOCASE	(F1.8)	XY	(F1.8) R (F1.8)	} occurs HCase Times
* (16)		id	(16)	

### 2. DEFINITION OF INPUT DATA ITEMS

NOCASE	Number of Cases (Speed Points) to be Plotted
NPLOT	Plotting option. NPLOT = 1, Plots will be made. NPLOT = 0, No plots will be made.
NHASE	Test Point Identification (Percent Design Speed)
NHASE	Number of Input Deviation Angles to be Plotted for each NOCASE. Includes Streamline, Computing Station and Corresponding Deviation Angle
NOCASE	Deviation angle
XY	Normalized Axial Distance
R	Radial Distance
id	Computing Station Number Corresponding to Phase II Calculations
id	Streamline Number Corresponding to Phase II Calculations

\* Continuation of previous line.

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c. PROGRAM LISTING

```

PROGRAM DEVLOT(INPUT,OUTPUT,PLOT)
DIMENSION DEVSGN(10,3),XX2(10,3),R(10,3),II(10,3),JJ(10,3)
READ 10,NCASE,NPLOT
10 FORMAT (2I6)
PRINT 20,NCASE,NPLOT
20 FORMAT (1H1,10X,20HROTJ THRU-3BLADE DEVIATION,//,10X,17HNUMBER OF
1CASES =,I3,//,10X,7HNPLOT =,I2)
M=1
30 READ 40,NSPEED,NPOINTS
40 FORMAT (2I6)
PRINT 50,NSPEED,NPOINTS
50 FORMAT (1H1,10X,12HTEST SPEED =,I4,1HX,//,10X,23HNUMBER OF DATA PO
INTS =,I3,/,2X)
READ 60,((DEVSGN(I,J),XX2(I,J),R(I,J),II(I,J),JJ(I,J),J=1,3),I=1,6
1)
60 FORMAT (3F12.6,2I6)
PRINT 70
70 FORMAT (//,22X,10HNORMALIZED,/,11X,7HSTATION,2X,14HAXIAL DISTANCE,1
1X,9HDEVIATION,2X,10HSTRAKE LINE,3X,6HRAJUS,/,2X)
DO 80 J=1,3
DO 80 I=1,6
80 XX2(I,J)=X(2(I,J)/2.0
DO 100 J=1,3
DO 100 I=1,6
PRINT 90, II(I,J),XX2(I,J),DEVSGN(I,J),JJ(I,J),R(I,J)
90 FORMAT (10X,I6,3X,F10.2,+,X,F10.4,3X,I6,3X,F10.4)
100 CONTINUE
IF(NPLOT.EQ.0)GO TO 150
CALL PLOT(0.0,-12.0,-3)
CALL PLOT(3.0,2.0,-3)
CALL AXIS(0.,0.,25HNORMALIZED AXIAL DISTANCE,-25,5.,0.,0.,.2)
CALL AXIS(0.,0.,25HROTJ INCIDENCE/DEVIATION,25,7.,90.,0.,5.)
FPN=NSPEED)
CALL NUMBER(3.0,8.25,.25,FPN,0.,-1)
CALL SYMBOL(1.0,6.7,.105,0,0.,-1)
CALL SYMBOL(1.30,6.45,.125,3MHUB,0.,3)
CALL SYMBOL(1.0,6.1,.105,1,0.,-1)
CALL SYMBOL(1.30,6.35,.125,3HMID,0.,3)
CALL SYMBOL(1.0,5.7,.105,2,0.,-1)
CALL SYMBOL(1.30,5.65,.125,3HTIP,0.,3)
DO 110 J=1,3
XX2(7,J)=0.0
XX2(8,J)=0.2
DEVSGN(7,J)=0.0
DEVSGN(8,J)=5.0
L=J-1
110 CALL LINE(XX2(1,J),DEVSGN(1,J),6,1,1,L)
CALL PLOT(8.,0.,-3)

```

```
150 CONTINUE
    IF (M.EQ.NCASE) GO TO 170
    M=M+1
    GO TO 30
170 CONTINUE
    CALL PLOT2
    END
```

## SECTION C2. STAPLOT PROGRAM

### a. STAPLOT INPUT DATA FORMAT

In the following chart, one line corresponds to one card. Values in parentheses indicate the input format for the corresponding variable.

NCASE	(I6)	NPLOT	(I6)		
NTITLE	(112)				
NPSPTS	(I6)				
FDIST	(F10.0)	PSP	(F10.0)	} Occurs NPSPTS Times	
FDIST	(NPPT)	(F10.0)	PSP (NPPT)	(F10.0)	} Occurs NCASE Times
FDIST	(NPPTS)	(F10.0)	PSP (NPPTS)	(F10.0)	
NCSPTS	(I6)				
FDIST	(F10.0)	SSP	(F10.0)	} Occurs NCSPTS Times	
FDIST	(NPPT)	(F10.0)	SSP (NPPT)	(F10.0)	
FDIST	(NPPTS)	(F10.0)	SSP (NPPTS)	(F10.0)	

## 1. DEFINITION OF INPUT DATA ITEMS

NCASE      Number of Test Point Cases to be run  
(Each requires a separate input data set).

NPLOT      Plotting Option. NPLOT = 1, Plots will be  
made. NPLOT = 0, No plots will be made.

NFILE      12 Digit Test Point Identification Number  
for each NCASE.

NPSPTS      Number of Pressure Surface Static Pressure  
Readings to be Input for each NCASE.

PDIST      Chord Distance from Leading Edge (On chosen  
radius) of each Pressure Tap on Pressure  
surface.

PCP      Pressure Surface Static Pressure at each PDIST.

SDIST      Same as PDIST, except for Suction Surface  
Pressure Taps.

SCP      Suction Surface Static Pressure at each SDIST.

NSPPTS      Same as NPSPTS except for Suction Surface.

NPPT      (NPSPTS + 1) Array Location for Starting  
Value of Static Pressure Axis (YAXIS).

NPPTS      (NSPPTS + 1) Array Location Pressure/in value  
for Pressure Axis (YAXIS).

NSPT      (NSPPTS + 1) Same as NPPT.

NSPTS      (NSPPTS + 2) Same as NPPTS.

PERCENT(1) Starting Value of Percent Chord Axis (X AXIS).

PERCENT(PTS) Percent Chord/in value for X Axis.

PDIST(NPPT) Same as PDIST(NPPT).

PDIST(NPPTS) Same as PDIST(NPPTS).

PCP(1) Starting Value of Static Pressure Axis.

PSF(NPPTS)	Pressure/in Value for Static Pressure Axis.
SSP(NPPT)	Same as PSP (NPPT)
SSP(NPPTS)	Same as PSP(NPPTS)

c. PROGRAM LISTING

```

PROGRAM STAPLOT(INPUT,OUTPUT,PLOT)
DIMENSION PJIST(400),PSP(400),SSP(400),SDIST(400)
READ 10,NCASE,NPLOT
10 FORMAT(2I12)
PRINT 20,NCASE,NPLOT
20 FORMAT (1H1,10X,31HSTATOR SURFACE STATIC PRESSURES,//, 9X,17HNUMBER
OF CASES =,I3,//,9X, 7HNPLOT =,I3)
I=1
30 READ 40,NTITLE
40 FORMAT (I12)
PRINT 50,NTITLE
50 FORMAT (1H1,//,20X,18HTEST POINT NUMBER ,I12)
READ 60,NPSPTS
60 FORMAT (I12)
J=NPSPTS+2
READ 70,(PDIST(K),PSP(K),K=1,J)
70 FORMAT (F10.2,F10.3)
DO 80 L=1,NPSPTS
80 PDIST(L)=(((PDIST(L)-2.93)/1.795)*100.0)
PRINT 90,(PDIST(K),PSP(K),K=1,NPSPTS)
90 FORMAT (///,24X,22HSTATIC PRESSURE (PSIA),//,27X,16HPRESSURE SURFA
CE,//,18X,13HPERCENT CHORD,10X,8HPRESSURE,//,(17X,F10.2,11X,F10.3)
2)
READ 100,NSSPTS
100 FORMAT (I12)
J=NSSPTS+2
READ 110,(SDIST(K),SSP(K),K=1,J)
110 FORMAT (2F10.3)
DO 120 L=1,NSSPTS
120 SDIST(L)=(((SDIST(L)-2.93)/1.795)*100.0)
PRINT 130,(SDIST(K),SSP(K),K=1,NSSPTS)
130 FORMAT(///,28X,15HSUCTION SURFACE,//,18X,13HPERCENT CHORD,10X,8HPR
ESSURE,//,(17X,F10.2,11X,F10.3))
IF(1-NPLOT) 150,140,150
140 CONTINUE
NPPT=NPSPTS+1
NPPTS=NPPTS+2
NSPT=NSSPTS+1
NSPTS=NSPTS+2
CALL PLOT(0.0,-12.0,-3)
CALL PLOT(3.0,2.0,-3)
CALL AXIS(0.,0.,13HPERCENT CHORD,-13.5.,0.,PDIST(NPPT),PDIST(NPPTS
1))
CALL AXIS(0.,0.,15HPRESSURE (PSIA),15.5.,90.,PSP(NPPT),PSP(NPPTS))
CALL LINE(PDIST,PSP,NPSPTS,1,1,0)
CALL LINE(SDIST,SSP,NSSPTS,1,1,4)
FPN=NTITLE
CALL NUMBER(1.8,6.25,.2,FPN,0.,-1)

```



```

CALL SYMBOL(1.5,5.8,.105,0,0.,-1)
CALL SYMBOL(1.8,5.74,.125,16MPRESSURE SURFACE,0.,16)
CALL SYMBOL(1.5,5.48,.105,4,0.,-1)
CALL SYMBOL(1.8,5.42,.125,15MSUCTION SURFACE,0.,15)
CALL SYMBOL(1.5,5.16,.105,0,0.,-1)
CALL SYMBOL(1.5,5.16,.105,4,0.,-1)
CALL SYMBOL(1.8,5.18,.125,17MCALCULATED VALUES,0.,17)
CALL SYMBOL(1.8,4.90,.125,24MLEADING & TRAILING EDGES,0.,24)
CALL PLOT(6.,0.,-3)
150 CONTINUE
    IF (I-NCASE) 160,170,170
160 I=I+1
    GO TO 30
170 CONTINUE
    CALL PLOTE
    END

```

## **APPENDIX D**

### **RAW EXPERIMENTAL DATA**

This appendix presents a listing of the experimental data after being dumped from magnetic tape onto computer cards. The first two ten-character "words" of each test contain the test identification number.



TEST I.O.J. NUMBER 212050213440

0000000212	05021344	00000000000056	0+000362600000000057	0+000566600000000058	0+0016756
0000000053	0+0000106000000000	00000000000000	0+000202000000000061	0+000249600000000062	0+0002516
0000000063	0+0002526000000000	00000000000000	0+001029600000000065	0+001027000000000066	0+0009576
0000000067	0+0009026000000000	00000000000000	0+000959600000000069	0+000555600000000070	0+0009346
0000000071	0+0009356000000000	00000000000000	0+000946600000000073	0+000543600000000074	0+0010266
0000000075	0+0010396000000000	00000000000000	0+000977600000000077	0+001021600000000078	0+0010266
0000000079	0+0010759000000000	00000000000000	0+000334600000000081	0+001044600000000082	0+0009956
0000000083	0+0010166000000000	00000000000000	0+000332600000000085	0+000970600000000086	0+0009766
0000000087	0+0009886000000000	00000000000000	0+000358600000000089	0+000525600000000090	0+0014356
0000000091	0+0009906000000000	00000000000000	0+000341600000000093	0+000567600000000094	0+0009416
0000000095	0+0418376000000000	00000000000000	0+001004600000000097	0+000571600000000098	0+0009916
0000000099	0F0003033000000000	00000000000000	0+017036600000000001	0+017509600000000001	0+0073036
0000000103	0+0014526000000000	00000000000000	0+010542600000000003	0+017359600000000003	0+0073036
0000000107	0+0013556000000000	00000000000000	0+017033600000000005	0+017651600000000005	0+0074216
0000000111	0+0011910000000000	00000000000000	0+010293600000000007	0+017101600000000007	0+0071636
0000000115	0+0015056000000000	00000000000000	0+015379600000000009	0+017225600000000009	0+0078436
0000000119	0+0012336000000000	00000000000000	0+015934600000000011	0+017556600000000011	0+0060906
0000000123	0+0014386000000000	00000000000000	0+015999600000000013	0+016660600000000013	0+0060806
0000000127	0+0013706000000000	00000000000000	0+016077600000000015	0+016084600000000015	0+0060856
0000000131	0+0011646000000000	00000000000000	0+010334600000000017	0+016635600000000017	0+0060336
0000000135	0+0014926000000000	00000000000000	0+016933600000000019	0+016637600000000019	0+0060566
0000000139	0+0012596000000000	00000000000000	0+016551600000000021	0+018129600000000021	0+0061036
0000000143	0+0015226000000000	00000000000000	0+016679600000000023	0+017565600000000023	0+0061296
0000000147	0+0014206000000000	00000000000000	0+017155600000000025	0+018553600000000025	0+0061226
0000000151	0+0012146000000000	00000000000000	0+017430600000000027	0+018256600000000027	0+0061106
0000000155	0+0015706000000000	00000000000000	0+017532600000000029	0+018679600000000029	0+0061306
0000000159	0+0013546000000000	00000000000000	0+013521600000000031	0+018486600000000031	0+0061746
0000000163	0+0015356000000000	00000000000000	0+012935600000000033	0+018357600000000033	0+0061846
0000000167	0+0015056000000000	00000000000000	0+013533600000000035	0+018479600000000035	0+0064076
0000000171	0+0012156000000000	00000000000000	0+014334600000000037	0+018632600000000037	0+0061306
0000000175	0+0012460000000000	00000000000000	0+015757600000000039	0+018567600000000039	0+0064436
0000000179	0+0013516000000000	00000000000000	0+017071600000000041	0+017510600000000041	0+0073026
0000000183	0+0003346000000000	00000000000000	0+017072600000000043	0+017509600000000043	0+0073026
0000000187	0+0003336000000000	00000000000000	0+035679600000000045	0+036535600000000045	0+0083636
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TEST 1.0. NUMBER 21205091640

0000000212	05061044	00000000000056	00010436	00000000000057	00010546	00000000000058	00010656
0000000053	00000010	00000000000060	00000236	00000000000061	00000252	00000000000062	00000212
0000000053	00000234	00000000000064	00011276	00000000000065	00011266	00000000000066	00011266
0000000067	00011336	00000000000068	00001056	00000000000069	00010256	00000000000070	00010256
0000000071	00010306	00000000000072	00011436	00000000000073	00010276	00000000000074	00010276
0000000075	00011136	00000000000076	00010456	00000000000077	00011256	00000000000078	00011456
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0000000083	00011136	00000000000084	00011136	00000000000085	00010516	00000000000086	00011646
0000000087	00011166	00000000000088	00011416	00000000000089	00010756	00000000000090	00003496
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0000000095	00035356	00000000000096	00011236	00000000000097	00010426	00000000000098	00010556
0000000099	00000053	00000000000100	00017016	00000000000101	00017504	00000000000102	000073056
0000000101	00015436	00000000000103	00010716	00000000000104	00017556	00000000000105	000073056
0000000103	00013236	00000000000104	00017036	00000000000105	00017656	00000000000106	00005336
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0000000107	00017656	00000000000109	00010406	00000000000110	00013266	00000000000111	000064126
0000000109	00017086	00000000000111	00016436	00000000000112	00015356	00000000000113	000058566
0000000111	00015226	00000000000113	00016456	00000000000114	00017316	00000000000115	000058566
0000000113	00015376	00000000000115	00016406	00000000000116	00017367	00000000000117	000058576
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0000000119	00016456	00000000000121	00017906	00000000000122	00016036	00000000000123	000058246
0000000121	00015436	00000000000123	00017943	00000000000124	00019436	00000000000125	000058356
0000000123	00015616	00000000000125	00016213	00000000000126	00020216	00000000000127	000058366
0000000125	00015336	00000000000127	00016356	00000000000128	00020234	00000000000129	000058156
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0000000133	00015336	00000000000135	00017576	00000000000136	00020152	00000000000137	000061376
0000000135	00016276	00000000000137	00016036	00000000000138	00020220	00000000000139	000059086
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0000000143	00003376	00000000000145	00035356	00000000000146	00055166	00000000000147	000062546
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# TEST I.O. NUMBER 212050619750

0000000212	05061575000000000056	0+0015056000000000057	0+001466600000000056	0+001466600000000056	0+001466600000000056
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0000000063	0+000207600000000061	0+001001600000000063	0+001001600000000063	0+001001600000000063	0+001001600000000063
0000000067	0+001535000000000068	0+001525000000000063	0+001525000000000063	0+001525000000000063	0+001525000000000063
0000000071	0+001400000000000072	0+015904000000000073	0+001452000000000074	0+001452000000000074	0+001452000000000074
0000000075	0+001050600000000076	0+001400000000000077	0+001452000000000078	0+001452000000000078	0+001452000000000078
0000000079	0+001050600000000080	0+001500000000000081	0+001452000000000082	0+001452000000000082	0+001452000000000082
0000000083	0+001050600000000084	0+001400000000000085	0+001452000000000086	0+001452000000000086	0+001452000000000086
0000000087	0+001050600000000088	0+001572000000000089	0+001452000000000090	0+001452000000000090	0+001452000000000090
0000000091	0+001557000000000092	0+001420000000000093	0+001452000000000094	0+001452000000000094	0+001452000000000094
0000000095	0+004070600000000096	0+001400000000000097	0+001452000000000098	0+001452000000000098	0+001452000000000098
0000000099	0F00100000000000101	0+0017000000000000201	0+0017000000000000201	0+0017000000000000201	0+0017000000000000201
0000000401	0+002202000000000103	0+0010493600000000203	0+0017000000000000203	0+0017000000000000203	0+0017000000000000203
0000000403	0+002675000000000105	0+0017053600000000205	0+0017053600000000205	0+0017053600000000205	0+0017053600000000205
0000000405	0+002133000000000107	0+0016139000000000207	0+0016501000000000207	0+0016501000000000207	0+0016501000000000207
0000000407	0+002577000000000109	0+0017053600000000209	0+0013420000000000309	0+0013420000000000309	0+0013420000000000309
0000000409	0+002401000000000111	0+0015820000000000211	0+0015820000000000311	0+0015820000000000311	0+0015820000000000311
0000000411	0+002121000000000113	0+0015030600000000213	0+0016705000000000313	0+0016705000000000313	0+0016705000000000313
0000000413	0+002531000000000115	0+0020294000000000215	0+0016657000000000315	0+0016657000000000315	0+0016657000000000315
0000000415	0+002172000000000117	0+0015030600000000217	0+0016640000000000317	0+0016640000000000317	0+0016640000000000317
0000000417	0+002507000000000119	0+0017120000000000219	0+0016655000000000319	0+0016655000000000319	0+0016655000000000319
0000000419	0+002422000000000121	0+0017053600000000221	0+0015303000000000321	0+0015303000000000321	0+0015303000000000321
0000000421	0+002162000000000123	0+0017053600000000223	0+0015050000000000323	0+0015050000000000323	0+0015050000000000323
0000000423	0+002605000000000125	0+0015030600000000225	0+0015050000000000325	0+0015050000000000325	0+0015050000000000325
0000000425	0+002214000000000127	0+0016737000000000227	0+0015050000000000327	0+0015050000000000327	0+0015050000000000327
0000000427	0+002505000000000129	0+0016737000000000229	0+0015050000000000329	0+0015050000000000329	0+0015050000000000329
0000000429	0+002311000000000131	0+0014210000000000231	0+0015050000000000331	0+0015050000000000331	0+0015050000000000331
0000000431	0+002270000000000133	0+0015053600000000233	0+0015050000000000333	0+0015050000000000333	0+0015050000000000333
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0000000435	0+002207000000000137	0+0017012000000000237	0+0015050000000000337	0+0015050000000000337	0+0015050000000000337
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TEST 1.0. NUMBER 212050916230

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0000000007	0+00161800000000000068	0+00157960000000000069	0+001555600000000070	0+0014816
0000000071	0+00140960000000000072	0+00192560000000000073	0+001472000000000074	0+0016646
0000000075	0+00107360000000000076	0+00143960000000000077	0+001628000000000078	0+0017026
0000000079	0+00174960000000000080	0+00160060000000000081	0+001730600000000082	0+0015666
0000000083	0+00165160000000000084	0+00161060000000000085	0+001560000000000086	0+0016676
0000000087	0+00165360000000000088	0+00162860000000000089	0+001546600000000090	0+0021556
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0000000095	0+00493460000000000096	0+00159760000000000097	0+001500000000000098	0+0015666
0000000099	0F0019043000000000101	0+00170676000000000201	0+0017916600000000301	0+0073076
0000000+01	0+0002156000000000103	0+00165776000000000203	0+0017406600000000303	0+0073036
0000000+03	0+0026926000000000105	0+00170536000000000205	0+0017500000000000305	0+0061426
0000000+05	0+0021366000000000107	0+00162466000000000207	0+0017116600000000307	0+0059636
0000000+07	0+0025736000000000109	0+00159526000000000209	0+0015978600000000309	0+0059256
0000000+09	0+0025176000000000111	0+00160496000000000211	0+0020052600000000311	0+0049916
0000000+11	0+0021436000000000113	0+00160606000000000213	0+0016595100000000313	0+0070236
0000000+13	0+0027000000000000115	0+00165596000000000215	0+0016694600000000315	0+0049856
0000000+15	0+0022176000000000117	0+00175346000000000217	0+0016857600000000317	0+0049416
0000000+17	0+0025376000000000119	0+00172076000000000219	0+0016852600000000319	0+0049126
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0000000+21	0+0021326000000000123	0+00183456000000000223	0+0015307600000000323	0+0050246
0000000+23	0+0027156000000000125	0+00187576000000000225	0+0021627600000000325	0+0049556
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0000000+29	0+0025396000000000131	0+00155866000000000231	0+0021497600000000331	0+0054076
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0000000+33	0+0026746000000000135	0+00177506000000000235	0+0021454600000000335	0+0054916
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0000000+39	0+0026206000000000141	0+00170736000000000241	0+0017516600000000341	0+0073076
0000000+41	0+0004046000000000143	0+00170736000000000243	0+0017519600000000343	0+0073076
0000000+43	0+0004046000000000145	0+00256860000000000245	0+0036550600000000345	0+0003656
0000000+45	0+0074036000000000147	0+00535806000000000247	0+0055192600000000347	0+0062566
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TEST I.O. NUMBER 212051015050

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0000000063	0+000271600000000064	0+001591600000000065	0+001591600000000065	0+001591600000000065	0+001591600000000065
0000000067	0+001493600000000068	0+001477600000000069	0+001477600000000070	0+001477600000000070	0+001477600000000070
0000000071	0+0014+16000000000072	0+0014+36000000000073	0+0014+36000000000074	0+0014+36000000000074	0+0014+36000000000074
0000000075	0+0014+32600000000076	0+0014+22600000000077	0+0014+22600000000078	0+0014+22600000000078	0+0014+22600000000078
0000000079	0+001657600000000080	0+0014+46000000000081	0+001617600000000082	0+001617600000000082	0+001617600000000082
0000000083	0+001557600000000084	0+0014+46000000000085	0+001524600000000086	0+001524600000000086	0+001524600000000086
0000000087	0+001502600000000088	0+0014+56000000000089	0+001432600000000090	0+001432600000000090	0+001432600000000090
0000000091	0+001503600000000092	0+001402600000000093	0+001457600000000094	0+001457600000000094	0+001457600000000094
0000000095	0+056540000000000096	0+001484600000000097	0+001464600000000098	0+001464600000000098	0+001464600000000098
0000000099	0F001007300000000101	0+01700460000000000201	0+01751660000000000301	0+01751660000000000301	0+01751660000000000301
0000000101	0+002046600000000102	0+01240760000000000203	0+01724060000000000303	0+01724060000000000303	0+01724060000000000303
0000000103	0+002475600000000105	0+01704760000000000205	0+01755560000000000305	0+01755560000000000305	0+01755560000000000305
0000000105	0+001895600000000107	0+01602460000000000207	0+01684460000000000307	0+01684460000000000307	0+01684460000000000307
0000000107	0+002455600000000109	0+01555860000000000209	0+01842860000000000309	0+01842860000000000309	0+01842860000000000309
0000000109	0+002143600000000111	0+01564360000000000211	0+01870160000000000311	0+01870160000000000311	0+01870160000000000311
0000000111	0+001961600000000113	0+01563560000000000213	0+01654860000000000313	0+01654860000000000313	0+01654860000000000313
0000000113	0+002561600000000115	0+01603960000000000215	0+01654460000000000315	0+01654460000000000315	0+01654460000000000315
0000000115	0+001899600000000117	0+01650260000000000217	0+01648660000000000317	0+01648660000000000317	0+01648660000000000317
0000000117	0+002523600000000119	0+01703060000000000219	0+01649360000000000319	0+01649360000000000319	0+01649360000000000319
0000000119	0+002243600000000121	0+01711460000000000221	0+01858160000000000321	0+01858160000000000321	0+01858160000000000321
0000000121	0+002032600000000123	0+01737260000000000223	0+01874560000000000323	0+01874560000000000323	0+01874560000000000323
0000000123	0+002557600000000125	0+01809660000000000225	0+02034060000000000325	0+02034060000000000325	0+02034060000000000325
0000000125	0+001304600000000127	0+01844160000000000227	0+02026260000000000327	0+02026260000000000327	0+02026260000000000327
0000000127	0+002540600000000129	0+01845960000000000229	0+02044160000000000329	0+02044160000000000329	0+02044160000000000329
0000000129	0+002317600000000131	0+01233460000000000231	0+02021260000000000331	0+02021260000000000331	0+02021260000000000331
0000000131	0+002219600000000133	0+01277760000000000233	0+01939860000000000333	0+01939860000000000333	0+01939860000000000333
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0000000137	0+002412600000000139	0+01731060000000000239	0+02034260000000000339	0+02034260000000000339	0+02034260000000000339
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0000000143	0+000406600000000145	0+03569960000000000245	0+03695526000000000345	0+03695526000000000345	0+03695526000000000345
0000000145	0+007411600000000147	0+05335360000000000247	0+05551526000000000347	0+05551526000000000347	0+05551526000000000347
0000000147	0+0141+06				







TEST I.O. NUMBER 212051F14360

0000000212	0515143600000000000056	(+002071600000000000057	0+00205260000000000058	0+00173326
0000000059	0+00001160000000000060	(+000298600000000000061	0+00029500000000000062	0+0002896
0000000063	0+00029060000000000064	(+00222160000000000065	0+002198000000000066	0+0020746
0000000067	0+00207160000000000068	0+00209460000000000069	0+002055600000000070	0+0020096
0000000071	0+00200060000000000072	(+00201960000000000073	0+002015600000000074	0+0021136
0000000075	0+00222760000000000076	(+00192760000000000077	0+002125600000000078	0+0022196
0000000079	0+00235660000000000080	0+00215360000000000081	0+002253600000000082	0+0020346
0000000083	0+00215460000000000084	(+00195560000000000085	0+002106600000000086	0+0021836
0000000087	0+00203960000000000088	(+00212660000000000089	0+001947600000000090	0+0012006
0000000091	0+00216360000000000092	(+00190760000000000093	0+002112600000000094	0+0020046
0000000095	0+00569696000000000096	(+00216560000000000097	0+002042600000000098	0+0021256
0000000099	0F0012063000000000101	(+00170556000000000201	0+017508600000000301	0+0073106
0000000401	0+0020806000000000103	0+0161536000000000203	0+016585600000000303	0+0073096
0000000403	0+0031516000000000105	(+00170306000000000205	0+017879600000000305	0+0071486
0000000405	0+0019246000000000107	(+00156716000000000207	0+016488600000000307	0+0066316
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0000000415	0+0013306000000000117	(+00165326000000000217	0+015595600000000317	0+0039966
0000000417	0+0029536000000000119	(+00170706000000000219	0+015595600000000319	0+0039496
0000000419	0+0026446000000000121	(+00173760000000000221	0+019755600000000321	0+0039816
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0000000425	0+0020616000000000127	(+00192476000000000227	0+015807600000000327	0+0040416
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0000000441	0+0000412600000000143	(+00170606000000000243	0+017510600000000343	0+0073096
0000000443	0+0004116000000000145	(+00356756000000000245	0+036544600000000345	0+0003656
0000000445	0+0074176000000000147	(+00535826000000000247	0+05552026000000000347	0+0063026
0000000447	0+0141526			





TEST I.O. NUMBER 2120F1715560

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0000000063 0+000235600000000064 C+002269500000000065 0+0022516000000066 0+0021336  
0000000067 0+002136000000000068 C+002131600000000069 0+0021046000000070 0+0020476  
0000000071 0+002043600000000072 C+002044600000000073 0+0020476000000074 0+0022216  
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0000000087 0+002147600000000088 C+002154600000000089 0+0019576000000090 0+0011516  
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0000000427 0+003436600000000129 C+001951160000000229 0+0224136000000329 0-0040206  
0000000429 0+003395600000000131 C+001859600000000231 0+0221236000000331 0-0043476  
0000000431 0+002928600000000133 C+001123600000000233 0+0219026000000333 0-0040436  
0000000433 0+003523600000000135 C+001550860000000235 0+0221036000000335 0-0040856  
0000000435 0+002974600000000137 C+001707760000000237 0+0223576000000337 0-0040856  
0000000437 0+003330600000000139 C+001853160000000239 0+0223016000000339 0-0045606  
0000000439 0+003478600000000141 C+001705360000000241 0+0175026000000341 0-0073076  
0000000441 0+000041360000000143 C+001705360000000243 0+0175036000000343 0-0073086  
0000000443 0+000041360000000145 C+003566460000000245 0+0365326000000345 0-0003656  
0000000445 0+007417600000000147 C+005357060000000247 0+0551656000000347 0+0063026  
0000000447 0+0141506



TEST I.O. NUMBER 2120519163:0

0000000012	0519103500000000000050	0+00212960000000000057	0+0021100000000000058	0+0017246
0000000059	0+00001360000000000051	0+00093556000000000051	0+000300000000000062	0+0003016
0000000063	0+000300000000000054	0+002443600000000055	0+002425000000000066	0+0023146
0000000067	0+002225000000000058	0+002234000000000063	0+002219000000000070	0+0021076
0000000071	0+002101000000000072	0+002033000000000073	0+002107000000000074	0+0023076
0000000075	0+002346000000000076	0+002037000000000077	0+002270000000000078	0+0023976
0000000079	0+002457000000000080	0+002242000000000081	0+002425000000000082	0+0021986
0000000083	0+002334000000000084	0+002247000000000085	0+002185000000000086	0+0023516
0000000087	0+002331000000000088	0+002275000000000089	0+002187000000000090	0+0021226
0000000091	0+002310000000000092	0+002040000000000093	0+002235000000000094	0+0021206
0000000095	0+004000000000000096	0+002270000000000097	0+002102000000000098	0+0021956
0000000099	0F001203000000000101	0+0017033000000000201	0+0017052000000000301	0+0021936
0000000101	0+003027000000000103	0+0010310000000000203	0+0017150000000000303	0+0021936
0000000103	0+003030000000000105	0+0017022000000000205	0+0017000000000000305	0+0055176
0000000105	0+002024000000000107	0+0015917000000000207	0+0016734000000000307	0+0052766
0000000107	0+003570000000000109	0+0015401000000000209	0+0021040000000000309	0+0052346
0000000109	0+003523000000000111	0+0015352000000000211	0+0021102000000000311	0+0030366
0000000111	0+002950000000000113	0+0015529000000000213	0+0010415000000000313	0+0030856
0000000113	0+003530000000000115	0+0010402000000000215	0+0016412000000000315	0+0030826
0000000115	0+003040000000000117	0+0017735000000000217	0+0016255000000000317	0+0037506
0000000117	0+003540000000000119	0+0017235000000000219	0+0016355000000000319	0+0035966
0000000119	0+003515000000000121	0+0015355000000000221	0+0020405000000000321	0+0037196
0000000121	0+003013000000000123	0+0015001000000000223	0+0020120000000000323	0+0030446
0000000123	0+003050000000000125	0+0015530000000000225	0+0023450000000000325	0+0037836
0000000125	0+003135000000000127	0+0015924000000000227	0+0023300000000000327	0+00308306
0000000127	0+003000000000000129	0+0015914000000000229	0+0023530000000000329	0+0030546
0000000129	0+005049000000000131	0+0010435400000000231	0+0023307000000000331	0+0045536
0000000131	0+005135000000000133	0+0010439600000000233	0+0023072000000000333	0+0039056
0000000133	0+003794000000000135	0+0010439600000000235	0+0023244000000000335	0+0046266
0000000135	0+003137000000000137	0+0015546000000000237	0+0023472000000000337	0+0040426
0000000137	0+003514000000000139	0+0020270000000000239	0+0023405000000000339	0+0042236
0000000139	0+003752000000000141	0+0017048000000000241	0+0017050000000000341	0+0073066
0000000141	0+000415000000000143	0+0017048000000000243	0+0017050000000000343	0+0073086
0000000143	0+000415000000000145	0+0035500000000000245	0+0030521000000000345	0+0003066
0000000145	0+007417000000000147	0+0053500000000000247	0+0055150000000000347	0+0063026
0000000147	0+0141526			

TEST I.O. NUMBER 212070215070

0000000212	07021507000000000056	C+0022456000000000057	0+0022255600000000058	0+0009706
0000000053	0+00000350000000000050	C-00013450000000000051	0-0001445000000000062	0-0001406
0000000063	0-0843+86000000000064	C+002329600000000065	0+002451600000000066	0+0022756
0000000067	0+00227960000000000068	C+002250600000000069	0+002226600000000070	0+0021376
0000000071	0+00212360000000000072	C+002173600000000073	0+002172600000000074	0+0023326
0000000075	0+00243160000000000076	C+002109600000000077	0+002326600000000078	0+0025156
0000000079	0+00263660000000000080	C+002375600000000081	0+002577600000000082	0+0022116
0000000083	0+00244060000000000084	C+002132600000000085	0+002310600000000086	0+0024366
0000000087	0+00222660000000000088	C+002411600000000089	0+002111600000000090	0-0008406
0000000091	0+00240960000000000092	C+002072600000000093	0+002386600000000094	0+0021556
0000000095	0+04665160000000000096	C+002355600000000097	0+002215600000000098	0+0023456
0000000099	0F0013453000000000101	C+0172906000000000101	0+0161406000000000101	0-0072526
0000000401	0+0029396000000000103	C+0161746000000000103	0+0169726000000000103	0-0072926
0000000403	0+0046726000000000105	C+0172726000000000105	0+0161166000000000105	0-0061016
0000000405	0+0026556000000000107	C+0156166000000000107	0+0164326000000000107	0-0056926
0000000407	0+0043706000000000109	C+0147866000000000109	0+0165206000000000109	0-0057256
0000000409	0+0035796000000000111	C+0150526000000000111	0+0165176000000000111	0-0024086
0000000411	0+0027706000000000113	C+0152236000000000113	0+0158866000000000113	0-0024396
0000000413	0+0045996000000000115	C+0156506000000000115	0+0156786000000000115	0-0023256
0000000415	0+0025486000000000117	C+0177096000000000117	0+0158006000000000117	0-0022586
0000000417	0+0043536000000000119	C+0174536000000000119	0+0156116000000000119	0-0022206
0000000419	0+0030326000000000121	C+0158196000000000121	0+0215516000000000121	0-0023026
0000000421	0+0029966000000000123	C+0134366000000000123	0+0211306000000000123	0-0023506
0000000423	0+0048726000000000125	C+0206866000000000125	0+0223546000000000125	0-0023206
0000000425	0+0025236000000000127	C+0212526000000000127	0+0221146000000000127	0-0022886
0000000427	0+0044636000000000129	C+0210146000000000129	0+0225186000000000129	0-0022756
0000000429	0+0057376000000000131	C+0110216000000000131	0+0221086000000000131	0-0041376
0000000431	0+0031296000000000133	C+0102366000000000133	0+0216156000000000133	0-0027376
0000000433	0+0048976000000000135	C+0142926000000000135	0+0219066000000000135	0-0045176
0000000435	0+0028546000000000137	C+0149166000000000137	0+0224096000000000137	0-0029896
0000000437	0+0045256000000000139	C+0154276000000000139	0+0222556000000000139	0-0040016
0000000439	0+0041196000000000141	C+0173056000000000141	0+0161336000000000141	0-0072876
0000000441	0+0002956000000000143	C+0173056000000000143	0+0161536000000000143	0-0072676
0000000443	0+0002956000000000145	0+0358536000000000145	0+0371556000000000145	0-0003566
0000000445	0+0072376000000000147	C+0537446000000000147	0+0553556000000000147	0+0062396
0000000447	0+0139386			























TEST 1.0. NUMBER 301130015333

0000000301	16061538500000000057	C+004570600000000053	0+001247800000000059	0+0000106
0000000302	0+000567600000000051	L+000657600000000062	0+000668600000000063	0+0006686
0000000303	0+000513660000000055	C+000555600000000065	0+004725600000000067	0+0046106
0000000304	0+004225600000000059	0+004483600000000070	0+004418600000000071	0+0043766
0000000305	0+004446000000000073	C+004365600000000074	0+004702600000000075	0+0048876
0000000306	0+004347600000000077	0+004416000000000078	0+003020600000000079	0+0052926
0000000307	0+004727600000000081	0+005085600000000082	0+004516600000000083	0+0049666
0000000308	0+004353600000000085	C+004679600000000085	0+004808600000000087	0+0045266
0000000309	0+004546000000000089	C+004235600000000090	0+004555600000000091	0+0047856
0000000310	0+004258600000000093	C+004816600000000094	0+004357600000000095	0+0219956
0000000311	0+004549600000000097	0+004482600000000098	0+004704600000000099	0F0017353
0000000312	0+017049600000000201	C+010106000000000301	0+007272600000000401	0+0040546
0000000313	0+015506000000000203	C+014504600000000303	0+007272600000000403	0+0066216
0000000314	0+017001600000000205	C+015983600000000305	0+003147600000000405	0+0034716
0000000315	0+014336000000000207	C+013783600000000307	0+004425600000000407	0+0065616
0000000316	0+013531600000000209	C+014930600000000309	0+004540600000000409	0+0044326
0000000317	0+013331500000000211	C+015210600000000311	0+000016600000000411	0+0036346
0000000318	0+014067600000000213	C+013327600000000313	0+000120600000000413	0+0060886
0000000319	0+014345600000000215	C+013006600000000315	0+000166600000000415	0+0031216
0000000320	0+017245600000000217	0+012907600000000317	0+000174600000000417	0+0062546
0000000321	0+017381600000000219	C+012917600000000319	0+000472600000000419	0+0043296
0000000322	0+013877600000000221	C+021824600000000321	0+000347600000000421	0+0040506
0000000323	0+021039600000000223	0+020804600000000323	0+000631600000000423	0+0062726
0000000324	0+022509600000000225	C+022766600000000325	0+000620600000000425	0+0032866
0000000325	0+023278600000000227	C+022473600000000327	0+000665600000000427	0+0064066
0000000326	0+022715600000000229	C+023107600000000329	0+000757600000000429	0+0045836
0000000327	0+010177600000000231	C+022609600000000331	0+002220600000000431	0+0047056
0000000328	0+009324600000000233	C+021509600000000333	0+000354600000000433	0+0068476
0000000329	0+014026600000000235	0+022146600000000335	0+003151600000000435	0+0035676
0000000330	0+014866000000000237	0+022927600000000337	0+000313600000000437	0+0065206
0000000331	0+015631600000000239	C+022789600000000339	0+002813600000000439	0+0052976
0000000332	0+017050600000000241	C+016016600000000341	0+007272600000000441	0+0000146
0000000333	0+017050600000000243	C+016016600000000343	0+007272600000000443	0+0000136
0000000334	0+035732600000000245	0+035095600000000345	0+000321600000000445	0+0070446
0000000335	0+053072600000000247	C+053337600000000347	0+006342600000000447	0+0137906











TEST I.D. NUMBER 3011e1e15730

0000000301	1816157900000000000057	0+00000000000000000053	0+00184900000000000059	0+00001006
0000000060	0+00000600000000000061	0+00060500000000000062	0+00060600000000000063	0+00060556
0000000064	0+00073260000000000065	0+00060600000000000066	0+00060600000000000067	0+00060516
0000000063	0+00000000000000000069	0+00000000000000000070	0+00000000000000000071	0+0000000070
0000000072	0+00000000000000000073	0+00000000000000000074	0+00000000000000000075	0+0000000076
0000000076	0+00000000000000000077	0+00000000000000000078	0+00000000000000000079	0+0000000079
0000000080	0+00000000000000000081	0+00000000000000000082	0+00000000000000000083	0+0000000080
0000000084	0+00000000000000000085	0+00000000000000000086	0+00000000000000000087	0+0000000086
0000000088	0+00000000000000000089	0+00000000000000000090	0+00000000000000000091	0+0000000088
0000000092	0+00000000000000000093	0+00000000000000000094	0+00000000000000000095	0+0000000092
0000000096	0+00000000000000000097	0+00000000000000000098	0+00000000000000000099	0+0000000096
0000000101	0+00000000000000000102	0+00000000000000000103	0+00000000000000000104	0+0000000101
0000000103	0+00000000000000000104	0+00000000000000000105	0+00000000000000000106	0+0000000103
0000000105	0+00000000000000000106	0+00000000000000000107	0+00000000000000000108	0+0000000105
0000000107	0+00000000000000000108	0+00000000000000000109	0+00000000000000000110	0+0000000107
0000000109	0+00000000000000000110	0+00000000000000000111	0+00000000000000000112	0+0000000109
0000000111	0+00000000000000000112	0+00000000000000000113	0+00000000000000000114	0+0000000111
0000000113	0+00000000000000000114	0+00000000000000000115	0+00000000000000000116	0+0000000113
0000000115	0+00000000000000000116	0+00000000000000000117	0+00000000000000000118	0+0000000115
0000000117	0+00000000000000000118	0+00000000000000000119	0+00000000000000000120	0+0000000117
0000000119	0+00000000000000000120	0+00000000000000000121	0+00000000000000000122	0+0000000119
0000000121	0+00000000000000000122	0+00000000000000000123	0+00000000000000000124	0+0000000121
0000000123	0+00000000000000000124	0+00000000000000000125	0+00000000000000000126	0+0000000123
0000000125	0+00000000000000000126	0+00000000000000000127	0+00000000000000000128	0+0000000125
0000000127	0+00000000000000000128	0+00000000000000000129	0+00000000000000000130	0+0000000127
0000000129	0+00000000000000000130	0+00000000000000000131	0+00000000000000000132	0+0000000129
0000000131	0+00000000000000000132	0+00000000000000000133	0+00000000000000000134	0+0000000131
0000000133	0+00000000000000000134	0+00000000000000000135	0+00000000000000000136	0+0000000133
0000000135	0+00000000000000000136	0+00000000000000000137	0+00000000000000000138	0+0000000135
0000000137	0+00000000000000000138	0+00000000000000000139	0+00000000000000000140	0+0000000137
0000000139	0+00000000000000000140	0+00000000000000000141	0+00000000000000000142	0+0000000139
0000000141	0+00000000000000000142	0+00000000000000000143	0+00000000000000000144	0+0000000141
0000000143	0+00000000000000000144	0+00000000000000000145	0+00000000000000000146	0+0000000143
0000000145	0+00000000000000000146	0+00000000000000000147	0+00000000000000000148	0+0000000145
0000000147	0+00000000000000000148	0+00000000000000000149	0+00000000000000000150	0+0000000147











TEST I.D. NUMBER 301231319200

0000000301	23131520000000000057	[+00015000000000000058	0+00135500000000000059	0+0000126
0000000000	0+00007260000000000051	[+00000046000000000062	0+00005500000000000063	0+00000396
0000000064	0+00019900000000000055	[+00000560000000000060	0+00057000000000000067	0+00054976
0000000068	0+00023000000000000059	[+00033000000000000070	0+00051200000000000071	0+00050936
0000000072	0+00051100000000000073	[+00050540000000000074	0+00053300000000000075	0+00056756
0000000076	0+00051150000000000077	[+00055036000000000078	0+00051170000000000079	0+00061166
0000000080	0+00055100000000000081	[+00055500000000000082	0+00053400000000000083	0+00059376
0000000084	0+00049050000000000085	[+00054190000000000086	0+00054770000000000087	0+00051596
0000000088	0+00073000000000000089	[+00075060000000000090	0+00052590000000000091	0+00052386
0000000092	0+00099000000000000093	[+00055020000000000094	0+00045250000000000095	0+0228156
0000000096	0+00050100000000000097	[+00052230000000000098	0+00053260000000000099	0F0019543
0000000100	0+00173900000000000101	[+00162780000000000102	0+00032500000000000103	0+00342736
0000000104	0+00155000000000000105	[+00142350000000000106	0+00032500000000000107	0+00363436
0000000108	0+00173500000000000109	[+00162360000000000110	0+00011530000000000111	0+00323916
0000000112	0+00129000000000000113	[+00133500000000000114	0+00023740000000000115	0+00387926
0000000116	0+00135700000000000117	[+00121530000000000118	0+00052100000000000119	0+00327936
0000000120	0+00135700000000000121	[+00122510000000000122	0+00122230000000000123	0+00334456
0000000124	0+00135700000000000125	[+00123540000000000126	0+00102050000000000127	0+00374576
0000000128	0+00143020000000000129	[+00124010000000000130	0+00120570000000000131	0+00319446
0000000132	0+00153200000000000133	[+00121310000000000134	0+00111330000000000135	0+00379706
0000000136	0+00177300000000000137	[+00122550000000000138	0+00125410000000000139	0+00329336
0000000140	0+00204030000000000141	[+00205150000000000142	0+00113300000000000143	0+00336176
0000000144	0+00235200000000000145	[+00230300000000000146	0+00130220000000000147	0+00365546
0000000148	0+00241600000000000149	[+00234450000000000150	0+00123700000000000151	0+00318246
0000000152	0+00248200000000000153	[+00227780000000000154	0+00135070000000000155	0+00377706
0000000156	0+00251240000000000157	[+00241490000000000158	0+00122300000000000159	0+00328836
0000000160	0+00251400000000000161	[+00211760000000000162	0+00080000000000000163	0+00342326
0000000164	0+00256000000000000165	[+00210100000000000166	0+00106450000000000167	0+00379166
0000000168	0+00113250000000000169	[+00225170000000000170	0+00055010000000000171	0+00319566
0000000172	0+00122310000000000173	[+00222700000000000174	0+00113010000000000175	0+00376996
0000000176	0+00131110000000000177	[+00237290000000000178	0+00047750000000000179	0+00335306
0000000180	0+00050220000000000181	[+00052700000000000182	0+00030570000000000183	0+00243556
0000000184	0+00104130000000000185	[+00173120000000000186	0+00072000000000000187	0+00288036
0000000188	0+00300320000000000189	[+00322970000000000190	0+00075460000000000191	0+00357146
0000000192	0+00053420000000000193	[+00053520000000000194	0+00144050000000000195	0+00427066





# TEST I.C. NUMBER 301231615700

0000000301	23161700000000000057	C+00523460000000000058	0+00128760000000000059	0+00000146
000000060	0+000072600000000061	C+00006460000000000062	0+000065600000000063	0+00000676
000000064	0+000173600000000065	C+00060736000000000066	0+005354600000000067	0+0054856
000000063	0+000224600000000069	C+005353600000000070	0+005105600000000071	0+0050598
000000072	0+000396000000000073	C+005057600000000074	0+005327600000000075	0+0057326
000000076	0+005115600000000077	C+005338600000000078	0+005563600000000079	C+0060336
000000080	0+005574600000000081	C+005724600000000082	0+005252600000000083	0+0058546
000000084	0+004342600000000085	C+005451600000000086	0+005362600000000087	0+0051346
000000088	0+005633600000000089	C+004901600000000090	0+005368600000000091	0+0052456
000000092	0+005006000000000093	C+005608600000000094	0+005037600000000095	0+0210306
000000096	0+005297600000000097	C+005136600000000098	0+005455600000000099	0F0019933
000000101	0+017396000000000201	C+0162796000000000301	0+000326600000000401	0+0348636
000000103	0+015546000000000203	C+0142966000000000303	0+000327600000000403	0+0379176
000000105	0+017350600000000205	C+0162316000000000305	0+004125600000000405	0+0335216
000000107	0+014623600000000207	C+0134436000000000307	0+004524600000000407	0+0384386
000000109	0+013029600000000209	C+0154466000000000309	0+004672600000000409	0+0342776
000000111	0+013452600000000211	C+0156326000000000311	0+012121600000000411	0+0344816
000000113	0+013740600000000213	C+0124156000000000313	0+010202600000000413	0+0374206
000000115	0+014339600000000215	C+0124756000000000315	0+012053600000000415	C+0331296
000000117	0+016609600000000217	C+0122026000000000317	0+011613600000000417	0+0379826
000000119	0+017763600000000219	C+0123346000000000319	0+012540600000000419	0+0342386
000000121	0+020579600000000221	C+0255546000000000321	0+011331600000000421	0+0345246
000000123	0+023519600000000223	C+0230256000000000323	0+012576600000000423	0+0377036
000000125	0+024276000000000225	C+0266356000000000325	0+012324600000000425	0+0330366
000000127	0+024930600000000227	C+0259196000000000327	0+013450600000000427	0+0380586
000000129	0+026112600000000229	C+0273036000000000329	0+012256600000000429	0+0346566
000000131	0+010452600000000231	C+0269376000000000331	0+008152600000000431	0+0347896
000000133	0+013754600000000233	C+0248386000000000333	0+010327600000000433	0+0386386
000000135	0+015486000000000235	C+0255536000000000335	0+006656000000000435	0+0332566
000000137	0+015332600000000237	C+0272856000000000337	0+011621600000000437	0+0380296
000000139	0+016373600000000239	C+0273176000000000339	0+005206000000000439	0+0355356
000000141	0+006619600000000241	C+0052706000000000341	0-003859600000000441	0+0243606
000000143	0+018411600000000243	C+0173116000000000343	0+000715600000000443	0+0288546
000000145	0+036037600000000245	C+0352526000000000345	0+007544600000000445	0+0357156
000000147	0+053926600000000247	C+0535266000000000347	0+014467600000000447	0+0427166

TEST I.O. NUMBER 301240015302

0000000301	2408153020000000000057	0+00335760000000000050	0+00113600000000000059	0+0000120
0000000060	0+00008760000000000061	0+00007960000000000062	0+00000810000000000063	0+00000830
0000000064	0+00642660000000000065	0+00629760000000000066	0+00522400000000000067	0+0057240
0000000068	0+00540600000000000069	0+00533860000000000070	0+00537000000000000071	0+00533000
0000000072	0+00531600000000000073	0+00527160000000000074	0+00551000000000000075	0+00593000
0000000076	0+00537960000000000077	0+00569760000000000078	0+00632000000000000079	0+00635600
0000000080	0+00575460000000000081	0+00607760000000000082	0+00555000000000000083	0+00617100
0000000084	0+00511760000000000085	0+00563360000000000086	0+00525000000000000087	0+00534000
0000000088	0+00599660000000000089	0+00496000000000000090	0+00553000000000000091	0+00534500
0000000092	0+00525360000000000093	0+00502460000000000094	0+00517000000000000095	0+01770000
0000000096	0+00520660000000000097	0+00542860000000000098	0+00500100000000000099	0F0020203
0000000101	0+01750260000000000101	0+01640760000000000101	0+00033300000000000101	0+03470900
0000000103	0+01545160000000000103	0+01432260000000000103	0+00033300000000000103	0+03053100
0000000105	0+01745160000000000105	0+01636160000000000105	0+00127400000000000105	0+03226900
0000000107	0+01456660000000000107	0+01341760000000000107	0+00461700000000000107	0+03904000
0000000109	0+01291700000000000109	0+01276360000000000109	0+00511300000000000109	0+03331000
0000000111	0+01329460000000000111	0+01297960000000000111	0+01202000000000000111	0+03395000
0000000113	0+01362260000000000113	0+01236160000000000113	0+01071500000000000113	0+03769500
0000000115	0+01430960000000000115	0+01239460000000000115	0+01252000000000000115	0+03223900
0000000117	0+01653760000000000117	0+01210660000000000117	0+01100000000000000117	0+03020800
0000000119	0+01792460000000000119	0+01223960000000000119	0+01361000000000000119	0+03331100
0000000121	0+02061460000000000121	0+02509260000000000121	0+01156600000000000121	0+03400300
0000000123	0+02360160000000000123	0+02347460000000000123	0+01354500000000000123	0+03722100
0000000125	0+02463260000000000125	0+02474060000000000125	0+01307500000000000125	0+03221600
0000000127	0+02542660000000000127	0+02308860000000000127	0+01421000000000000127	0+03014000
0000000129	0+02605460000000000129	0+02537960000000000129	0+01250000000000000129	0+03324000
0000000131	0+00996260000000000131	0+02440500000000000131	0+00062000000000000131	0+03500400
0000000133	0+00890360000000000133	0+02281400000000000133	0+01000000000000000133	0+03023200
0000000135	0+01307360000000000135	0+02359060000000000135	0+00025200000000000135	0+03230000
0000000137	0+01296160000000000137	0+02544760000000000137	0+01102300000000000137	0+03012100
0000000139	0+01365260000000000139	0+02484460000000000139	0+00534700000000000139	0+03401000
0000000141	0+00657460000000000141	0+00524360000000000141	0+00391100000000000141	0+02415300
0000000143	0+01839860000000000143	0+01731060000000000143	0+00007500000000000143	0+02070300
0000000145	0+03615360000000000145	0+03543560000000000145	0+00755400000000000145	0+03560000
0000000147	0+00540406000000000147	0+05366160000000000147	0+00144750000000000147	0+04255800



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